Final Geotechnical Data Report Tri-City Water Pollution Control Plant Phase 1 Expansion Clackamas County, Oregon

May, 2008

# SHANNON & WILSON, INC.

GEOTECHNICAL AND ENVIRONMENTAL CONSULTANTS

Final Geotechnical Data Report Tri-City Water Pollution Control Plant Phase 1 Expansion Clackamas County, Oregon

May, 2008



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# FINAL GEOTECHNICAL DATA REPORT FOR TRI-CITY WATER POLLUTION CONTROL PLANT PHASE ONE EXPANSION CLACKAMAS COUNTY, OREGON

#### **1.0 INTRODUCTION**

## 1.1 Background

This Geotechnical Data Report presents a summary of the geotechnical data that was obtained and compiled for site characterization and to support the design phase of the proposed Tri-City Water Pollution Control Plant (WPCP) Interim Expansion, which includes upgrades to the existing facility and the construction of a new Membrane Bioreactor treatment facility. This expansion will provide capacity to handle growth from both the Tri-City Service District (TCSD) and Clackamas County Service District No. 1 (CCSD#1). Water Environment Services (WES, a department of Clackamas County) has contracted the MWH team to provide engineering services for the design of the Interim Expansion.

The project elements, as Shannon & Wilson (S&W) currently understands, are as described in the following section:

- Storm water control- WES is investing systems that reduce the amount of storm water that leaves both the existing and proposed plant site.
- Meet future treatment demands- Increased treatment capacity will be obtained though the construction of a new Membrane Bioreactor Process.
- Integrating future expansion- MWH is developing a master plan that will allow future expansion of the proposed facility.

### 1.2 Site Location

The WPCP is located at 15951 S. Agnes Ave in Clackamas County near the confluence of the Clackamas and the Willamette Rivers. The legal location description is the SE Quarter of the SW Quarter of Section 20 in Township 2 South and Range 2 East. Figure 1, Vicinity Map shows the project location in relation to nearby landmarks. The proposed plant expansion area will be

immediately to the south of the existing plant. Preliminary locations of each of the interim expansion structures in relation to the existing plant are shown on Figure 2.

### 2.0 SCOPE OF WORK

The purpose of this report is to summarize the data collected to provide additional site characterization and to support of the design efforts of MWH for the Tri-City WPCP Phase One Expansion. Also, we understand that the data contained in this report will be used as reference information for preparation of construction documents for the project.

For additional reference information, this report contains a collection of subsurface data gathered from previous projects at the WPCP Site, and are listed in the following section. The subsurface data, which includes boring logs, laboratory test data, and exploration location drawings, were collected by other consultants during a number of different projects for WES.

## 3.0 REVIEW OF EXISTING INFORMATION

The data collected by others, which S&W reviewed and included in this data report are from the following documents.

*"Geotechnical Design Recommendations, Tri-City WPCP Liquids Expansion"* by CH2M Hill, Inc, 2002, prepared for the Tri-City Service District.

"Geotechnical Data Report, Tri-City WPCP Liquids Expansion" by CH2M Hill, Inc, 2002, prepared for the Tri-City Service District.

"Soils Report, Tri-City Sewerage Treatment Plant" by CH2M Hill, Inc, 1982, prepared for the Tri-City Service District.

*"Seismic Vulnerability Assessment, Tri-City Wastewater Treatment Plant"* by URS Corporation, 2002, prepared for Water Environment Services.

*"Phase I and Phase II Environmental Site Assessment, Tax Lot 502"* by URS Corporation, 2001, prepared for Tri-City Service District.

"Remedial Action Work Plan, Unpermitted Rossman Landfill" by URS Corporation, 2000, prepared for Tri-City Service District.

## 4.0 SITE GEOLOGY AND SEISMIC SETTING

## 4.1 Site Topography

The WPCP is located approximately 4500 feet to east / northeast of the confluence of the Willamette and Clackamas River, as shown on Figue 1. The project site is bordered on the north by the Clackamas River and by Clackamette Cove to the southwest, both of which are at approximately elevation 15 ft above mean sea level. To the north and west of the site the ground is relatively flat for approximately 2000 feet before giving rise to steep terrace formations. Onsite, the ground surface near the planned facilities is generally flat, but varies from elevation 44 to 46 feet.

## 4.2 Site Geology

The project site is underlain by three significant geologic units. The youngest unit is found below the relatively shallow site fill and is composed of catastrophic flood deposits laid down during the outwashing of glacial Lake Missoula some 15,000 years ago. Soils found in the flood deposits are generally silts with sand interbeds. The unit found below the flood deposits is known as the Troutdale formation. This unit is made up of many different soil types throughout the Portland area, but locally consists of very dense gravel and cobbles. A geologic unit named Sandy River Mudstone is found below the Troutdale gravels and locally observed along the banks of the Clackamas River. The Sandy River Mudstone Unit is generally composed of Pliocene-aged sedimentary rock beds. When encountered during our explorations the Sandy river mudstone was identified as very soft siltstone/very hard clayey silt.

## 4.3 Seismic Setting

Within the present understanding of the regional tectonic framework and historical seismicity, three broad seismogenic sources have been identified:

- ► A mega-thrust source at in interface between the North American and Juan de Fuca plates in the Cascadia Subduction Zone (CSZ).
- ► A deep subcrustal zone (intra-slab) in the subducted Juan de Fuca Plate and Gorda plates in the CSZ.
- A shallow crustal zone within the forearc of North American Plate.

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For the general area of the WPCP, the seismogenic sources that contribute significantly to the ground motion hazard include both megathrust earthquakes on the CSZ (located about 95 miles west of the site) and shallow crustal earthquakes on nearby faults. The nearest mapped shallow crustal faults are the Portland Hills Fault and the Oatfield Fault. According to the United States Geological Survey (USGS) Quaternary Fault Database, the Oatfield fault has been traced to within less than a mile of the WPCP site. The Portland hills fault has been traced to within 2 miles of the WPCP site.

Table 1 illustrates the different properties or parameters for the earthquakes that contribute to the ground motion hazard levels. We used these earthquake parameters in evaluating the seismic hazards at the Tri-City WPCP site. The magnitudes and distances of earthquakes were obtained from the USGS web site, Probabilistic Seismic Hazard Deaggregation, based upon the project site location (Longitude = -122.590, and Latitude = 45.375). Peak ground accelerations (PGA) shown on Table 1 were obtained from the 2002 USGS Seismic Hazard Maps (Frankel et al., 2002) and USGS Ground Motion Parameter Tool (Version 5.0.7) for the Pacific Northwest Region. The relative contribution of seismogenic sources to the ground motion hazard levels were calculated from the USGS PSHA. As shown on this table shallow crustal and CSZ megathrust earthquakes contribute the most to the seismic hazard at the WPCP site.

Exceedance Probability	Bedrock PGA (g)	Seismogenic Source	Contribution to Seismic Hazard	Modal Distance from Site (km)	Modal Magnitude (M <sub>w</sub> )
2 % in 50 yr	0.389	Shallow Crustal	80 %	10	6.0
		CSZ Intra-slab	N/A	N/A	N/A
		CSZ Megathrust	20 %	95	8.5

## TABLE 1 Earthquake Characterization by Seismogenic Source

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#### 5.0 FIELD EXPLORATIONS, IN-SITU AND LABORATORY TESTING

#### 5.1 Shannon & Wilson Explorations

Shannon & Wilson planned and executed a subsurface exploration program to characterize the subsurface conditions at the WPCP project site. The program consisted of three individual exploration Stages. Stage One efforts focused on developing a general subsurface model across the project site. Stage Two explorations were specifically directed at refining a subsurface anomaly that was detected during the Stage One explorations. Stage Three explorations focused on gathering specific subsurface data that is required for the facility design. The locations of S&W's explorations, in addition to locations of pertinent previous subsurface explorations by others, are illustrated on Figure 2. The relative locations of S&W explorations were established by the use of field methods, including hand taping and laser range finding to known on-site features. The locations of S&W's exploration locations and they too should be considered approximate. A full description of S&W exploration program and logs of the borings are contained in Appendix D.

#### 5.2 Shannon & Wilson Laboratory Testing

A laboratory testing program was developed and implemented in order to evaluate physical and engineering characteristics of the subsurface soils. Laboratory tests on selected soil samples included standard classification tests, which consisted of visual examination, moisture/density tests, Atterberg limits, grain-size analysis, hydrometers, and grain-size wash analysis, i.e., percent finer than the No. 200 sieve. In addition, in-place density tests, in-situ shear strength and unconfined compressive strength tests were conducted on selected undisturbed thin-walled samples. Appendix B contains results from S&W laboratory testing program, in addition to Figure B1, which summarizes all laboratory testing performed on samples collected on-site (this includes the laboratory results from previous work done by others).

## 5.3 Shannon & Wilson In-Situ Testing

## 5.3.1 Falling Head Test On Borehole Piezometers

In order to obtain estimates of the soil hydraulic conductivity, an in-place falling head test was conducted on borings IB-12 and IB-13. A description of these tests results are contained in Appendix C.

## 5.4 Previous Explorations and Laboratory Testing by Others

Contained in Appendix D is information from previous explorations and laboratory tests by others. Only data portions of the reports are included with information we believe is pertinent to the project; however, with most of the references noted, the complete report is available for additional information as needed. The included data from previous work is generally plan of explorations and boring logs and laboratory test results. As noted previously in this report, laboratory results from done by others is summarized together with S&W generated data on Figure B1 in Appendix B; the boring numbers indicate which tests were done by others.

Contained in Appendix D is information from previous explorations and laboratory tests by others. Only data portions of the reports are included with information we believe is pertinent to the project; however, with most of the references noted, the complete report is available for additional information as needed. The data from previous work is generally the subsurface conditions, plan of explorations, boring logs, and laboratory testing.

## 6.0 DISCUSSION OF SUBSURFACE CONDITIONS

## 6.1 Subsurface Soil Conditions

The subsurface soils encountered in the field explorations have been grouped, for discussion purposes, into units, from the ground surface downward, as follows:

- Site Fill
- Alluvial silt, sandy silt and silty sand
- Alluvial gravelly sand and sandy gravel
- Siltstone

A detailed discussion of the soil units is presented in the following paragraphs.

#### 6.1.1 Site Fill

During the explorations S&W has identified several types and locations of fill at this site. We identified three different fill groups. One is on the property to west of the plant site, which we believe is deep (~43 feet) and was part of the backfill for a historic gravel pit. The second type is the fill related to the historic trolley grade, and the third is site fill related to the construction of the original WPCP.

The WPCP fill ranges in thickness from 4 to 7 feet. This fill was part of the original plant construction; therefore, it appears to be made up of excess select fine-grained native soil fill and remnants of the coarse-grained preload fill soils and graveled surface areas. The fine-grained fill is non- to low plasticity medium stiff silt with scatted organics. Thickness of the fine-grained soils was typically between 2 to 3 feet. Below the fine-grained fill, the coarse-grained soils were very dense and consisted of a combination of silt, gravel and cobbles. The coarse-grained soils were typically between 3 to 4 feet thick.

#### 6.1.2 Alluvial silt, sandy silt and silty sand

This layer is quite variable across the site in both composition and relative thickness. This layer is largely made up of silts and silty sands. In some areas, primarily closer to the river, the soil is more sandy. These materials are flood-deposited and fine-grained with low to non-plastic characteristics. Thickness of the deposit ranges from 22 to 37 feet, on average the upper 20 feet of the unit is soft to stiff silt and the lower portion is a 2 to 4 feet thick bed of loose silty sand. The thickness range of this layer in the vicinity of the planned interim structures is 25 to 30 feet.

TABLE 8
Alluvial Silt and Sand Standard Penetration Resistance

Soil	Average	N-values High	Low
Silt	4.5	12	0
Sandy Silt	3.5	15	0
Silty Sand	6	25	0

### 6.1.3 Alluvial gravelly sand, sandy gravel

This material is flood deposited and primarily coarse-grained material with fines in the matrices between gravel particles. This material is non-plastic and dense to very dense. This unit is encountered fairly regularly across the site at an elevation of approximately 20 ft msl with the exception being the anomaly area beneath the proposed fine-screening building where the top of the gravel was significantly lower and was encountered at an elevation of 7 ft msl.

#### TABLE 9

### Alluvial Sand and Gravel Standard Penetration Resistance

Soil	Average	N-values High	Low
Gravel, sandy gravel, gravel with cobbles	>50 bpf	50 blows-1"	18

#### 6.1.4 Siltstone

Below the gravel unit is a siltstone layer that appears to be quite uniform in depth below the ground surface. Based on the borings that encountered the siltstone unit, we estimate the top of the unit is at a depth of 40 ft bgs (EL 5 ft msl). The siltstone is a very weak rock and shows signs of weathering and that remolds to a non-plastic silt or medium plasticity clayey silt depending on the degree of weathering.

#### TABLE 10

Siltstone Standard Penetration Resistance

#### 6.2 Ground Water

Ground water beneath the site was noted during drilling and subsequently measured in piezometers installed in borings IB-6, IB-12, and IB-13. The measured ground water depths with the dates are presented on Table 11. S&W measured the ground water in all of the observation wells on-site that could be located. Additional historic ground water levels measurements by others are contained in Appendix D. The ground water table at this site generally fluctuates seasonally. The highest ground water level is during the late winter and spring periods (January through April) and lowest during the late summer and early fall (August through October). The maximum fluctuation is unknown. Perched ground water at shallow depths above the ground water may be present during all seasons of the year, but especially prevalent following periods of heavy rainfall.

TABLE 11 Ground Water Level Readings

Boring	Depth to gr 7/26/07	ound water from gro 2/25/08	und surface (ft) 4/25/08
IB-6	22.5	33.0	32.6
IB-12		Below well (>15)	Below well (>15)
IB-13		Below well (>15)	Below well (>15)
B-101		32.9	32.2

#### 7.0 LIMITATIONS

This work has been completed and report prepared for the exclusive use of MWH for specific application to the design of the Tri-City Water Pollution Control Plant, Phase 1 Expansion Project. The field explorations and water level measurements indicate subsurface conditions

only at the specific locations and times indicated. Soil and water level variations may exist between exploration and piezometer locations.

The data contained in this report are based upon site conditions as they now exist, and further assume that the explorations performed by others are representative of the subsurface conditions in those project areas. Within the limitations of the scope, schedule, and budget, the data presented in this report were collected and presented in accordance with generally accepted professional geotechnical engineering principles and practice in this area at the time this report was prepared. This work was performed in accordance with generally accepted current local professional practices for the nature of work accomplished no other warranty, express or implied, is made.

If, during final design and construction, subsurface conditions different from those encountered in the field explorations are observed or appear to be present, we should be advised at once so that we can review these conditions and reconsider our data where necessary. If there is a substantial lapse of time between this report and the start of work at the site, or if conditions have changed because of modifications to project layout, natural forces or construction operations at or adjacent to the site, we recommend that this report be reviewed to determine the relevance of the data concerning the changed conditions or the time lapse.

This report is intended to include no interpretive information, and only the data in this report may be provided to prospective contractors as a basis for bidding. This report is not a warranty of subsurface conditions.

Unanticipated soil conditions are commonly encountered and cannot fully be determined by information from the explorations described in this report. Such unexpected conditions frequently require that additional expenditures be made to attain additional information to properly characterize the subsurface conditions. Therefore, some contingency fund is recommended to accommodate the potential for extra costs.

The scope of our geotechnical services did not include any environmental assessment or evaluation regarding the presence or absence of hazardous or toxic materials in the soil, surface

water, ground water, or air, on or below the site, or for evaluation or disposal of contaminated soils or ground water, should any be encountered, except as noted in this report.

Shannon & Wilson, Inc. has prepared a document, "Important Information About Your Geotechnical Report," to assist you and others in understanding the use and limitations of this document. This document is included in Appendix E.

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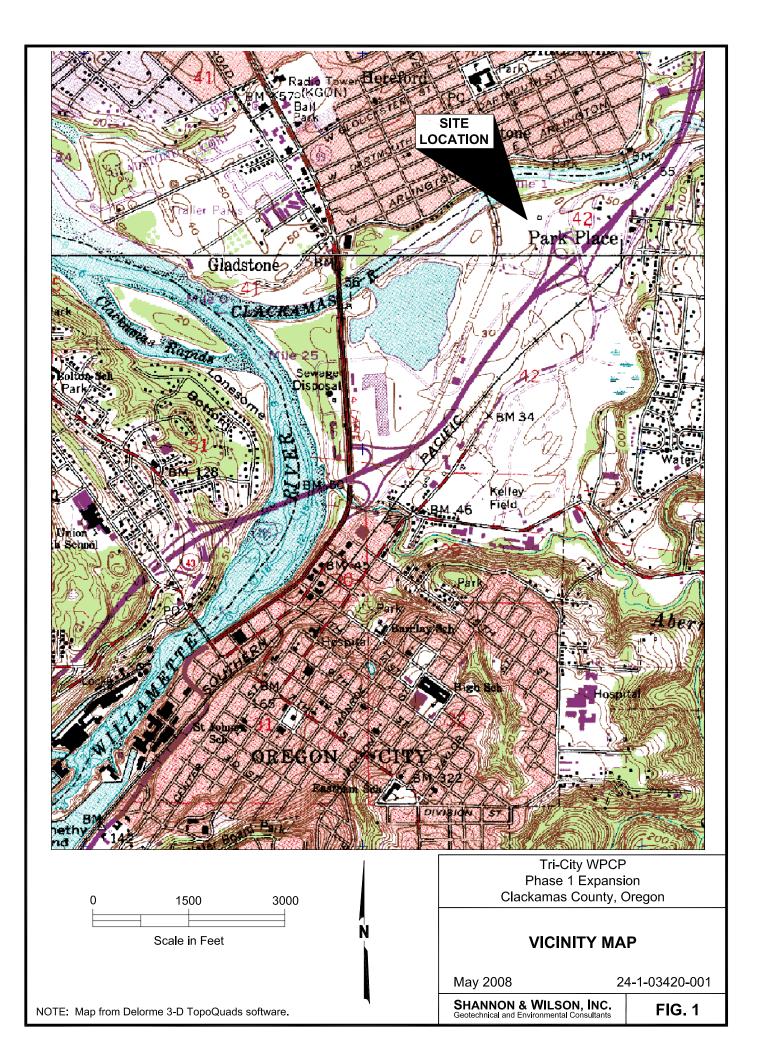
Derrick R. Hayes Engineering Staff

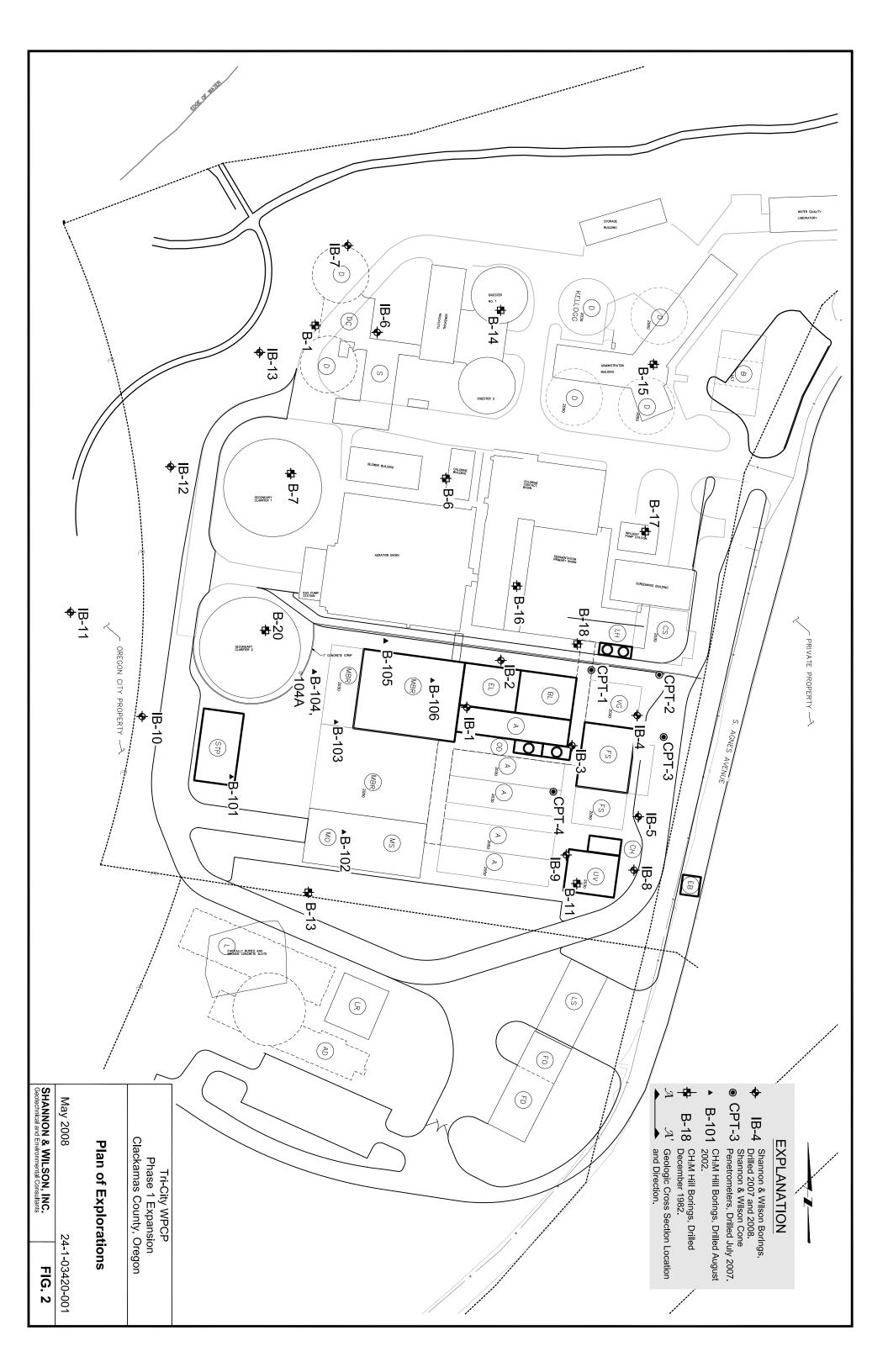


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# APPENDIX A S&W FIELD EXPLORATIONS

Appendix A Doc.doc

## APPENDIX A

## S&W FIELD EXPLORATIONS

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### **APPENDIX** A

### **S&W FIELD EXPLORATIONS**

### A.1 GENERAL

Shannon & Wilson planned and executed a subsurface exploration program to characterize the subsurface conditions at the WPCP project site. The program consisted of three individual exploration Stages. Stage One efforts focused on developing a general subsurface model across the project site. Stage Two explorations were specifically directed at refining a subsurface anomaly that was detected during the Stage One explorations. Stage Three explorations focused on gathering specific subsurface data that is required for the facility design. The locations of S&W's explorations, in addition to locations of pertinent previous subsurface explorations, are illustrated on Figure 2. The relative locations of S&W explorations were established by the use of field methods, including hand taping and laser range finding to known on-site features. The locations of S&W's explorations should be considered approximate. Table 2, below, describes the drilling method and depth below ground surface for all stages of S&W's subsurface explorations.

Boring		Nearest Structure to Boring	Bottom	
Label	Boring Type	Location		Approximate Elevation, ft MSL
IB-1	Mud Rotary	Aeration Basin	31.5	13
IB-2	Mud Rotary	Blower/electrical	31.5	13
IB-3	Mud Rotary	Primary Gallery	31.5	13
IB-4	Mud Rotary	Fine Screening	46.5	-1
IB-5	Mud Rotary	Fine Screening/UV	30.6	14
IB-6	Mud Rotary	Future Digester	51.5	-6
IB-7	Mud Rotary	Future Digester	51.5	-6
IB-8	Mud Rotary	UV Building	26.5	18
IB-9	Mud Rotary	UV Building	34.2	11
IB-10	Mud Rotary	West of Plant	40.2	10
IB-11	Hollow Stem Auger	West of Plant	46.5	-6
IB-12	Hollow Stem Auger	Retention Basin	31.5	16
IB-13	Hollow Stem Auger	Retention Basin	17	29

## TABLE A1

## **Exploration Hole Details**

Appendix A Doc.doc

CPT-1	Electric Cone Penetrometer	Primary Gallery	27.72	17
CPT-2	Electric Cone Penetrometer	Fine Screening	29.04	16
CPT-3	Electric Cone Penetrometer	Fine Screening	19.69	25
CPT-4	Electric Cone Penetrometer	Primary Gallery	33.14	12

Stage one and stage three subsurface explorations were performed by a drilling subcontractor hired by Shannon and Wilson. The subcontractor was Hardcore Drilling, Inc., of Dundee Oregon. Each of the borings were advanced using a truck-mounted CME-75 drill rig utilizing mud rotary drilling or hollow stem auger techniques. The drilling operations were directed by a representative from Shannon & Wilson who also logged the subsurface conditions during drilling and the logged and classified the soil samples that were collected during the operation. Soil sampling was performed using a standard split spoon sampler, Dames and Moore split spoon sampler and thin-walled Shelby tube sampler. Samples were sealed in containers and returned to our laboratory for further classification and index testing.

Stage One explorations, completed on the dates July 23<sup>rd</sup> through July 26<sup>th</sup>, 2007, consisted of seven mud rotary borings to depths ranging from 30 to 51.5 feet below the ground surface. Five borings, labeled IB-1 through IB-5, were located near of the Phase One Plant Expansion on the south side of the existing WPCP. Two borings, label IB-6 and IB-7, were located near the proposed digesters on the northwest corner of the WPCP site. A standpipe piezometer was installed in IB-6

Stage two explorations consisted of pushing four (CPT-1 through CPT-4) electric cone penetrometer test (CPT) holes on the August 14<sup>th</sup>, 2007. The work was performed by Vandehey Exploration, Inc. of Banks Oregon, who was a subcontractor to S&W. The CPT test holes were pushed to depths between 20 and 33 feet. The CPT probes were advanced to locate the top of the gravel layer near the Fine Screening Building. The CPT probes were stopped where they reached a refusal pushing force. No samples are collected during CPT exploration. The CPT logs provide a continuous record of soil resistance which includes tip resistance and side friction. Estimates of soil properties/classification can be made based on published correlations between tip and skin resistance. The estimated soil properties are based on analyses performed using published correlations and equations. The method used for estimating the properties listed above are:

- a. Uncorrected N-Value (N<sub>60</sub>) based on Robertson & Campanella. This Correlation of CPT data to ASTM International 1586 N-Value is interpretive and should not be considered factual or used as data on this project.
- b. Soil Behavior Type based on University of British Columbia-1983. This correlation is interpretive, and should not be considered the actual soil type according to ASTM D2488.

Some of the logs have no data in the upper five feet of soil because the holes had to be predrilled to advance the CPT through the gravelly fill material.

Stage Three explorations consisted of six borings (IB-8 through IB-13), ranging in depth form 17 to 46.5 feet, and completed during the dates February 25<sup>th</sup> through February 27<sup>th</sup> 2008. Boring IB-8 and IB-9 were drilled near the proposed UV disinfection building and advanced to the top of the dense gravel layer. Borings IB-10 and IB-11 were drilled on the west side of the aid in the characterization of subsurface materials between the plant and the river. Borings IB-12 and IB-13 were drilled near the footprint of the proposed storm water retention basin. Standpipe piezometers were installed in borings IB-12 and IB-13. In-situ infiltration (permeability) tests were performed on boring IB-12 and IB-13, see Appendix C for detailed description of the in-situ testing.

Logs of the current exploration program are contained in this Appendix. For reference, boring logs from previous reports in the plant area are contained in Appendix D.

Shannon & Wilson, Inc. (S&W), uses a soil classification system modified from the Unified Soil Classification System (USCS). Elements of the USCS and other definitions are provided on this and the following page. Soil descriptions are based on visual-manual procedures (ASTM D 2488-93) unless otherwise noted.

#### S&W CLASSIFICATION OF SOIL CONSTITUENTS

MAJOR constituents compose more than 50 percent, by weight, of the soil. Major consituents are capitalized (i.e., SAND).

Modifying (secondary) constituents compose 30 to 45 percent of the soil (i.e. sandy, silty, etc).

Minor constituents compose 12 to 50 percent of the soil and precede the major constituents (i.e., silty SAND). Minor constituents preceded by "slightly" compose 5 to 12 percent of the soil (i.e., slightly silty SAND).

Trace constituents compose 5 percent of the soil (i.e., slightly silty SAND, trace of gravel).

Dual symbols apply to coarse grained soils with 10 percent fines.

#### MOISTURE CONTENT DEFINITIONS

- Dry Absence of moisture, dusty, dry to the touch
- Moist Damp but no visible water
- Wet Visible free water, from below water table

#### ABBREVIATIONS

ATD	At Time of Drilling
Elev.	Elevation
ft	feet
FeO	Iron Oxide
MgO	Magnesium Oxide
HSA	Hollow Stem Auger
ID	Inside Diameter
in	inches
lbs	pounds
Mon.	Monument cover
Ν	Blows for last two 6-inch increments
NA	Not applicable or not available
NP	Non plastic
OD	Outside diameter
OVA	Organic vapor analyzer
PID	Photo-ionization detector
ppm	parts per million
PVC	Polyvinyl Chloride
SS	Split spoon sampler
SPT	Standard penetration test
USC	Unified soil classification
WLI	Water level indicator

#### **GRAIN SIZE DEFINITION**

DESCRIPTION	SIEVE NUMBER AND/OR SIZE
FINES	< #200 (0.08 mm)
SAND* - Fine - Medium - Coarse	#200 to #40 (0.08 to 0.4 mm) #40 to #10 (0.4 to 2 mm) #10 to #4 (2 to 5 mm)
GRAVEL* - Fine - Coarse	#4 to 3/4 inch (5 to 19 mm) 3/4 to 3 inches (19 to 76 mm)
COBBLES	3 to 12 inches (76 to 305 mm)
BOULDERS	> 12 inches (305 mm)

\* Unless otherwise noted, sand and gravel, when present, range from fine to coarse in grain size.

#### **RELATIVE DENSITY / CONSISTENCY**

COARSE-GR	AINED SOILS	FINE-GRAINED SOILS		
N, SPT, RELATIVE BLOWS/FT. <u>DENSITY</u>		N, SPT, <u>BLOWS/FT.</u>	RELATIVE CONSISTENCY	
0 - 4	Very loose	Under 2	Very soft	
4 - 10	Loose	2 - 4	Soft	
10 - 30	Medium dense	4 - 8	Medium stiff	
30 - 50	Dense	8 - 15	Stiff	
Over 50	Very dense	15 - 30	Very stiff	
		Over 30	Hard	

#### WELL AND OTHER SYMBOLS

Bent. Cement Grout	Page Pag Pp Page Pag Pp Page Pag	Surface Cement Seal	
Bentonite Grout		Asphalt or Cap	
Bentonite Chips		Slough	
Silica Sand		Bedrock	
PVC Screen		Fill	
Vibrating Wire			

Tri-City WPCP Phase 1 Expansion Clackamas County, Oregon

## SOIL CLASSIFICATION AND LOG KEY

May 2008

SHANNON & WILSON, INC. Geotechnical and Environmental Consultants

24-1-03420-001 FIG. A1 Sheet 1 of 2

	MAJOR DIVISIONS	5		GRAPHIC MBOL	TYPICAL DESCRIPTION
		Clean Gravel	GW		Well-graded gravel, gravel, gravel/sand mixtures, little or no fines.
COARSE- GRAINED SOIL (more than 50% retained on No. 200 sieve)	Gravel (more than 50%	(less than 5% fines)	GP		Poorly graded gravel, gravel-sand mixtures, little or no fines
	of coarse fraction retained on No. 4 sieve)	Gravel with Fines	GM		Silty gravel, gravel-sand-silt mixtures
		(more than 12% fines)	GC		Clayey gravel, gravel-sand-clay mixtur
	Sand (50% or more of coarse fraction passes the No. 4 sieve)	Clean Sand	SW		Well-graded sand, gravelly sand, little no fines
		(less than 5% fines)	SP		Poorly graded sand, gravelly sand, litt or no fines
		Sand with Fines	SM		Silty sand, sand-silt mixtures
		(more than 12% fines)	SC		Clayey sand, sand-clay mixtures
	Silt and Clay (liquid limit less than 50)	lananain	ML		Inorganic silt of low to medium plastici rock flour, sandy silt, gravelly silt, or clayey silt with slight plasticity
FINE-GRAINED SOIL (50% or more passes the No. 200 sieve)		Inorganic	CL		Inorganic clay of low to medium plasticity, gravelly clay, sandy clay, sil clay
		Organic	OL		Organic silt and organic silty clay of lo plasticity
	Silt and Clay (liquid limit 50 or more)	Inorgania	MH		Inorganic silt, micaceous or diatomaceous fine sand or silty soils, elastic silt
		Inorganic	СН		Inorganic clay or medium to high plasticity
		Organic	ОН		Organic clay of medium to high plasticity, organic silt
HIGHLY- ORGANIC SOIL	Primarily organ color, and	PT	<u><u><u>v</u></u> <u>v</u><u>v</u><u>v</u></u>	Peat, humus, swamp soils with high organic content (see ASTM D 4427)	

NOTE: No. 4 size = 5 mm; No. 200 size = 0.075 mm

NOTES

 Dual symbols (symbols separated by a hyphen, i.e., SP-SM, slightly silty fine SAND) are used for soils with between 5% and 10% fines or when the liquid limit and plasticity index values plot in the CL-ML area of the plasticity chart.

2. Borderline symbols (symbols separated by a slash, i.e., CL/ML, silty CLAY/clayey SILT; GW/SW, sandy GRAVEL/gravelly SAND) indicate that the soil may fall into one of two possible basic groups.

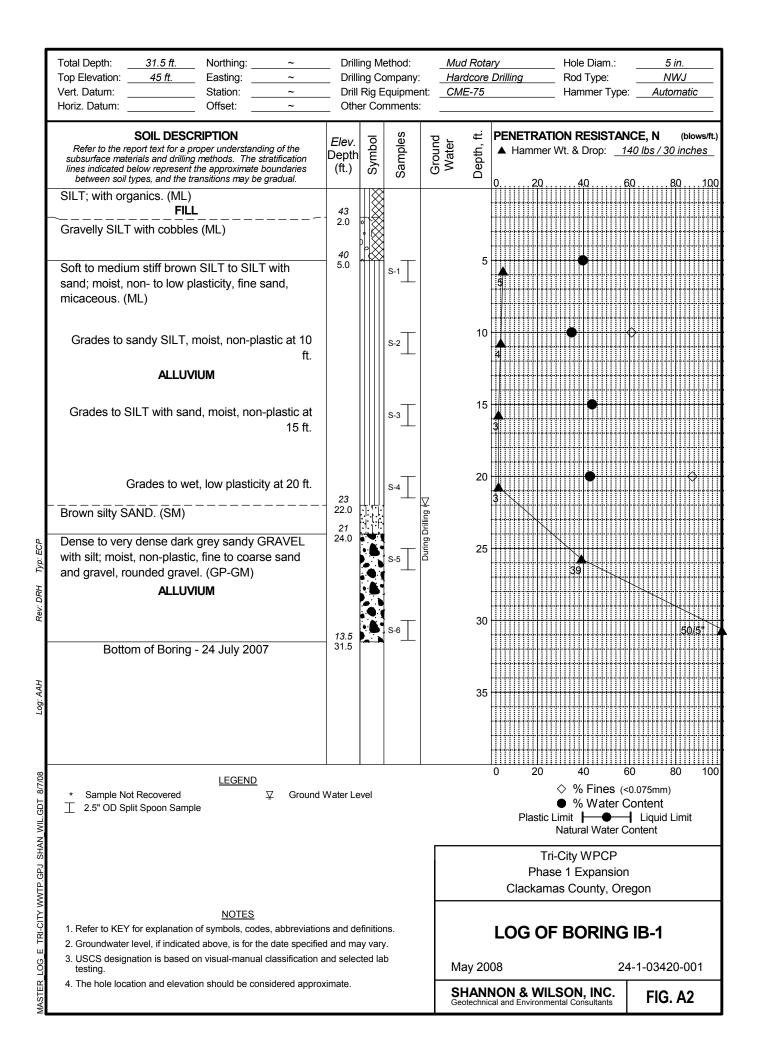
Tri-City WPCP Phase 1 Expansion Clackamas County, Oregon

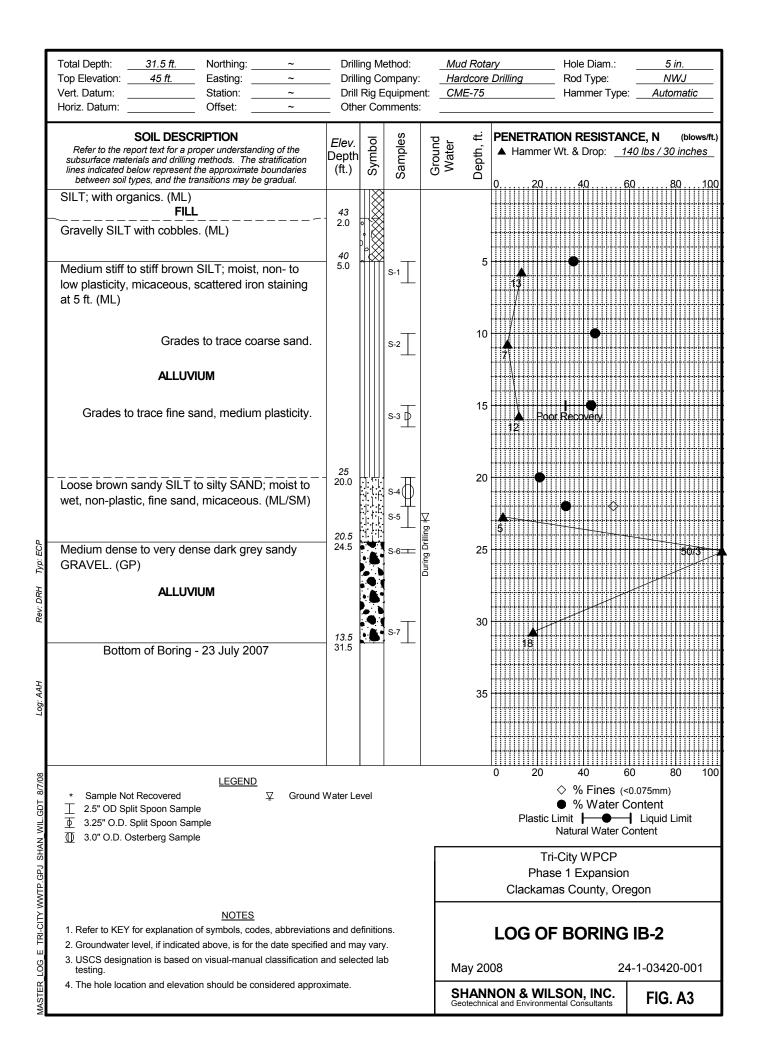
## SOIL CLASSIFICATION AND LOG KEY

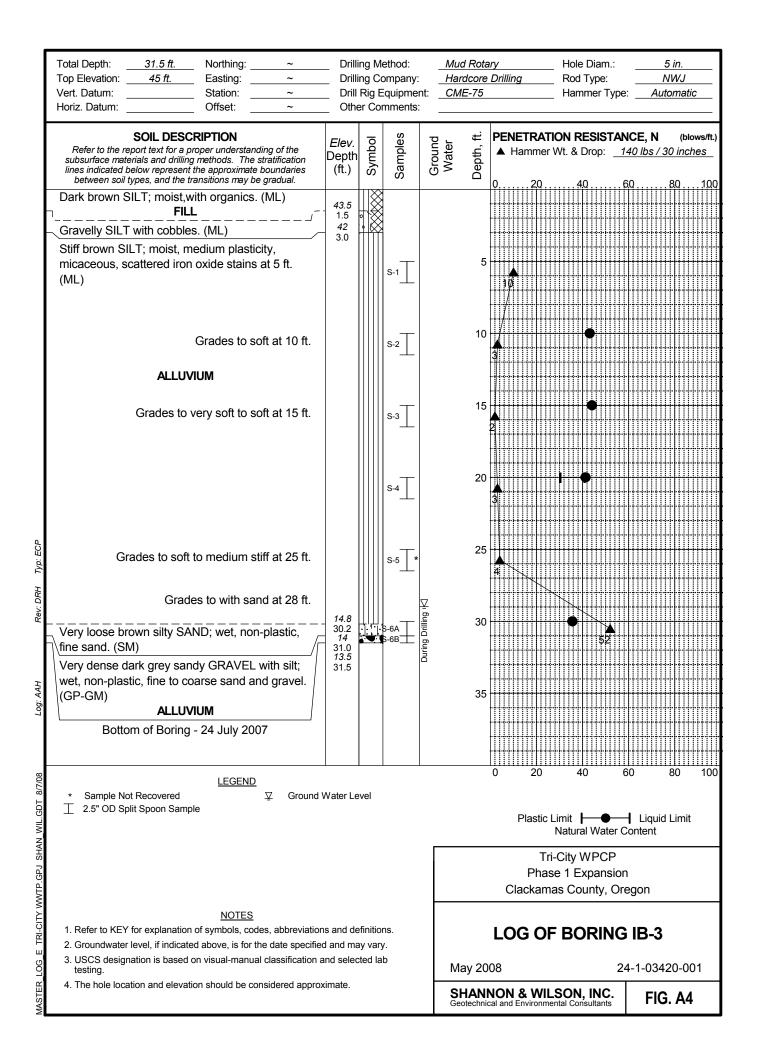
May 2008

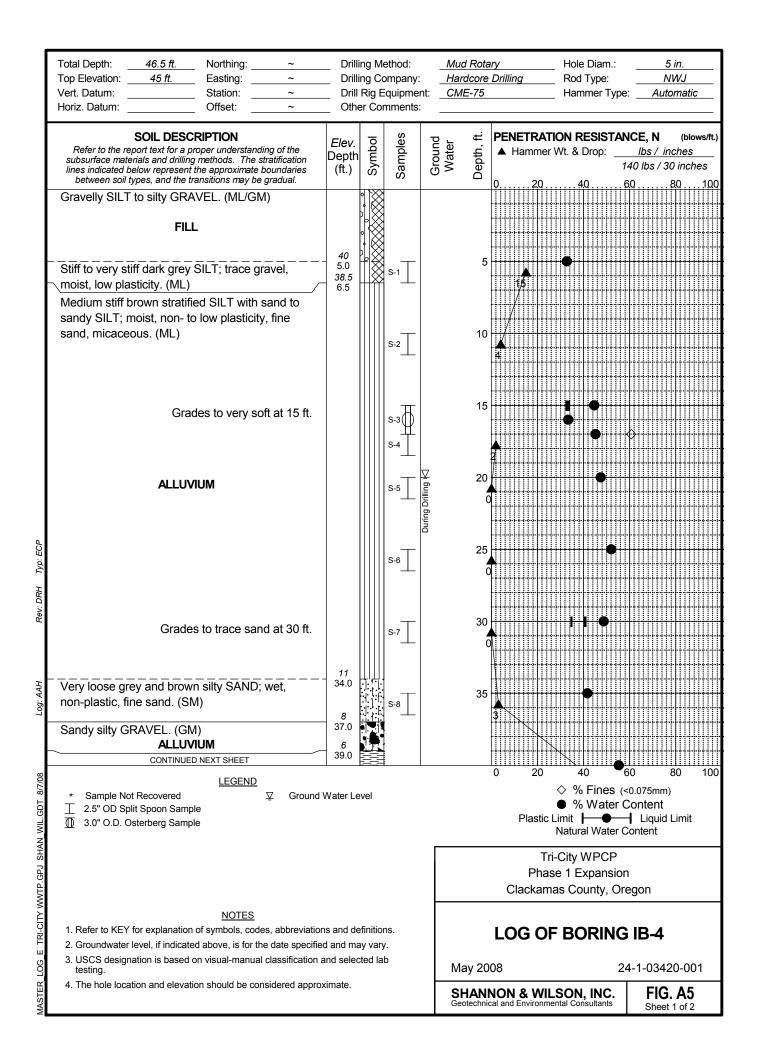
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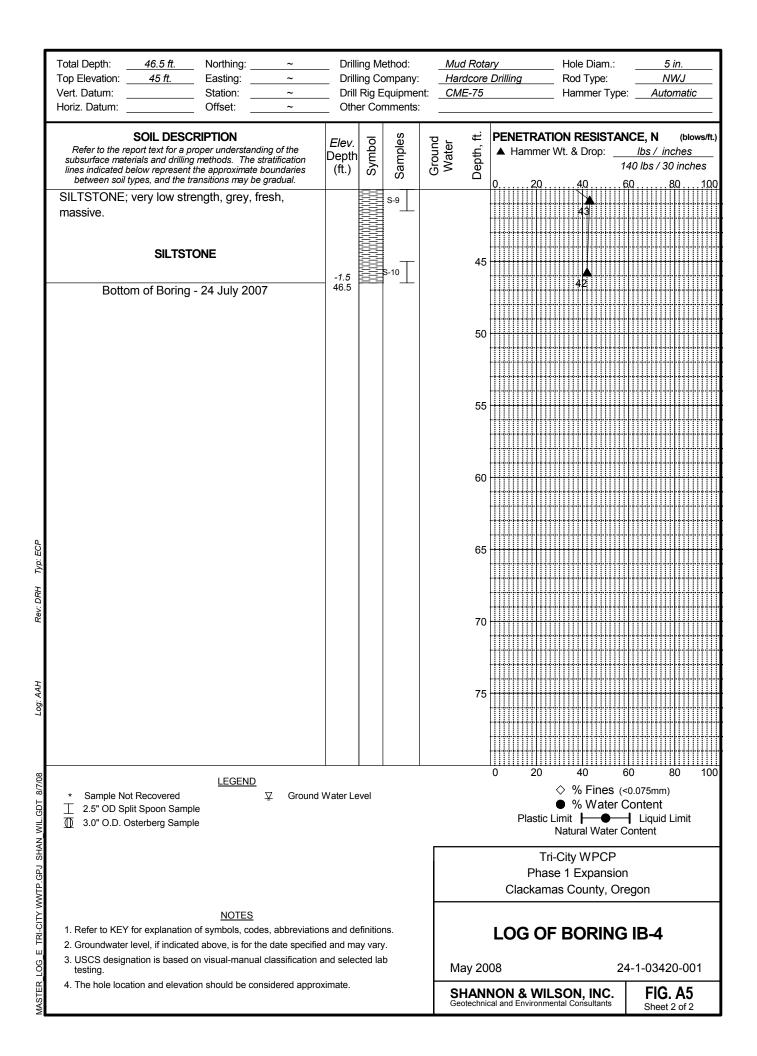
SHANNON & WILSON, INC. Geotechnical and Environmental Consultants FIG. A1 Sheet 2 of 2

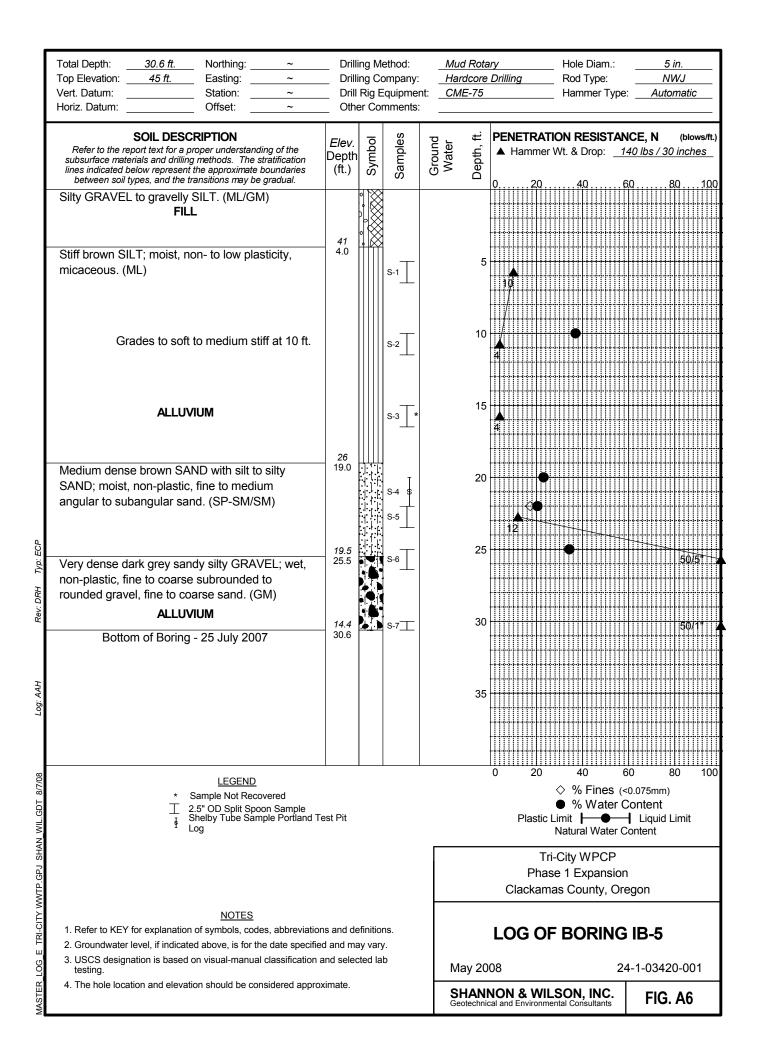


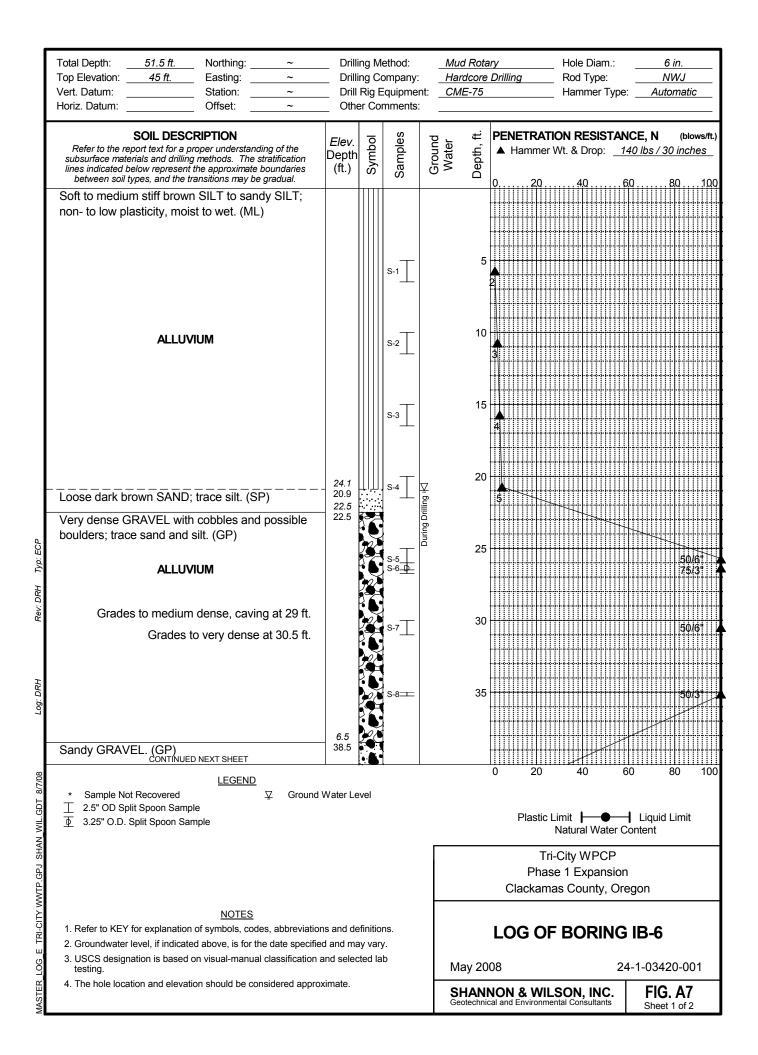


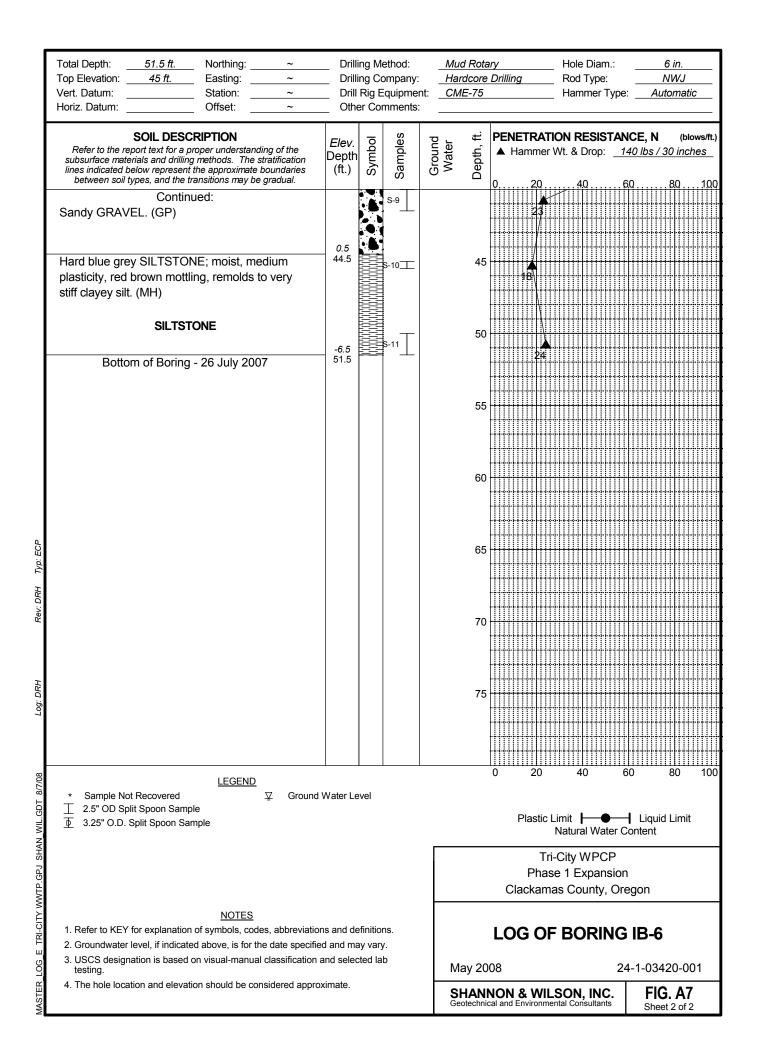




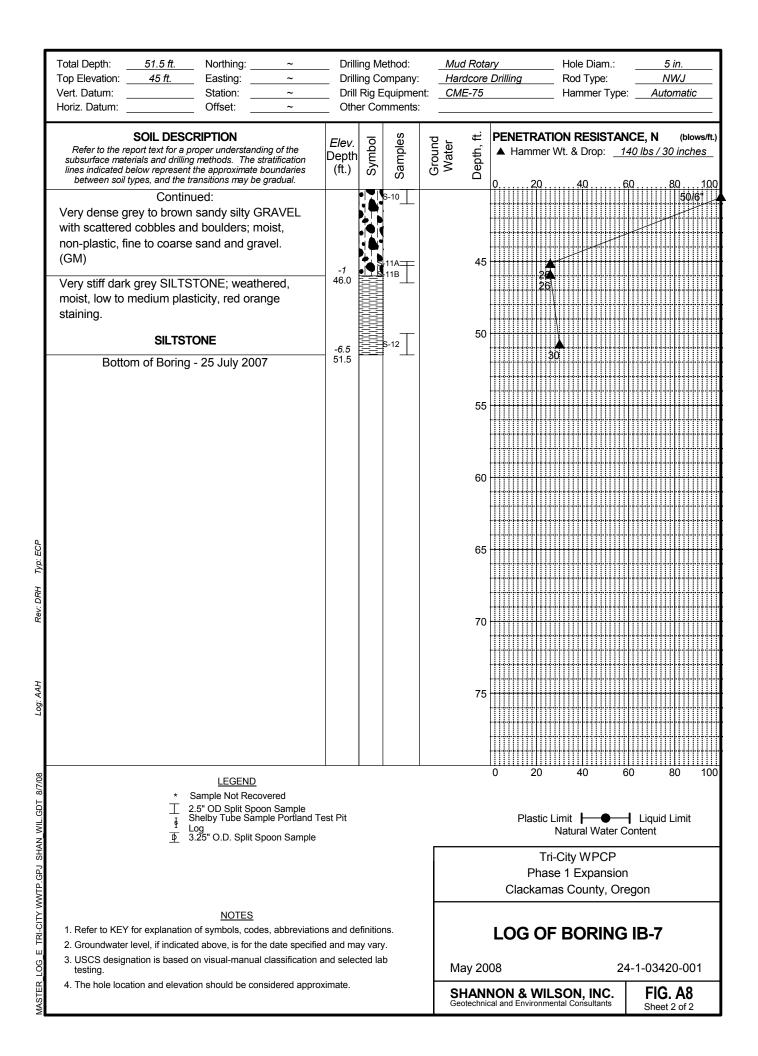




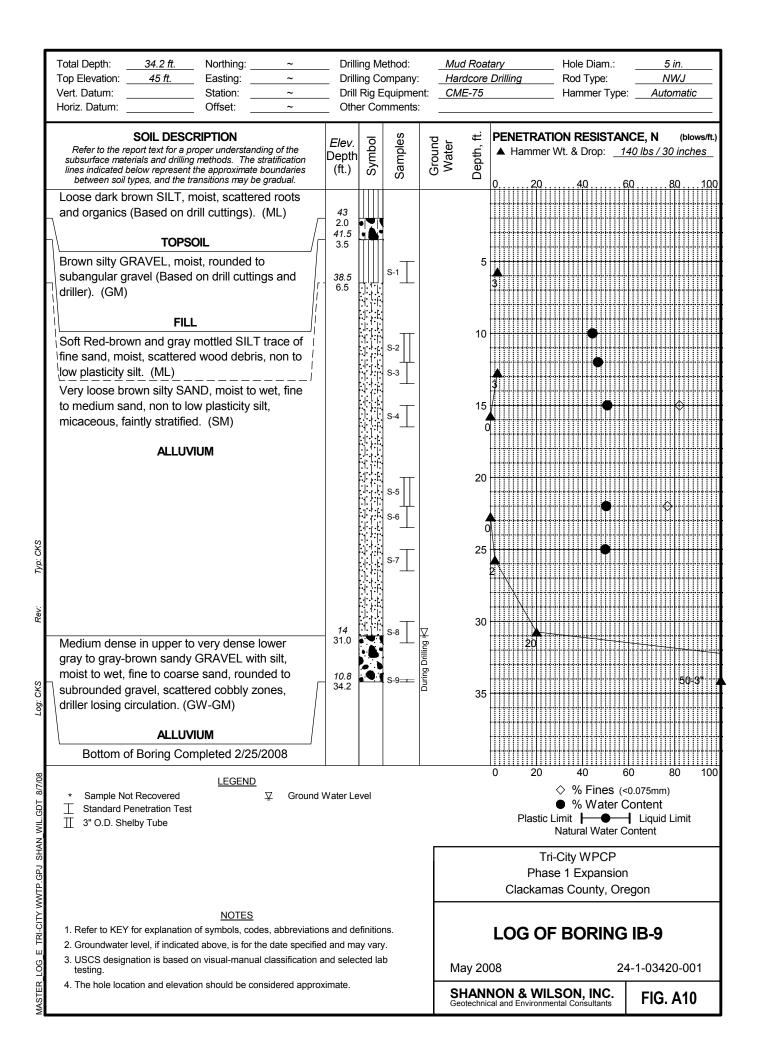


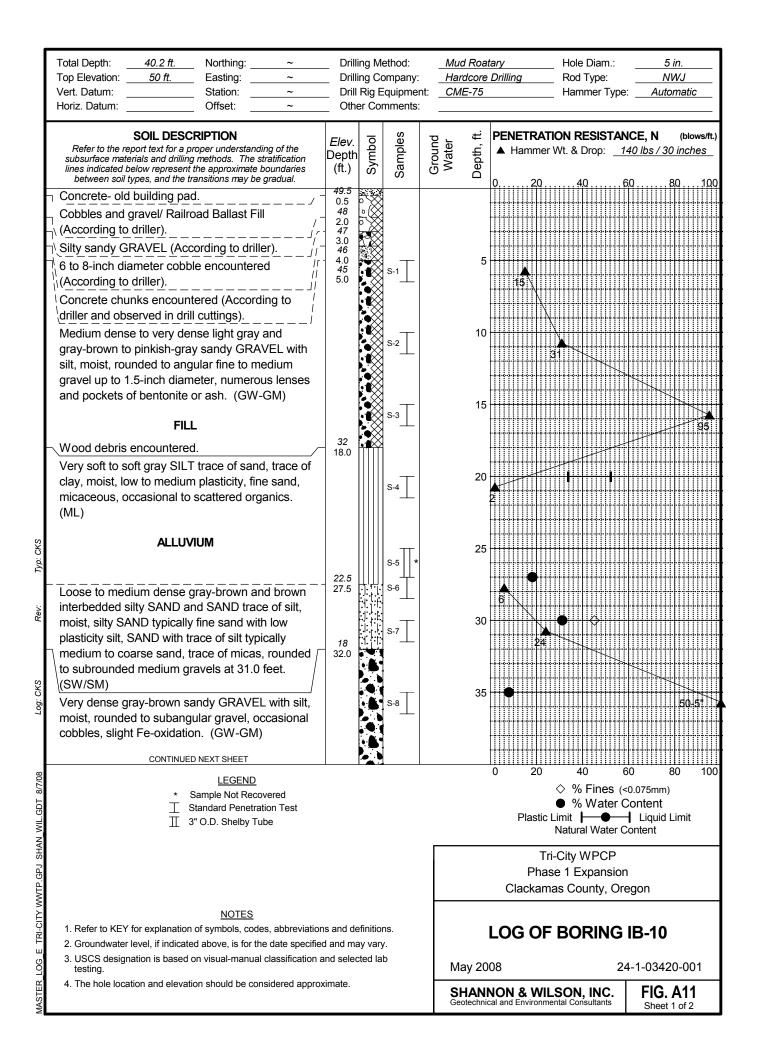


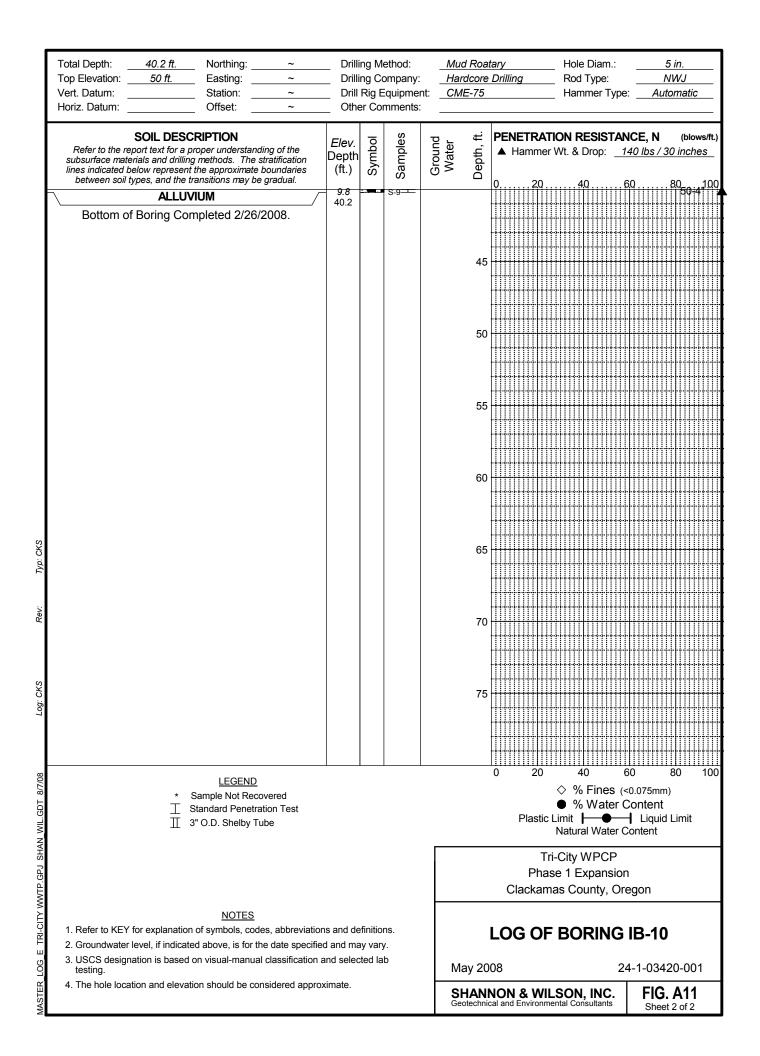
Total Depth: Top Elevation:	51.5 ft. 45 ft.	_ Northing: Easting:	~			lethod: company:		Rota	ary Hole Diam.: <u>5 in.</u> e Drilling Rod Type: NWJ
Vert. Datum:	40 <i>n</i> .	_ Station: Offset:	~ ~	Drill	Rig I	Equipmer	nt: CME		
Refer to the repo subsurface materia lines indicated belo	rt text for a p ls and drillin w represen	the approximate	tratification boundaries	<i>Elev.</i> Depth (ft.)	Symbol	Samples	Ground Water	Depth, ft.	PENETRATION RESISTANCE, N (blows ▲ Hammer Wt. & Drop: <u>140 lbs / 30 inches</u>
Very loose brow moist, non-plast (SM/ML)	n silty SA		SILT;					5	
Medium stiff bro	ALLUV			<u>35</u> 10.0				10	
sand, micaceou		,	.,	30					
Loose to mediu moist, non-plast		-	 ND;	- 30 - 15.0		s-3		15	5 
				21.5		S-4 \$		20	
Very dense grey with scattered c non-plastic, fine (GM)	obbles ar	nd boulders; m	oist,	23.5		S-6 D S-7		25	25 5 5 67 67
	ALLU	/IUM				S-8		30	) 
						S-9 <u> </u>		35	5 
	CONTINUE	D NEXT SHEET			<b>,   (</b>	(			0 20 40 60 80
	Ţ	Sample Not Recc 2.5" OD Split Spo Shelby Tube Sam Log 3.25" O.D. Split S	on Sample ple Portland T	est Pit					Plastic Limit H Liquid Limit Natural Water Content
									Tri-City WPCP Phase 1 Expansion Clackamas County, Oregon
<ol> <li>Refer to KEY for</li> <li>Groundwater lev</li> <li>USCS designati</li> </ol>	el, if indicat	ed above, is for th	e date specifie	ed and ma	ay var	<b>у</b> .	Ma	iy 20	LOG OF BORING IB-7
testing. 4. The hole location	n and eleva	tion should be cor	nsidered appro	ximate.				-	008     24-1-03420-001       INON & WILSON, INC.     FIG. A8       ical and Environmental Consultants     Sheet 1 of 2

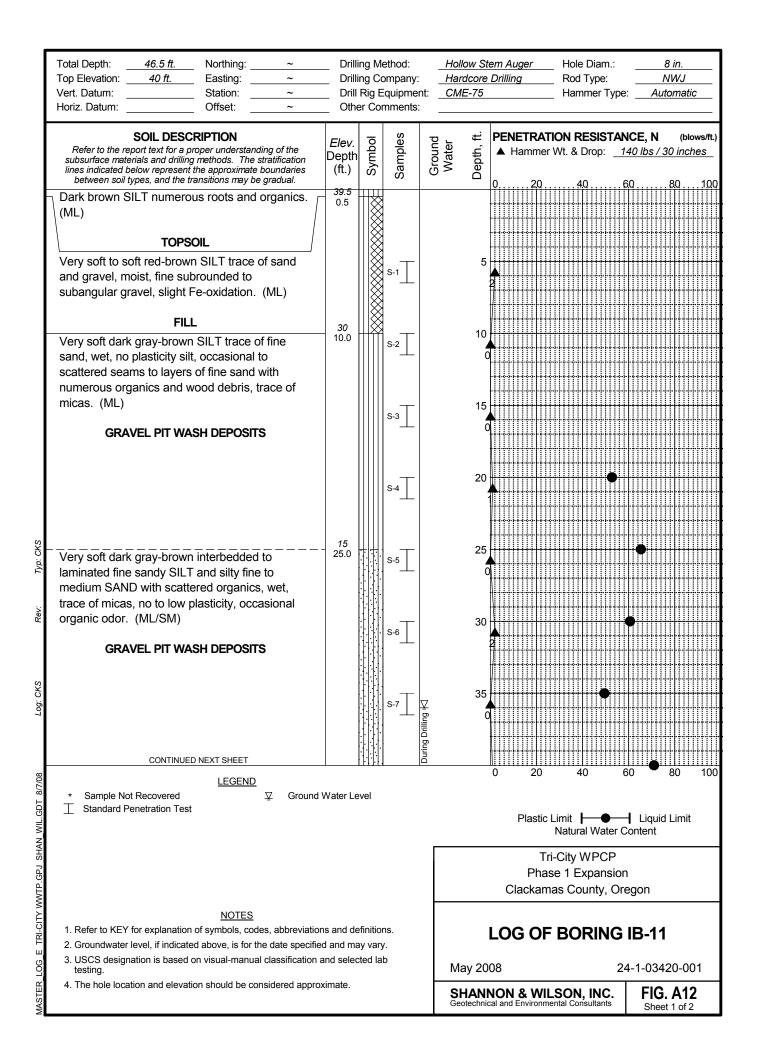


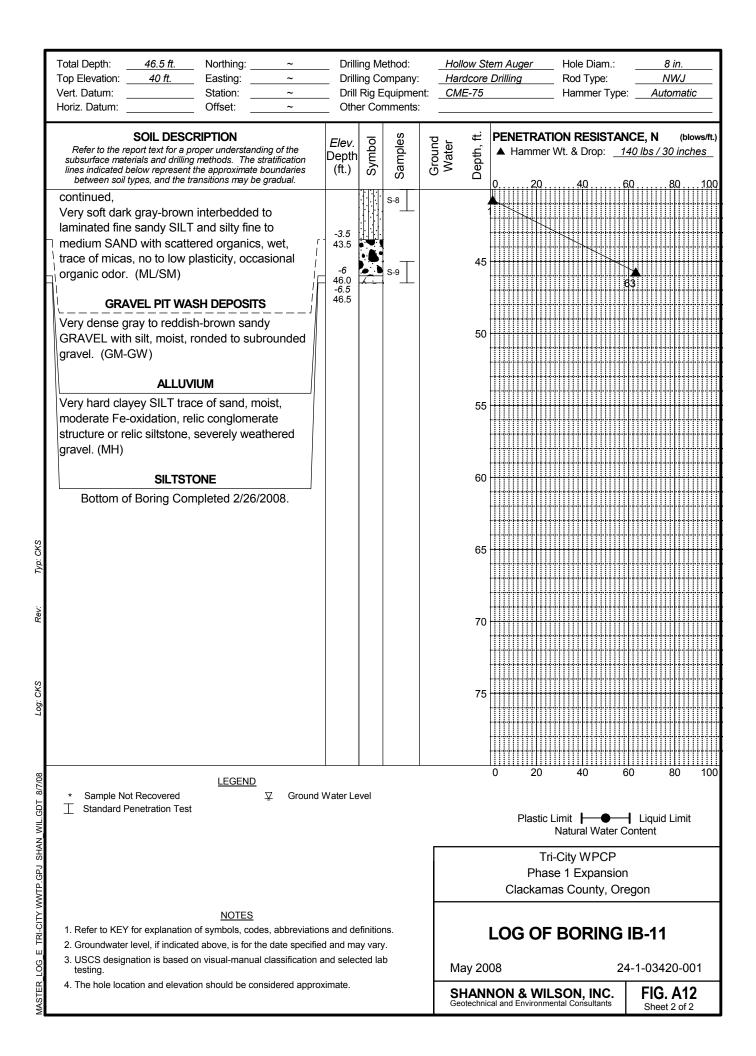
Total Depth:         26.5 ft.         Northing:         ~           Top Elevation:         45 ft.         Easting:         ~           Vert. Datum:         Station:         ~	Dril	ing Co	ethod: ompany: Equipmer	Hard		ary Hole Diam.: <u>5 in.</u> Drilling Rod Type: <u>NWJ</u> Hammer Type: Automatic
Horiz. Datum: Offset: ~	_	-	mments:			
<b>SOIL DESCRIPTION</b> Refer to the report text for a proper understanding of the subsurface materials and drilling methods. The stratification lines indicated below represent the approximate boundaries between soil types, and the transitions may be gradual.	<i>Elev.</i> Depth (ft.)	Symbol	Samples	Ground Water	Depth, ft.	PENETRATION RESISTANCE, N         (blows/ft.)           ▲ Hammer Wt. & Drop: <u>140 lbs / 30 inches</u> 0
Loose dark brown SILT, moist, numerous roots (Based on drill cuttings). (ML)	44 1.0					
TOPSOIL	40.5					
Brown silty GRAVEL, moist, rounded to subangular gravel (Based on drill cuttings). (GM)	4.5		S-1		5	
FILL					10	
Very loose brown silty SAND, moist, fine to medium sand, micaceous, no to low plasticity silt. (SM)	20		S-2		10	
Very soft brown sandy SILT, moist, no plasticity, fine sand. (ML)	30 15.0		S-4		15 0	
ALLUVIUM						
Very loose brown silty SAND, moist, fine to medium sand, micaceous, occasional seams of sandy GRAVEL with traceof silt. (SM)	25 20.0		S-5 S-6		20	
Dense SAND layer approximately 12 inches thick of unknown silt content (According to driller). (SW/SM)	21 24.0 20 25.0 18.5 26.5		s-7		25	90
Very dense gray and brown sandy GRAVELwith silt, moist, rounded to subrounded gravel, slight Fe-oxidation, granitic, quartzitic and basaltic clasts in a sand with silt matrix. (GW-GM)					30	
ALLUVIUM						*****
Bottom of Boring Completed 2/25/2008.					35	
LEGEND         ★       Sample Not Recovered         ⊥       Standard Penetration Test         ⊥       3" O.D. Shelby Tube						0 20 40 60 80 100
					Tri-City WPCP Phase 1 Expansion Clackamas County, Oregon	
NOTES						
<u>NOTES</u> 1. Refer to KEY for explanation of symbols, codes, abbreviation: 2. Groundwater level, if indicated above, is for the date specified	d and m	ay var	<b>/</b> .			LOG OF BORING IB-8
<ol> <li>USCS designation is based on visual-manual classification and selected lab testing.</li> <li>The hole location and elevation should be considered approximate.</li> </ol>				Ma	ay 20	08 24-1-03420-001
				SH	SHANNON & WILSON, INC. Geotechnical and Environmental Consultants FIG. A9	

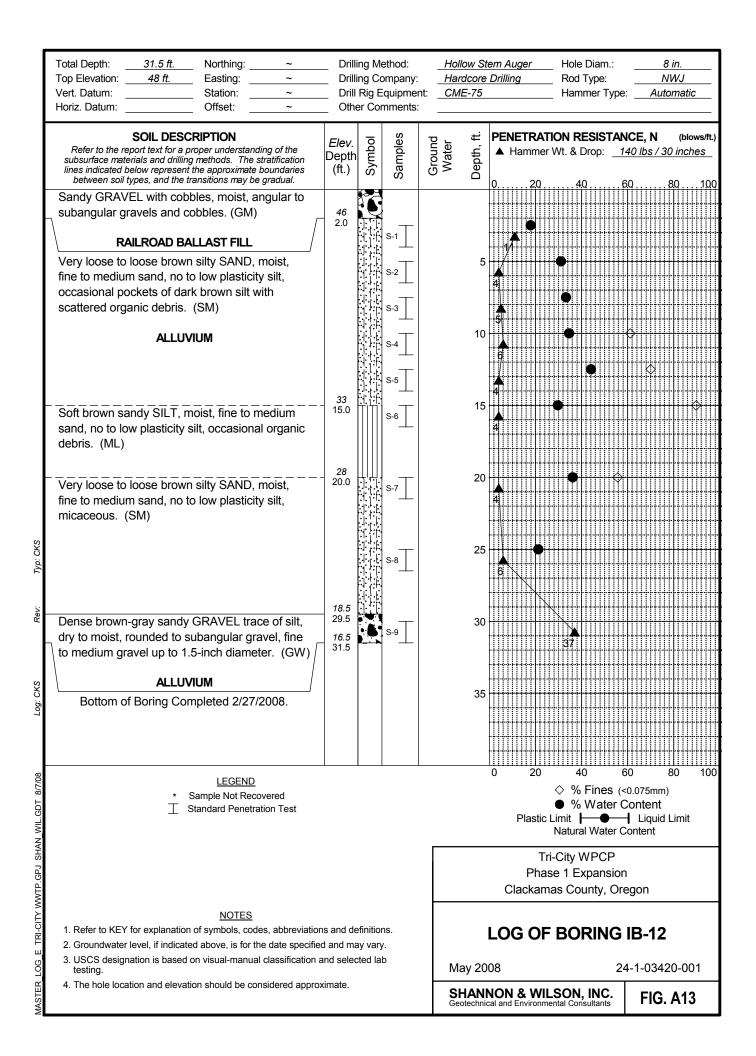


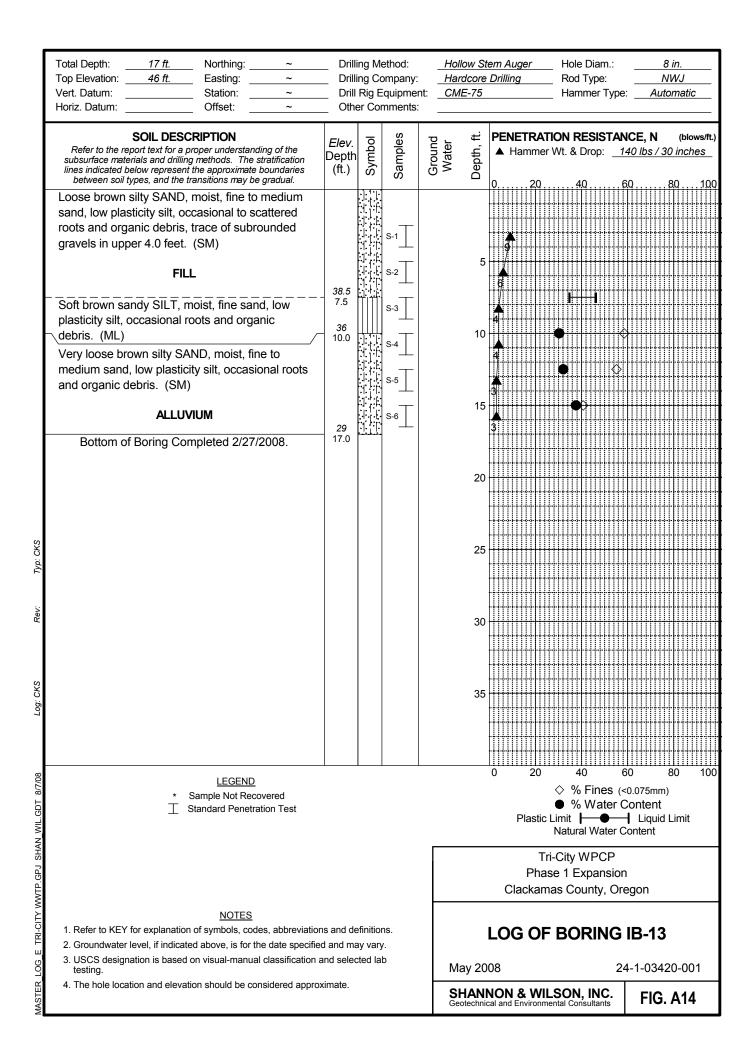


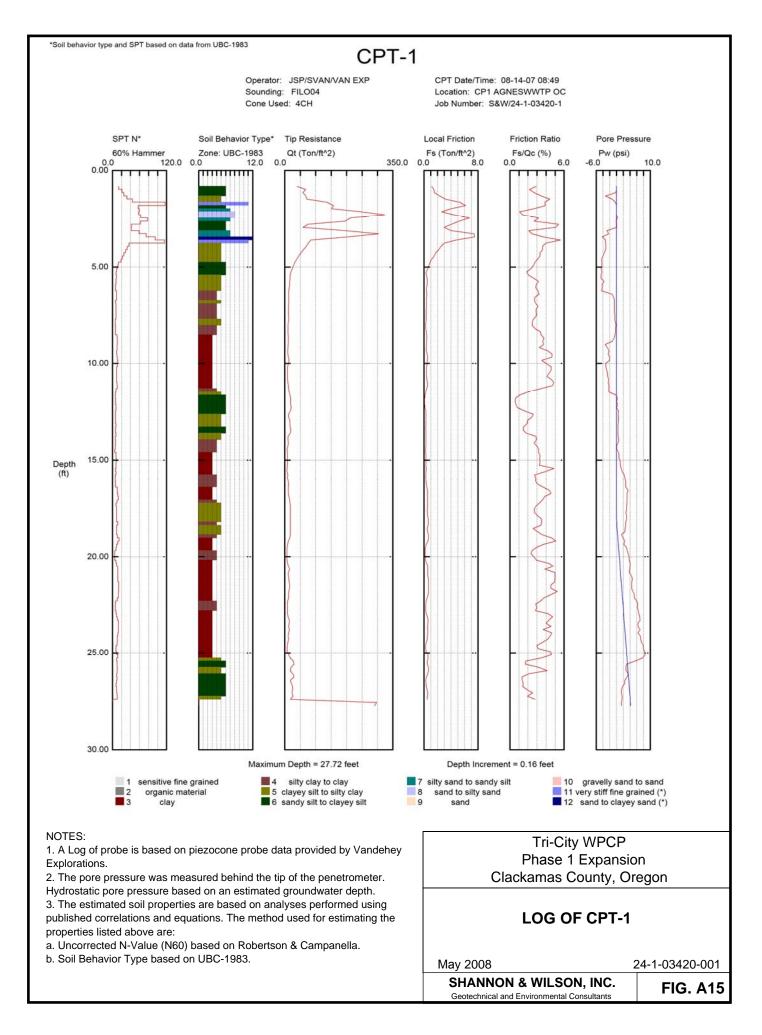


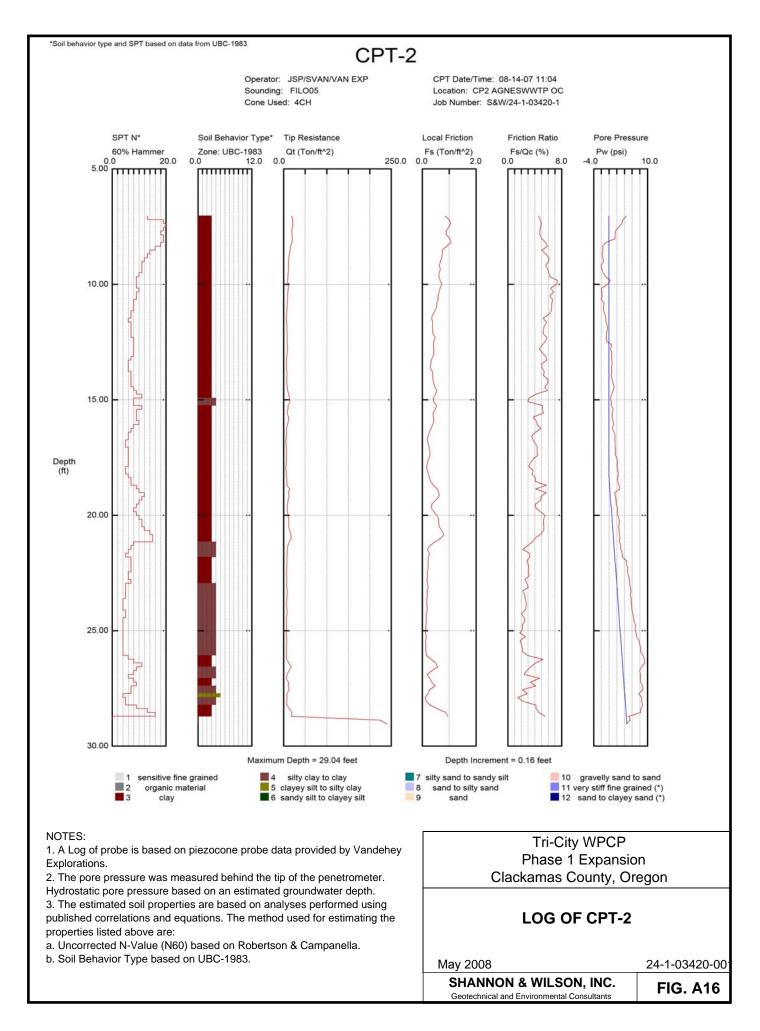


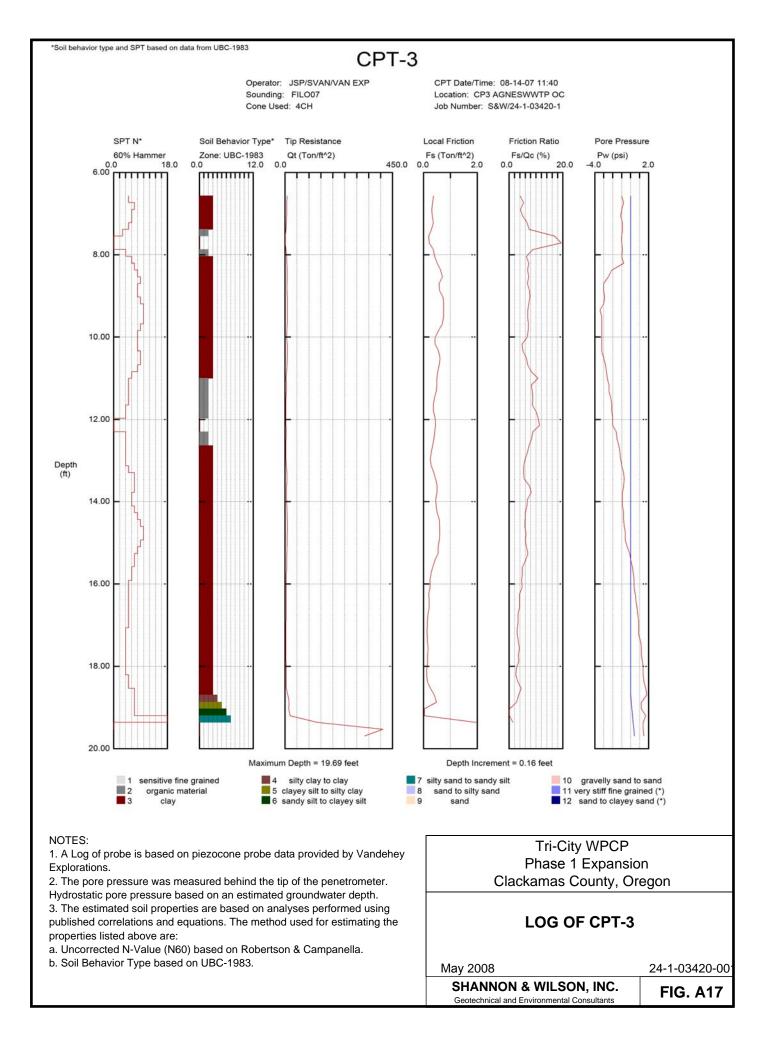


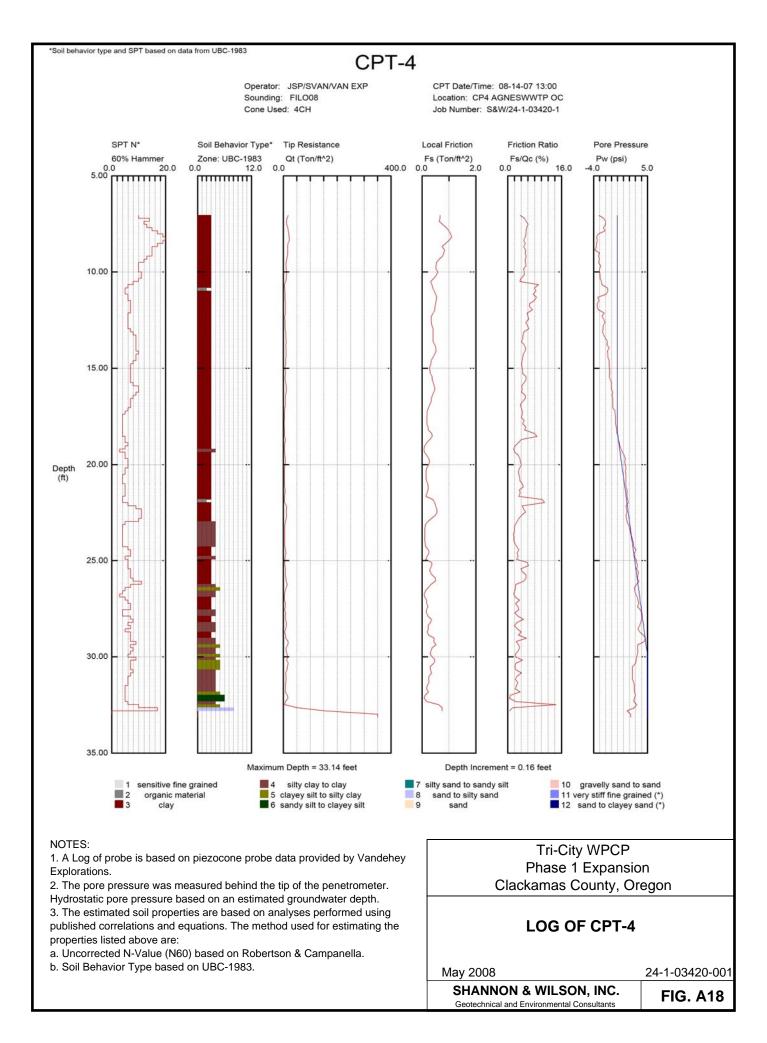












# APPENDIX B S&W LABORATORY TESTING

Appendix B Doc.doc

### APPENDIX B

### S&W LABORATORY TESTING

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- B2 Atterberg Limits
- B3 Grain Size Analysis (Sheets 1 to 3)
- B4 Consolidation Test

#### **APPENDIX B**

#### S&W LABORATORY TESTING

#### **B.1 GENERAL**

A laboratory testing program was developed and implemented in order to evaluate physical and engineering characteristics of the subsurface soils. Laboratory tests on selected soil samples included standard classification tests, which consisted of visual examination, moisture/density tests, Atterberg limits, grain-size analysis, hydrometers, and grain-size wash analysis, i.e., percent finer than the No. 200 sieve. In addition, in-place density tests, in-situ shear strength and unconfined compressive strength tests were conducted on selected undisturbed thin-walled samples. This Appendix contains the full lab results from S&W laboratory testing program, in addition to Figure B1, which summarizes all laboratory testing performed on samples collected on site (this includes the laboratory results from previous work done on-site by others). We cannot assure the completeness or accuracy of the data from other sources, but the information was used by Shannon & Wilson to supplement our interpretation of subsurface conditions and soil properties. The last column of Figure B1 indicates from which previous report the laboratory data was assembled.

#### **B.1.1** Moisture (Natural Water) Content

Selected soil samples were evaluated to determine their in-situ water content. The moisture content is defined as the ratio of the weight of water to the dry weight of soil, expressed as a percentage. The results from our moisture testing are shown on Figure B-1. Additionally, the results of the moisture content determinations are presented on the logs of the borings in Appendix A.

#### **B.1.2** Atterberg Limits

Atterberg Limits were determined on selected samples of fine-grained soils (that is, silts, clays and clayey silts) for the purpose of classifying fine-grained soils into groups based on plastic properties of the soil. Plastic properties of soils are used in a number of soil property correlations. Table 1 below shows the results of the Atterberg Limits tests that were performed by Shannon & Wilson. The results of the Atterberg Limits test are plotted on the plasticity chart on Figure B2 in this appendix.

Appendix B Doc.doc

Boring	Depth, ft	Liquid Limit	Plastic Limit	Plasticity Index	Classification		
IB-2	15	44	32	12	ML		
IB-3	20	41	30	11	ML		
IB-4	15	34	33	1	ML		
IB-4	30	41	35	6	ML		
IB-9	20	NP	NP	NP	ML		
IB-10	20	52	34	18	MH		
IB-13	7.5	45	35	11	ML		

TABLE 1 Atterberg Limits

#### **B.1.3 Grain-Size Analyses**

Grain-size analyses were conducted on selected soil samples to determine their particle size distribution. For most samples, a wet sieve analyses was performed to determine a percentage (by weight) of the sample passing the No. 200 (0.75 mm) sieve. For selected samples, a full grain size distribution curve was developed by testing the minus No. 10 material using a hydrometer, washing the full sample over a No. 200 sieve, and sieving the plus No. 200 material through a series of sieves to determine the distribution of the plus No. 200 material. The hydrometer plus sieving results were used to develop the particle-size distribution curves down to 0.002 mm. Table 2 below shows the tabular results of S&W grain size analysis. Figure B3 in this appendix presents the results of the Grain-Size Analysis.

Boring	Depth, ft	Percent Gravel	Percent Sand	Percent Fines	Classification	
IB-1	10			60.8	ML	
IB-1	20			87.2	ML	
IB-2	22	0.0	52.2	47.8	SM	
IB-4	17			60.7	ML	
IB-4	35			42.0	SM	
IB-5	22	0.0	43.2	56.8	ML	
IB-8	5			83.8	ML	
IB-9	15	0.0	17.9	82.1	ML	
IB-9	22			76.8	ML	
IB-10	30			45.2	SM	
IB-12	10			61.1	ML	
IB-12	12.5		70.0		ML	

TABLE 2 Grain-Size Analysis

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IB-12	15	0	10.3	89.7	
IB-12	20			55.6	ML
IB-13	10			58.4	ML
IB-13	12.5	0	44.9	32.0	
IB-13	15			40.6	SM

#### **B.1.4 Unit Weight of Undisturbed Samples**

The unit weights, or densities, from the thin-walled Shelby tube samples were determined in the laboratory. Results from S&W testing are below in Table 3. The results from all Unit weight measurements performed on-site are presented in this appendix.

Boring	Depth, ft	Dry Density pcf					
IB-2	20	73.87					
IB-4	15	84.37					
IB-5	20	95.56					
IB-8	20	91.0					
IB-9	10	83.3					

TABLE 3Unit Weight of Undisturbed Samples

### **B.1.5** Consolidation Test

Shannon & Wilson performed one consolidation test on a sample from the Alluvial Silts at a depth of 20 ft, in the vicinity of the UV disinfection building. A consolidation test indicates the amount of deformation that a soil may undergo when subjected to a certain load. The consolidation test indicated that the soils at under the UV building have exhibit compressive characteristics as shown on Figure B4, in this appendix. The results from all consolidation tests performed on-site are presented on Figure B1, with the full lab results presented in Appendix D.

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#### FIGURE B1 - LAB TESTING SUMMARY

			SPT			epth (ft)				Water			imits		ain Size Di			Unit We	ight (pcf)		t Shear	Laboratory
Boring	Sample Number	Sample Type	N-value	Тор	Bottom	Rec. (ft)	Geologic Unit	USCS	Classification		L.L	P.L.	P.I.	Gravel (%)	Sand (%)	Fines (%)	C <sub>C</sub> C <sub>U</sub>	Wet	Dry	C' (psf)	φ (deg)	
B-101	SS-1	SPT	23	2.5	4		SILT	ML		30.0												CH <sub>2</sub> M
B-101	SS-8	SPT	7	27.5	29		SILT	ML		45.0	42	31	11									CH2M
B-102	SS-3	SPT	11	10	11.5		SILT	ML		42.0												CH2M
B-102	SO-6	Shelby	N/A	22.5	24.5		SILT	ML		43.0	48	32	26					110	77			CH2M
B-102 B-102	SS-7 SS-10	SPT SPT	9 27	24.5 30.5	26 32		SILT Silty SAND	ML SM		45.0						19.0						CH2M CH2M
B-102 B-103	SS-4	SPT	2	15	16.5		SILT	ML		50.0	44	31	14			19.0						CH2N CH2N
B-103	SS-6	SPT	4	22.5	24		SILT	ML		46.0	44	51	14									CH2M
B-103	SS-8	SPT	15	27	28.5		Silty SAND	SM		1010						29.0						CH2N
B-103	SS-11	SPT	35	36	37.5		Silty GRAVEL	GM								6.0						CH2N
B-104	SS-1	SPT	54-11"	5	5.92		SILT	ML		34.0												CH2N
B-104	SS-4	SPT	9	26	27.5		Silty SAND	SM		37.0						47.0						CH2N
B-105	SS-1	SPT	19	5	6.5		SILT	ML		32.0												CH2N
B-105	<u>SS-4</u>	SPT	6	15	16.5		SILT	ML		35.0	10		0									CH2N
B-105 B-106	SS-7 SO-6	SPT Shelby	6 N/A	25	26.5 24.5		SILT SILT	ML		47.0 47.0	42	36 38	6 9					104	70.8			CH2M CH2M
B-106 B-106	SS-8	SPT	12	23 27.5	24.5		Silty SAND	SM		47.0	47	30	9			35.0		104	70.0			CH2N CH2N
B-6	SS-3	SPT	7	15	16.5		Silty SAND	SM								43.0	2 28					CH2N
B-7	ST-3	Shelby	N/A	15	16.5		SILT	ML									0			200	32.3	CH2N
B-15	SS-5	SPT	5	15	16.5		SILT	ML			NP	41	NP									CH2N
B-16	ST-4	Shelby	N/A	10	12		Sandy SILT	ML		52.0	NP	50	NP			82.0	3 21	102	67			CH2N
B-17	SS-1	SPT	4	5	6.5		SILT	MH		81.0	51	35	16									CH2N
B-17	ST-3	Shelby	N/A	13	15		SILT	ML		54.0					6.0	94.0	5 33	107	69.4			CH2N
B-18	ST-4	Shelby	N/A	10	12		Silty SAND	SM		30.0	NP	NP	NP		53.0	47.0	1 25			0	35.5	CH2N
B-17	ST-3	Shelby	N/A	13	15		SILT	ML		54.0					2.0	98.0	2 6	405	<u> </u>			CH2N
B-17 IB-1	ST-7 S-1	Shelby SPT	N/A 5	23 5	25 6.5		Sandy SILT SILT	ML ML		52.0 39.7					32.0	68.0	2 10	105	69		4	CH2N Shannon
IB-1	S-1 S-2	SPT	4	10	11.5		Sandy SILT	ML		34.8						60.8						Shannon
IB-1	S-3	SPT	3	15	16.5		Sandy SILT	ML		43.7						00.0						Shannon
IB-1	S-4	SPT	3	20	21.5		Sandy SILT	ML		42.8						87.2						Shannon
IB-1	S-5	SPT	39	25	26.5		Sandy GRAVEL	GM/GP														Shannon
IB-2	S-1	SPT	13	5	6.5		SILT	ML		35.6												Shannon
IB-2	S-2	SPT	7	10	11.5		SILT	ML		45.0												Shannon
IB-2	S-3	SPT	12	15	16.5		SILT	ML		43.3	44	32	12									Shannon
IB-2	S-4	Shelby	N/A	20	22		Silty SAND	SM		21.0					50.0	47.0		89.35	73.87			Shannon
IB-2	S-5 S-6	SPT SPT	5 100	22 25	23.5 25.25		Silty SAND Sandy GRAVEL	SM GP		32.3					52.2	47.8						Shannon
IB-2 IB-3	S-6	SPT	3	10	11.5		Sandy GRAVEL	ML		43.1												Shannon Shannon
IB-3	S-3	SPT	2	15	16.5		SILT	ML		44.1												Shannon
IB-3	S-4	SPT	3	20	21.5		SILT	ML		41.3	41	30	11									Shannon
IB-3	S-5	SPT	4	25	26.5		SILT	ML														Shannon
IB-3	S-6A	SPT	52	30	31		Silty SAND	SM		35.6												Shannon
IB-4	S-1	SPT	15	5	6.5		SILT	ML		32.7												Shannon
IB-4	S-3	Shelby	N/A	15	17		Sandy SILT	ML		33.3	34	33	1					112.5	84.37			Shannon
IB-4	S-4	SPT	2	17	18.5		Sandy SILT	ML		45.2						60.7						Shannon
IB-4	S-5	SPT	0	20	21.5		SILT	ML		47.4												Shannon
IB-4 IB-4	S-6 S-7	SPT SPT	0	25 30	26.5 31.5		SILT SILT	ML		52.0 48.8	41	35	6									Shannon Shannon
IB-4	S-8	SPT	3	35	36.5		Silty SAND	SM		41.6	41	55	0			42.0						Shannon
IB-4	S-0	SPT	43	40	41.5		SILTSTONE	SILTST.		55.3						12.0						Shannon
IB-5	S-2	SPT	4	10	11.5		SILT	ML		36.9												Shannon
IB-5	S-4	Shelby	N/A	20	22		Silty SAND	SM		23.0								117.6	95.56			Shannon
IB-5	S-5	SPT	12	22	23.5		Silty SAND	SM		20.4					43.2	56.8						Shannon
IB-5	<u>S-6</u>	SPT	100	25	26.4		Silty Sandy GRAVEL	GM		34.3						00.0						Shannon
IB-8	S-1	SPT	3	5	6.5					46.4						83.8						Shannon
IB-8 IB-8	<mark>S-2</mark> S-3	Shelby SPT	N/A 4	10 12	12 13.5					37.7												Shannon Shannon
IB-8	S-3 S-4	SPT	4	12	16.5					40.1												Shannon
IB-8	S-5	Shelby	N/A	20	22					31.2								119.4	91			Shannon
IB-8	S-6	SPT	4	22	23.5					38.8								. 10. 7				Shannon
IB-9	S-2	Shelby	N/A	10	12					44.3								120.2	83.3			Shannon
IB-9	S-3	SPT	3	12	13.5					46.6												Shannon
IB-9	S-4	SPT	0	15	16.5					50.7				0.0	17.9	82.1						Shannon
IB-9	S-5	Shelby	N/A	20	22						NP	NP	NP									Shannon
IB-9	S-6	SPT	0	22	23.5					50.2						76.8						Shannon
IB-9	<u>S-7</u>	SPT	2	25	26.5					49.8			10									Shannon
IB-10	S-4	SPT	2	20	21.5					40.0	52	34	18									Shannon
IB-10 IB-10	<mark>S-6</mark> S-7	SPT SPT	6 24	27 30	28.5 31.5					18.2 31.2						45.2						Shannon Shannon
										31.2 8.0						40.2						Shannon
	S-8	SPI	100	35	36.5																	
IB-10 IB-10 IB-11	<mark>S-8</mark> S-4	SPT SPT	100 1	35 20	36.5 21.5					52.7												Shannon

#### Tri-City WPCP Interim Expansion 24-1-03420-001

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# SHANNON & WILSON, INC.

#### FIGURE B1 - LAB TESTING SUMMARY

			SPT	Sa	ample De	epth (ft)				Water	Atte	erberg	Limits		ain Size Di			eight (pcf)		Shear	Laboratory Data Source,
Boring	Sample Number	Sample Type	N-value	Тор	Bottom	Rec. (ft)	Geologic Unit	USCS	Classification		L.L	. P.L	P.I.	Gravel (%)	Sand (%)	Fines (%) C <sub>C</sub> C <sub>U</sub>	Wet	Dry	C' (psf)	φ (deg)	Date
IB-11	S-6	SPT	2	30	31.5					60.6											Shannon & Wilson, 2008
IB-11	S-7	SPT	0	35	36.5					49.5											Shannon & Wilson, 2008
IB-11	S-8	SPT	1	40	41.5					71.0	_										Shannon & Wilson, 2008
IB-12	S-1	SPT	11	2.5	4					17.9											Shannon & Wilson, 2008
IB-12	S-2	SPT	4	5	6.5					31.0											Shannon & Wilson, 2008
IB-12	S-3	SPT	5	7.5	9					33.2											Shannon & Wilson, 2008
IB-12	S-4	SPT	6	10	11.5					34.6						61.1					Shannon & Wilson, 2008
IB-12	S-5	SPT	4	12.5	14					44.1						70.0					Shannon & Wilson, 2008
IB-12	S-6	SPT	4	15	16.5									0.0	10.3	89.7					Shannon & Wilson, 2008
IB-12	S-7	SPT	4	20	21.5					36.1						55.6					Shannon & Wilson, 2008
IB-12	S-8	SPT	6	25	26.5					21.2	_										Shannon & Wilson, 2008
IB-13	S-3	SPT	4	7.5	9						45	35	11								Shannon & Wilson, 2008
IB-13	S-4	SPT	4	10	11.5					30.3						58.4					Shannon & Wilson, 2008
IB-13	S-5	SPT	3	12.5	14									0.0	44.9	32.0					Shannon & Wilson, 2008
IB-13	S-6	SPT	3	15	16.5					37.5						40.6					Shannon & Wilson, 2008

 $^{\ast}\mbox{Split}$  Sample, if two water contents were taken, the higher was reported.

Tri-City WPCP Interim Expansion 24-1-03420-001

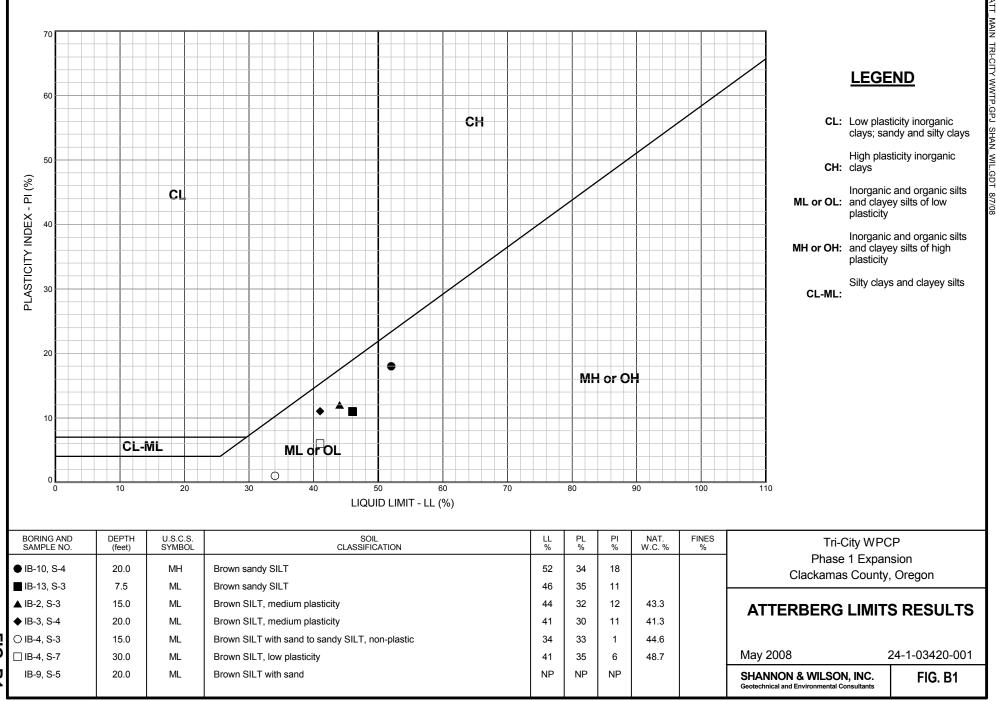
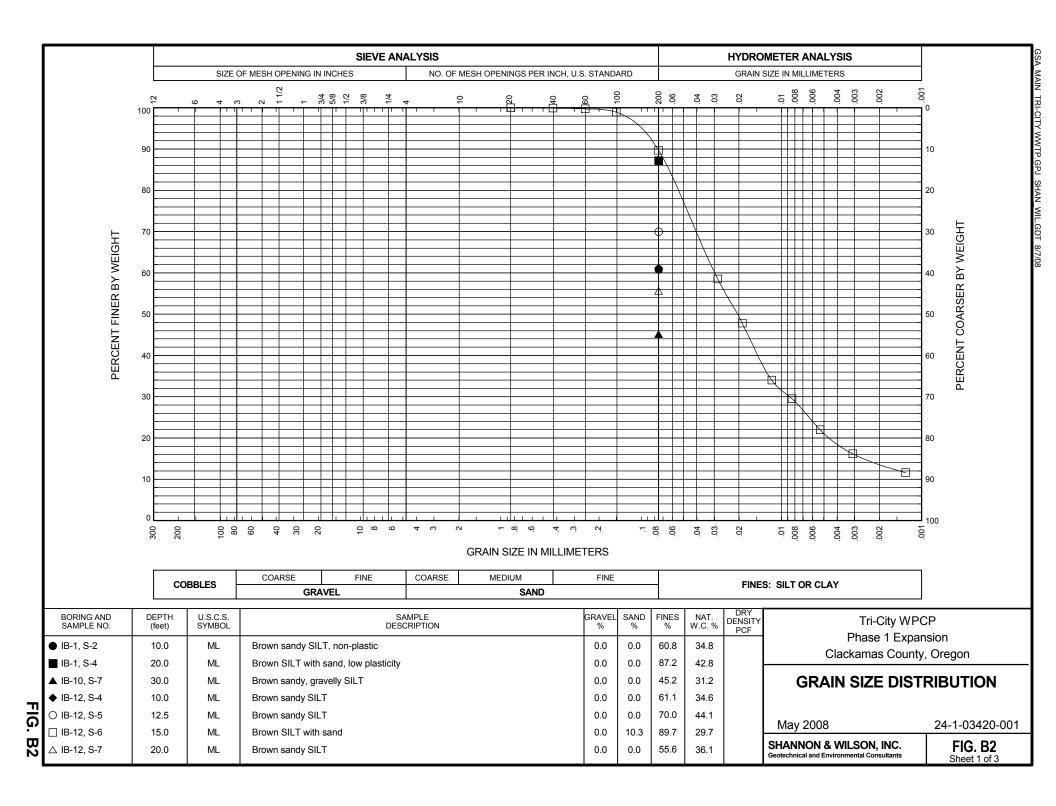
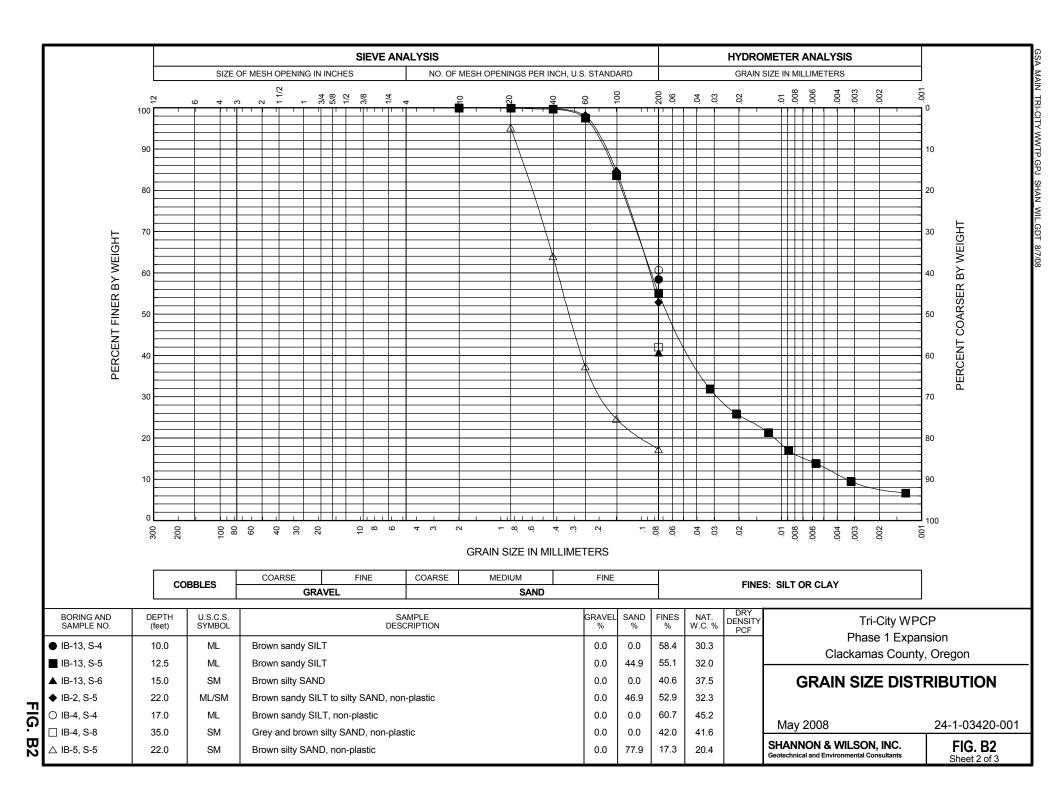
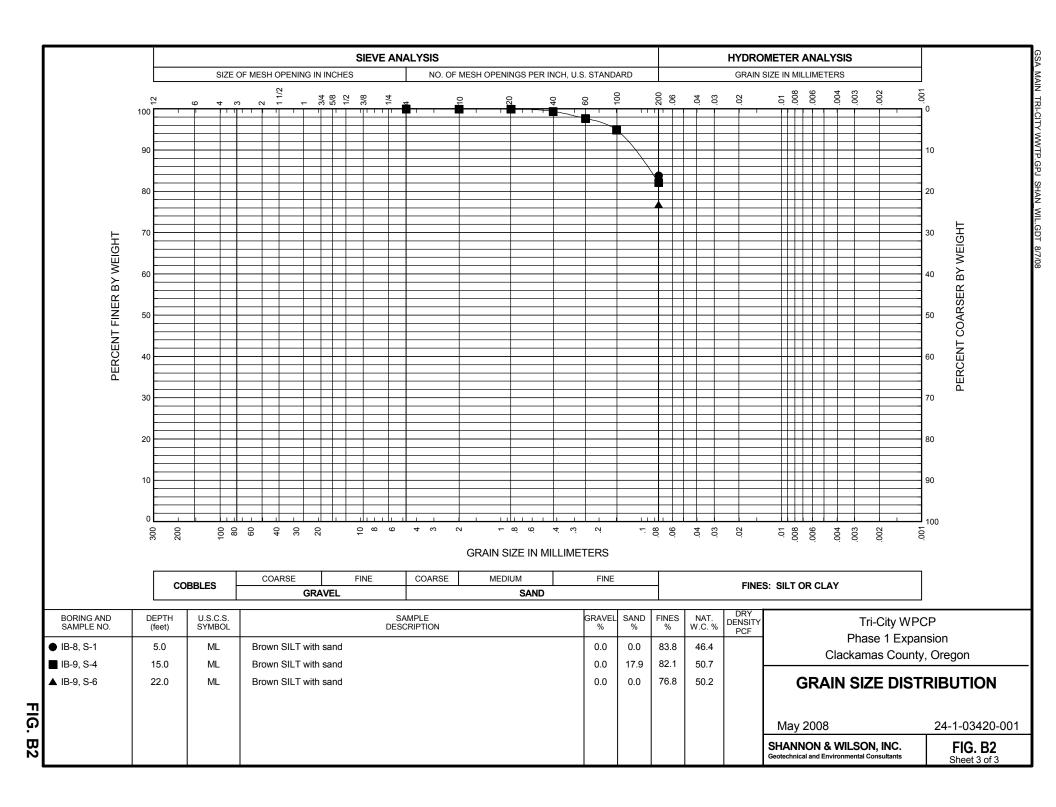
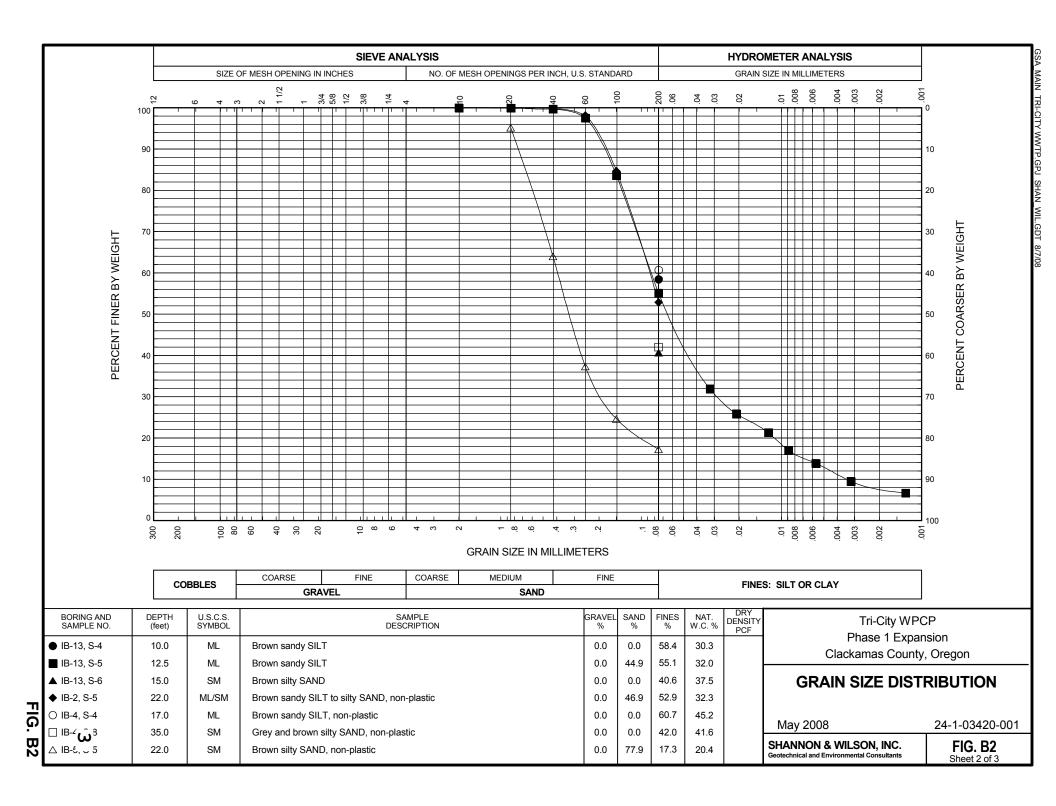


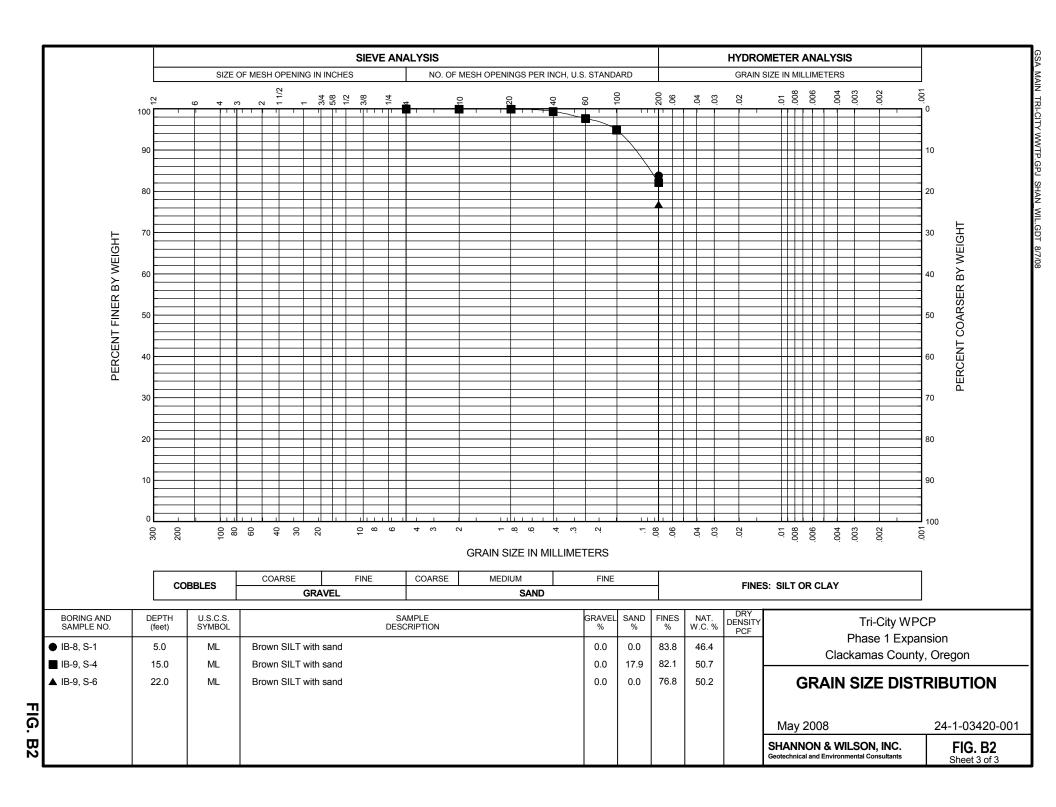
FIG. ω











### APPENDIX C

# S&W IN-SITU TESTING

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B.2	FALLING HEAD TEST	.1
B.3	REFERENCE	2

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C1 Falling Head Test Results

# LIST OF FIGURES

# Figure No.

C1	Falling Head Tests Observation Well IB-12
$C^{2}$	Folling Hood Taste Observation Wall IP 12

C2 Falling Head Tests Observation Well IB-13

### **APPENDIX C**

### **S&W IN-SITU TESTING**

### **B.1 GENERAL**

We conducted falling head permeability tests in observation wells IB-12 and IB-13 in order to estimate the hydraulic conductivity of the formation in the proposed storm-water retention basin. The observation wells are each 15 feet deep and screened in the bottom 5 feet. The locations of these observation wells are shown on the Plan of Explorations, Figure 2. The soil logs of the observation well borings are presented in Appendix A, Figures A13 and A14.

### **B.2 FALLING HEAD TEST**

Prior to testing, we saturated the soil in the test area by continuously filling the wells to the ground surface with potable water for more than 4 hours. We then performed two falling head permeability tests in each well. For each test:

- An acrylic plastic extension was temporarily affixed to the top of the standpipe.
- A Solinst Levelogger Gold Model 3001 electronic datalogging pressure transducer was placed in the bottom of the observation well.
- The well and acrylic plastic extension was filled with potable water to a level equivalent with a volume of seven liters over the top of the standpipe.
- The datalogger was set to record the water level in the well at 1 second intervals and all artificial flow to the well was stopped.
- The water level in the well was allowed to fall to less than 0.2 feet while the datalogger was recording.

The recorded change in head is plotted against time for each test in the semi-log plots presented in Figures C1 and C2. We made linear approximations of the portions of data which most likely represent the behavior of the target formation and used them to calculate soil hydraulic conductivity in general accordance with the procedures developed by Bower & Rice (1976). The term "general accordance" means that some assumptions and approximations were made to fit the conditions under which the tests were performed. The calculated hydraulic conductivities for each test are presented in Table 1, on the following page.

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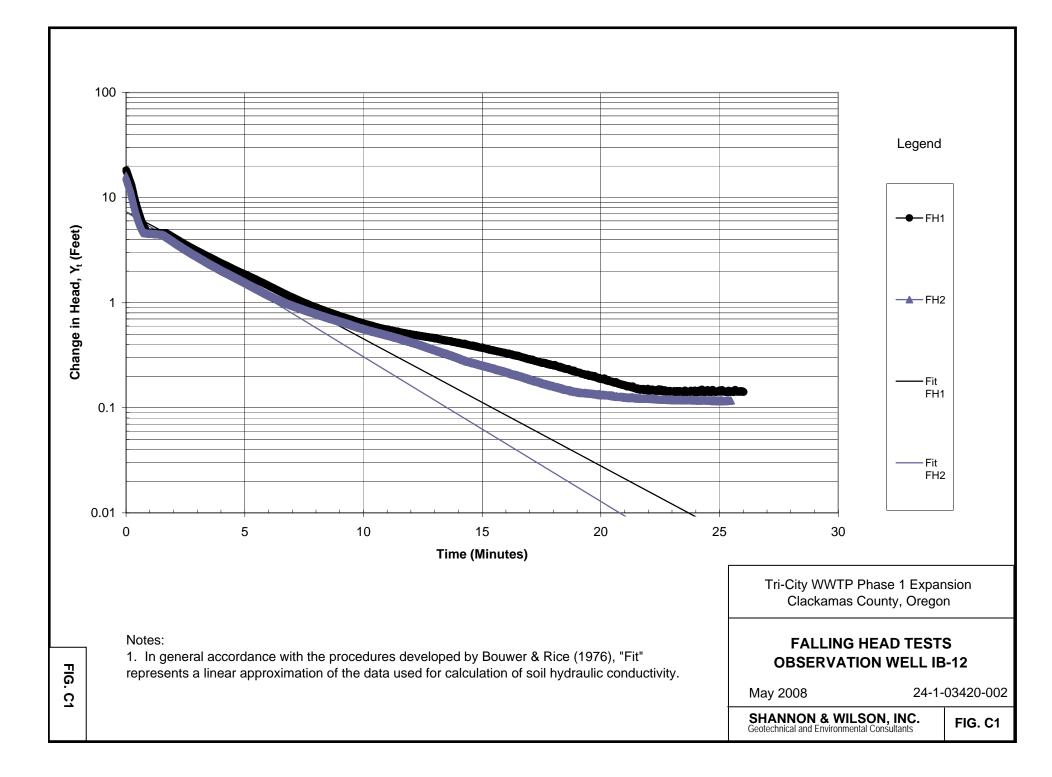
# TABLE C1

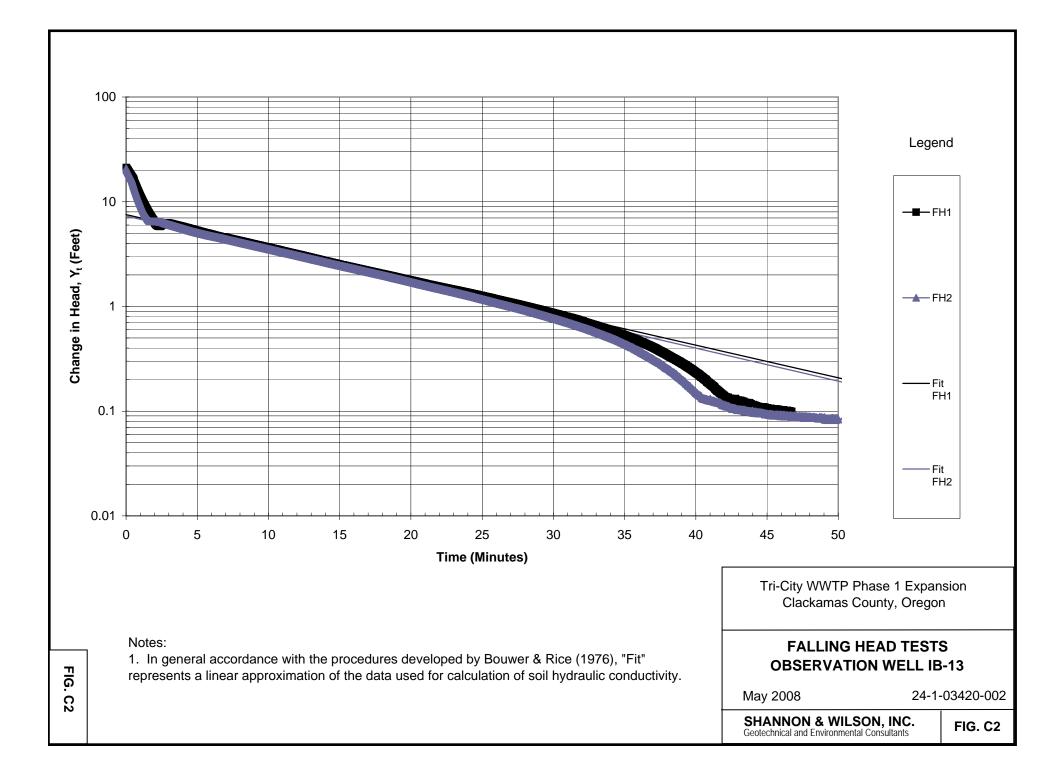
## Falling Head Test Results

BORING	TRIAL 1 K (cm/sec)	TRIAL 2 K (cm/sec)	AVERAGE K (cm/sec)
IB-12	8.1 x 10 <sup>-4</sup>	9.2 x 10 <sup>-4</sup>	8.7 x 10 <sup>-4</sup>
IB-13	2.1 x 10 <sup>-4</sup>	2.1 x 10 <sup>-4</sup>	2.1 x 10 <sup>-4</sup>

### **B.3 REFERENCE**

Bower, H., and Rice, R.C., A slug test for determining hydraulic conductivity of unconfined aquifers with completely or partially penetrating wells, *Water Resour. Res.*, 12(3), 423, 1976.





APPENDIX D

FIELD EXPLORATIONS AND LABORATORY TESTS BY OTHERS

### **APPENDIX D**

## FIELD EXPLORATIONS AND LABORATORY TESTS BY OTHERS

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None

### LIST OF FIGURES

### Figure No.

D2–D70 Previous Boring Logs

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#### **APPENDIX D**

### **PREVIOUS FIELD EXPLAORATIONS**

### D.1 GENERAL

This appendix contains logs from previous exploratory borings on site and the original laboratory testing results. The lab data directly follows the boring logs for each individual source. Sources for the previous explorations are listed in the report text. The approximate location of the borings is shown on Figure 2, Plan of Explorations. Exploratory borings from adjacent properties are not included in this appendix.

#### NOTES:

- 1. THE DEPTH AND THICKNESS OF THE SUBSURFACE STRATA INDICATED ON THE SECTIONS WERE GENERALIZED FROM AND INTERPOLATED BETWEEN SOIL BORINGS. INFORMATION ON ACTUAL SUBSURFACE CONDITIONS EXISTS ONLY AT THE SPECIFIC LOCATIONS AND DATES INDICATED. SOIL CONDITIONS AT OTHER LOCATIONS MAY DIFFER FROM CONDITIONS OCCURRING AT THE BORING LOCA-TIONS. ALSO, THE PASSAGE OF TIME MAY RESULT IN A CHANGE IN THE CONDITIONS AT THESE BORING LOCATIONS.
- 2. BORING LOCATIONS ARE SHOWN ON FIGURE 2.
- 3. BORINGS WERE LOGGED IN THE FIELD BY A CH2M HILL ENGINEERING GEOLOGIST.
- 4. BORINGS WERE DRILLED BY DON KENNER OF OREGON, INC. OF SHERWOOD, OREGON. BORINGS B-1 AND B-3 WERE DRILLED IN DECEMBER, 1981, USING A TRUCK-MOUNTED CME-55, THE REMAINDER OF THE BORINGS WERE DRILLED WITH A TRUCK MOUNTED CME-75 IN DECEMBER, 1981, AND IN JANUARY AND MAY, 1982.
- 5. TRANSITIONS BETWEEN SOIL TYPES MAY BE GRADUAL AND ARE APPROXIMATELY AT THE ELEVATIONS SHOWN.
- 6. SEE THE BORING LOGS FOR DETAILED DESCRIPTIONS OF THE SUBSURFACE CONDITIONS.

LEGEND



BORING NUMBER

-7

SPLIT-SPOON SAMPLE (ASTM D1586), "N"-VALUE

#### STANDARD PENETRATION TEST:

BLOWS - THE NUMBER OF BLOWS FOR THREE 6-INCH INCREMENTS REQUIRED FROM A 140-LB HAMMER FALLING 30 INCHES TO DRIVE A STANDARD 2-INCH O.D. SPLIT-BARREL SAMPLER (ASTM D1586).

"N" - THE SUM OF BLOWS FOR THE SECOND AND THIRD 6- INCH INCREMENTS. IF THE SAMPLER IS DRIVEN LESS THAN 18-INCHES, THEN "N" IS THE NUMBER OF BLOWS FOR THE FRACTION OF THE LAST 2 6-INCH INCREMENTS.

> FIGURE C-6 LEGEND AND NOTES Tri-City Sewage Treatment Plant



#### BORING LOG LEGEND:

#### SAMPLE TYPE:

- S SPLIT-BARREL (ASTM D1586 UNLESS OTHERWISE NOTED)
- ST SHELBY TUBE
- W WASH SAMPLE
- OT OSTERBERG TUBE
- NX DIAMOND CORE BARREL

#### STANDARD PENETRATION TEST:

BLOWS - THE NUMBER OF BLOWS FOR THREE 6-INCH INCREMENTS REQUIRED FROM A 140-LB HAMMER FALLING 30 INCHES TO DRIVE A STANDARD 2-INCH O.D. SPLIT-BARREL SAMPLER (ASTM D1586).

"N" - THE SUM OF BLOWS FOR THE SECOND AND THIRD 6-INCH INCREMENTS. IF THE SAMPLER IS DRIVEN LESS THAN 18 INCHES, THEN "N" IS THE NUMBER OF BLOWS FOR THE LAST TWO 6-INCH INCREMENTS.

UNIFIED SOIL CLASSIFICATION SYMBOL: GROUP SYMBOL AS PER ASTM D 2487

#### NOTES:

- 1. BORINGS WERE DRILLED BY DON KENNER OF OREGON, INC. OF SHERWOOD, OREGON. BORINGS B-1 AND B-3 WERE DRILLED IN DECEMBER, 1981, USING A TRUCK-MOUNTED CME-55. THE REMAINDER OF THE BORINGS WERE DRILLED WITH A TRUCK-MOUNTED CME-75 IN DECEMBER, 1981, AND IN JANUARY AND MAY, 1982.
- 2. ENGINEERING PROPERITES OF SUBSURFACE MATERIALS ARE OPINION OF THE ENGINEERING GEOLOGIST, EXCEPT WHERE LABORATORY TESTING WAS CONDUCTED.
- 3. THE BORING LOGS AND RELATED INFORMATION DEPICT SUBSURFACE CONDITIONS ONLY AT THE SPECIFIC LOCATIONS AND DATES INDICATED. SOIL CONDITIONS AND WATER LEVELS AT OTHER LOCATIONS MAY DIFFER FROM CONDITIONS OCCURRING AT THESE BORING LOCATIONS. ALSO, THE PASSAGE OF TIME MAY RESULT IN A CHANGE IN THE CONDITIONS AT THESE BORING LOCATIONS.
- 4. TRANSITIONS BETWEEN SOIL TYPES MAY BE GRADUAL AND ARE APPROXIMATELY AT THE ELEVATIONS SHOWN.
- 5. STANDARD PENETRATION TESTS WERE TAKEN IN APPROXIMATE ACCORDANCE WITH ASTM D1586.
- 6. SAMPLES WERE EXAMINED IN THE FIELD AND VISUALLY CLASSIFIED IN APPROXIMATE ACCORDANCE WITH ASTM 2488.
- 7. OPEN STANDPIPE PIEZOMETERS WERE INSTALLED IN BORINGS B-1, 3, 5, 7, 11, 13, 14, AND 21. ALL PIEZOMETERS CONSISTED OF A PERVIOUS PVC TIP THAT IS 18-INCHES LONG, 1.5-INCH INSIDE DIAMETER, AND HAS NOMINAL 0.010-INCH SLOTTED OPENINGS WITH 1/4-INCH SPACINGS. ALL TIPS WERE PACKED WITH 3/8-INCH PEA GRAVEL. RISER PIPE CONSISTS OF 3/4-INCH PVC PIPE, WITH APPROXIMATELY 0.5-FEET OF STANDPIPE ABOVE THE GROUND SURFACE. SEE INDIVIDUAL BORING LOGS FOR POSITION OF PERVIOUS TIP, ZONE OF GRAVEL-PACKING, AND LOCATION OF BENTONITE SEAL(S).

D3

BORING LOGS

CH2M

MAJOR	DIVISION	LETTER DESIGNATION	GRAPHIC SYMBOL	DESCRIPTION
	GRAVEL AND GRAVELLY SOIL	GW		Well-graded gravel or gravel-sand mixtures, little or no fines
		GP	1:3:	Poorly-graded gravel or gravel-sand mixtures, little or no fines
OILS		GM		Silty gravel, gravel-sand-silt mixtures
COARSE GRAINED SOILS		GC		Clayey gravel, gravel-sand-clay mixtures
	SAND AND SANDY SOIL	SW		Well-graded sand or gravelly sand, little or no fines
COA		SP		Poorly graded sand or gravelly sand, little or no fines
		SM		Silty sand, sand-silt mixtures
		SC		Clayey sand, sand-silt mixtures
FINE GRAINED SOILS	SILTS AND CLAYS OF LOW PLASTICITY	ML		Inorganic silt of low to medium plasticity, gravelly silt, sandy silt, clayey silt
		CL		Inorganic clay of low to medium plasticity, gravelly clay, sandy clay, silty clay
		OL		Organic silts of low plasticity
	SILTS AND CLAYS OF HIGH PLASTICITY	МН		Inorganic silts of high plasticity.
		СН		Inorganic clays of high plasticity
		ОН		Organic clay and silt of medium to high plasticity
	HIGHLY ORGANIC SOILS	PT		Peat and other highly organic soils
	FILL			Fill, variable composition
	ROCK			Siltstone
				GRAPHIC COLUMN LEGEND
				D4

CH2M					SOIL BORING LOG						
PROJECT TRICITY STP DRILLING METHOD ROTARY MUD, C ELEVATION 42.51 FEET WATER LEVELSEE TEXT DATE:						LOCATION OREGON CITY, OREGON ME-55 DRILLERS & EQUIPMENT D. KENNER OF OREGON, INC. BORE HOLE: B-1 START: 12/21/81 FINISH: 12/22/82 INSPECTOR CWH					
DEPTH BELOW SURFACE	INTERVAL	SAMPLE H H H H H H H H H H H H H H H H H H H	RECOVERY (INCHES)	STANDA PENETRA TEST RES BLOWS 6''-6''-6''	FION	SOIL DESCRIPTION (COLOR, RELATIVE DENSITY OR CONSISTENCY, MOISTURE, GRAIN SHAPE AND TYPE, STRUCTURE, CEMENTATION, ORGANICS, MATERIAL)	GRAPHIC LOG	UNIFIED SOIL CLASSIFICA- TION SYMBOL	COMMENTS (DRILLING PROGRESS, LOST CIRCULATION, TYPE OF DEPOSIT, PROBLEMS, ETC.)		
	5.0					•			START DRILLING a 11:25 LANDOWNER NOTES FILL MIGHT HAVE BEEN DUMPED ON SITE DUBING CONST- RUCTION OF I-205		
5-	7.0	ST-I	21			SAND. SIMILAR TO S-1 (SEE BELOW)			BEGIN WITH DRAG BIT CHANGE TO ROLLER BIT AT 24,9		
_	8.5	5-1	7	2-2-2	4	SAND, FINESAND WITH LESS THAN 5% NON PLASTIC FINES, BROWN, MOIST, VERY LOOSE.		SP	- ÈT,		
- 01	10.0	5-2	7	2-1-2	3	SAND, SAME AS S-1		SP			
- - 15	15.0	5-3		2-3-5	8	SAND, SANIE AS S-1		SP	-		
-  					0	-					
	<u>200</u> 21.5	5-4	17	2-2-2	4	SILTY SAND, SIMILAR TO S-1 EXCEPT 20-25% NON-PLASTIC FINES		SM			
-7,5 - -,25-	<u>25.0</u> 26.5	5.5	14	26-46-46	92	SANDY GRAVEL, POORLY GRADED; WELL ROUNDED GRAVEL AT LEAST TO 144TWCH, 20% FINE-TO-		GP	Deiller Notes HARC DRILLING AT 249FT MIXMORE MUD AT - 25FT,		
	- ممين + ليك بينم. 				<u>.</u>	COARSE SAND, MCSTLY MEDIUM, ABOUT 5% NON-PLASTIC FINES, WET, BROWN AND BLACK, VERY DENSE.	9,0		SLOW ROUGH DRILLING TO 46 FT.		

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SHEET 2 OF 3

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## SOIL BORING LOG

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DRILLIN	G MET	HOD_M	UD I		1E -5	DRILLERS & EQUIPMENT DON				
ELEVATI			-	ET	,				LE: <u>B-1</u>	
WATER	LEVEL	SEE TR	EXT	DATE:		START: 12/21/81FINISH: 12/	22/81		INSPECTOR CWH	
(77)	S	SAMPLE STANDAR							COMMENTS	]
1	AL	æ	RECOVERY (INCHES)	PENETRAT TEST RESI		(COLOR, RELATIVE DENSITY OR	10 106	UNIFIED SOIL CLASSIFICA- TION SYMBOL	(DRILLING PROGRESS, LOST CIRCULATION,	
DEPTH BELOW SURFACE	INTERVAL	NUMBER	CHE	BLOWS	BPF	CONSISTENCY, MOISTURE, GRAIN SHAPE AND TYPE, STRUCTURE, CEMENTATION, ORGANICS,	GRAPHIC	ASSI N S	TYPE OF DEPOSIT, PROBLEMS, ETC.)	·
		N	ЯЩ ПN	6''-6''-6''	"N"	MATERIAL)				
30	30 31.5	5-6	8	55-60/6.	105/	SANDY GRAVEL, SINILAR TO S-5, WITH ABOUT 30% GRAVEL	0.0	GP	LOST CIRCULATION AT 31.5 FT., 32 AND 35	
			0	/0	/12."				FT, REQUIRED MIXING	i.
	1		2				.00		MORE MUCH	ŕ
· ·	1						• 68 8		-	,
52	1				•		2.0			
	35.0	LS-7	•		( ) (	NO RECOVERY	200		SAME COARSE, ANGULAR	
	35,5	$\sim$	0	60/5"	60/ /5		0		SAME COARSE, ANGULAR SAND CUTTINGS IN SAMPLE TUB.	
.		Ì						1	DRILLER NOTES SAND -	
.	-								LENS AT 37-38 FT.	7.
							100		_	`
40-	40.0									- 1- 1- 1- 1- 1- 1- 1- 1-
-10	41.5	5-8	~	60/3"	60/ 13"	NO RECOVERY	.0.		SAMPLER BOUNCED TOURING SPT	
.	1		0	13	13"		0.00		LOSE CIRCULATIONAT	
.	1						0.	]	43FT	
-	-						2.0.	Ç	ADD NEW TRI LONE	
.	_						- B	1	BIT AT43FT	
45-	45.0	C I		•.		NO RECOVERY	4.6		DRILLER NOTES CHANGE	
	46.5	5-9	0	6qui	60/ 4"		10		AT 46 FT, -	1000
			·		14				SAMPLE 55-6 PROBABCY	daran .
								1	TRIP UP, SILFY SAND	~
									CARED ON SAMPLICA	
	50.0									÷
50-						SILTSTONE, HIGHLY WEATHERED PLASTICITY, 5-10% FINE-TO-MED-			_	
-	51.5	5-10	18	7-11-16	27	IUM SANDIN UPPER 9 INCHES DARK GRAYISH - GREEN WITH		ML	-	w
.	-					APRILICE RPAILIN AND TELLUMISH			-	
						MOTTLING, MOIST, VERY STIFT.				
	-								-	
55-	55.0									
				1					-	
1	57.0	ST-2	12							
10000000000						SILT, SAME AS S-10		ML		
-	58.5	SS-11	18	5-11-14	27				FINISHED DRILLING AT	
	and				END	BORING AT 58.5 FEET			1:00	
60						-			FORM D 1586 5/78	
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₩₩1 <sup>-</sup> 11111	-					SOIL BORING			
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	τ <u>_TRI</u>					LOCATION ORE			
				<u>DTARY, CN</u>	<u>1E-5</u>	DRILLERS & EQUIPMENT_D.			
ELEVAT				NTE.				E HOI	
		SAMPLE		STANDA		SOIL DESCRIPTION			COMMENTS
μ				PENETRAT TEST RESU	TION	COLOR, RELATIVE DENSITY OR	C C C	SOI CA-	(DRILLING PROGRESS,
DEPTH BELOW SURFACE	INTERVAL	NUMBER	RECOVERY (INCHES)	BLOWS	BPF	CONSISTENCY, MOISTURE, GRAIN SHAPE AND TYPE, STRUCTURE,	GRAPHIC	UNIFIED SOIL CLASSIFICA- TION SYMBOL	LOST CIRCULÀTION, TYPE OF DEPOSIT, PROBLEMS, ETC.)
DEI SUJ	INT	NN NN	REC (IN	6''-6''-6''	"N"	CEMENTATION, ORGANICS, MATERIAL)			
	-					PIEZO METER INSTALLATION	(588	NOTE	S, BORING LOG LEGEND) -
•	-					PLACE MENT OF PERMOUS TIP!	TOP	AT 3	3.5 FT, ВоПОМ
	~					AT 40.0FT. GRAVEL PACK ; FROM 58.5 FT	TO	24.9	FT
-						BENTONITE SEAL! FROM 22.9	TO	24.9	er,
	-					RISER PIPE LENSTH: 40 FEE	T,		
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					CME	-55 DRILLERS & EQUIPMENT DON	KEN	INER	OF OREGON, INC	
ELEVATI	ON	Ho.13	FT,			E	BOR	E HOI	LE: <u>B-3</u>	
WATER	LEVELS	SEE TE	<u> </u>	DATE:		START: 12/22/81 FINISH: 12/2	38		INSPECTOR <u>CWH</u>	`
(FT)	s	AMPLE		STANDA		SOIL DESCRIPTION	LOG	olt a. 30L	COMMENTS	
ACE	NTERVAL	ЕR.	RECOVERY (INCHES)	PENETRAT TEST RESU	ILTS	COLOR, RELATIVE DENSITY OR CONSISTENCY, MOISTURE, GRAIN		UNIFIED SOIL CLASSIFICA- TION SYMBOL	(DRILLING PROGRESS, LOST CIRCULATION,	
DEPTH BELOW SURFACE	NTEF	NUMBER	INCH	BLOWS 6''-8''-6''	BPF	SHAPE AND TYPE, STRUCTURE, CEMENTATION, ORGANICS, MATERIAL)	GRAPHIC	CLAS	TYPE OF DEPOSIT, PROBLEMS, ETC.)	
NBU NBU	11	4	æ=	0-0-0	IN	MATERIAL	πm		START DRILLING AT	
	-		f						2:35	
	5.0						- 		BEGIN WITH DRAG BIT, CHANGE TO - ROLLER BIT AT 25.3 FT.	
-0	6.5	5-1	8	Y12" -2	2	SANDY SILT, NON TO SLIGHTLY PLASTIC FINES, ABOUT 25% FINE SAND, BROWN, MOIST, VERY SOFT.		ML	• · · · · · · · · · · · · · · · · · · ·	
	7.0								र	1997
	9.0	ST-I	21		-				-	
10-	10.0					SALIDY SUT STALLAD TO S-1				er. Br
	11.5	S-2	8	2-2-2	4	SANDY SILT, SIMILAR TO 5-1, WITH 30-40% FINE SAND.		ML	_	
									-	
15_	15.0					SILTY SAND: FINE SAND WITH				- 
	_	ST-2	19			15-2041 NON TO SLIGHTLY LASTICIT		SM		
· ·	17.0					FINES, BROWN, WET, VERY SOFT			-	1. P. 1. 100
	-								-	2.2
	20.0			f					-	a.
20-		53	2	3-4-5	9	SILTY SAND: SIMILAR TO ST-2, WITH 10-15% FINES.		SM		Particular Part de No. 14
	21.5	50		0-7-0					DRILLER NOTES	
	_								GRAVEL AT 23.5 FT	5 <sup>*</sup> 1
	24.5						. •		-	
25-	-	5-4	2	19-28-32		SANDY GRAVEL POORLY-GRADED ROUNDED GRAVEL TO ATLEAST 14	0.0	GP- GM	SLOW, ROUGH DRILLING TO 485FT	Para Bara Santa Santa Man Man Man Man Man Man Man Man Man Ma
	26.0			1120-52	$\odot$	INCH MAXIMUM STEE, SHOWN TO	•		-	
approx.			a fe da			BLACK, WET, VERY DENSE.		7 (2012)	۰ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ	
			a la rendere de la contra de				0.	لارا معدما المعدمة المعدمة المعالمة المعالمة المعالمة المعالمة المعالمة المعالمة المعالمة المعالمة المعالمة الم	arvin arv	
Nor American State		a fan men welder welder welder welder	an a management of the second s			D8	4 4 60 4			[, i. t <sub>1</sub> ,
30-	1						RA D		FORM D 1586 5/78	1.2°

	]				r		:	PROJEC	SHEET	20=3
CH2M								_	600.A5	-
						SOIL BORIN	G LO	G		tar v
<b></b>			1)				0 m d av			
PROJECT					ME-5	LOCATION OF				
ELEVATI							_BOR	E HO	LE: <u>B-3</u>	
WATER	LEVEL	SEE TE	<u>T x</u>	DATE:		START: 12 22 81 FINISH:	23/9		INSPECTOR	CWH
(FEET)		AMPLE		STANDA PENETRAT	TION	SOIL DESCRIPTION	100	UNIFIED SOIL CLASSIFICA- TION SYMBOL	COMME	NTS
H ACE	INTERVAL	BER	RECOVERY (INCHES)	BLOWS	ULTS BPF	COLOR, RELATIVE DENSITY OR CONSISTENCY, MOISTURE, GRAIN	ніс	SIFIC	LOST CIRCUI	LATION, 2
DEPTH BELOW SURFACE	NTEF	NUMBER	RCO INCH	6"-6"-6"	''N''	SHAPE AND TYPE, STRUCTURE, CEMENTATION, ORGANICS, MATERIAL)	GRAPHIC	UNIF	TYPE OF DE PROBLEMS, E	
30	30.0				44	SANDY GRAVEL, SAME AS 5-4.	-	GP-	LAST 6" OF	DKWG
-	31.5	S-5	3	24-28-16	47	,	20	GM	FOR SS-5 1 BE A SAND	LENS
-			,				8 - B			
							9.			111
35-	35.0					NO RECOVERY	00		809990	A set of the set of th
	35.2	5-6	0	60/2"	60/2"	NO RECORDER	0.0			14 100 14 100 100 100 100 100 100 100 100 100 100
		. ~					10	·		- 
	-						00			alama Alama
							0.0			-
40-	40.0	5-7		1.01	607	SANDY GRAVEL, SAME AS 5-4	8	GP-		- <b>-</b>
-	41.3	11	3	694"	60/ /4″			GM		-
			-							
-	1					-	Øø			
45-	45.0						5			
-ر۳	45.2	\$8	0	60/2"	60/ /2"	NO RECOVERY	.0		-	
				12	12		0.		-	. <b></b>
				-			: 12		DRILLER NO	DRILLING
	-								RATE (UP) A	13.3 - 4
50-	50.0		-tototo aparentation			SILTSTONE HIGHLY WEATHERED,				ې بې
-	51.5	s-9	14	26-54-60	114/	10-15% FINE TO MEDIUM SHUE				-
-	-				l.,,,_	GREEN AND WHITSH MOTILING, SLIGHTLY MOIST, VERY DENSE.				_
-	~									-
-	55.0									
55-	56.0	5-10	14-	25-101	85/10"	SILTSTONE, SAME AS S-9,				
	0.00		14-	25-60/4"	/10"				FINISH DRI	
						END BORING AT 56.0 F	1====1		AT 1:00	
					u a a-v a alla sega sta mond					
	-					D9	And an alternatives	lan-sing search of		
	Langer Stranger			\$ 	<u> </u>			i	EOGM D 1	

FORM D 1586 5/78

CH2M
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SHEET 1 OF 3

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	100	00.	$\overline{n}$	$\sim$

SOIL BORING LOG

LOCATION OREGON CITY, OFEGON PROJECT TRI CITY WTP DRILLERS & EQUIPMENT D. KENNER OF OREGON. INC DRILLING METHOD ROTARY MUD', CME-75 ELEVATION 44.75 FEET BORE HOLE: B-5 INSPECTOR LWH 1/13/82 WATER LEVELSEE TEXT DATE: 1 12 82 FINISH: START: UNIFIED SOIL CLASSIFICA-TION SYMBOL SOIL DESCRIPTION LOG COMMENTS (FT)SAMPLE STANDARD PENETRATION RECOVERY (INCHES) DEPTH BELOW SURFACE NTERVAL TEST RESULTS COLOR, RELATIVE DENSITY OR IDRILLING PROGRESS, GRAPHIC LOST CIRCULATION, TYPE OF DEPOSIT, CONSISTENCY, MOISTURE, GRAIN SHAPE AND TYPE, STRUCTURE, CEMENTATION, ORGANICS, NUMBER BLOWS BPF PROBLEMS, ETC.) "N" 6''-6''-6'' MATERIAL) START DRILLING AT 2:10 , 5.0 SANDY SILT NON PLASTIC, ABOUT 35% FINE SAND BROWN, MOIST, VERY SOFT TO SOFT. 5 9 ML 5-1 1-1-1 2 6.5 8.0 ST-1 24 10.0 10 -SANDY SILT, SAME AS S-1. ML 1-1-1 2 S-2 12 11.5 15.0 15-SANDY SILT, SIMILAR TO S-1, WITH ABOUT 40% FINE SANDS 9 ML 1-2-1 5-3 3 16.5 18.0 ST-2 24 20 SANDY SILT SHITE AS S-1 30 1-1-3 ML 14 4 5-4 21.5 SAND, POORLY GRADED FINE SAND, 5-10% NON PLASTIC FINES, BROWN, MOIST, LOOSE 25.0 Z. SP-SN 3 5-3-7 0 SM S-5 26.5 DRILLER NOTES GRAVEL AT 27FE 3  $\odot$ D10 30

(	1					· · · ·			<u>3 SHEET 3 OF</u>	<u> </u>
CH2M HILL									т NUMBER 5600, A5	
						SOIL BO	RING LÓ			
PROJECT				STP					CREGAN	
ORILLIN		100 <u>~</u> 44.7!		<u>KOIART, C</u>	ME -	75 DRILLERS & EQUIPMENT			<u>F.OREGON, INC.</u> LE: <u>B-5</u>	· · ·
WATER					_					/H
		SAMPLE		STANDA		SOIL DESCRIPTION				<u></u>
			ERY S)	PENETRA TEST RES	TION	COLOR, RELATIVE DENSITY OR	. F0G	SOI ICA- MBO	DRILLING PROGRI	
FAC	NTERVAL	NUMBER	DV EI HES]	BLOWS	BPF	CONSISTENCY, MOISTURE, GRAIN SHAPE AND TYPE, STRUCTURE,	GRAPHIC	SSIF SSIF	LOST CIRCULATION	N, 1
DEPTH BELOW SURFACE	NTE	NUM	RECOVE	5**-6**-6**		CEMENTATION, ORGANICS, MATERIAL)	GRA	UNIFIED SOIL CLASSIFICA- TION SYMBOL	PROBLEMS, ETC.)	
60				·····	<u> </u>			-	DRILLER NOTICES	
-		ļ							CHANGE IN DRILL RATES TO 65 FT	
	ļ								•	<b>1</b>
										-
-			-							-
65-	650 658	S-12		  •	101	SILTSTONE, SIMILAR TO S- EXCEPT FOR LOCAL BLUE- GREEN AND ORANGE - BROW	11,	, ,	]	
	പ്പാപ്പ	0-14	9	28-6934	88/91/2	EXCEPT FOR LOCAL BLUE-	~			
-						MOTTLING				
									5.	
										r
70_									DOUT SP LINTS	1
									DRICLER NOTES, UNIFORM DRILL	ng j
									TO 75 FT, EXCEP" FOR OCCASSIONAL	
-									lenses of hard	er
-				-					material, possi gravel	5.7
-					1				<i>J</i> .	
75-	75.0 75.5	5-13		1.01	60/	SILTSTONE, SIMILAR TO S-11, E	PINK			
			5	60/5	15"	SILTSTONE, SIMILAR TO S-11, E FOR BLUE-GREEN AND ORANGE- MOTTLING.				
-						END BORING AT 75.5 FT				
-									Donin Loo Les	A
-						PLEZOMETER INSTALLATION	( sea no	tes o	28 SET BOTTON	M
				ļ		AT UND FT	1	1	}	_
-						GRAVEL PACK! FROM	1 76.5F	- 70	GROUND SURFAC	æ,
						BENTONITE SEAL FROM		) ;		, i
						RISER PIPE LENGTH :	40 FT.			
_										
-										-
-										-
whether editors are				an-under sole to be a series of				-	*	
-								d suff-suff-suff-suff-suff-suff-suff-suff		a constant
						D11				

CH2M HILL EET | OF 2

PROJECT NUMBER PISGOO-AS

											<b>_</b>
				<u>STP</u>	ا					TY. OREGON	
DRILLIN					<u>-146 -</u>	75 DRILLERS & EQUIPMENT D.				LE: B-6	
		NOT					_BC  12				
WATER	LEVEL	MEAS		DATE:						INSPECTOR CWH	7.
(FT)	5	SAMPLE		STANDA PENETRAT		SOIL DESCRIPTION	L0G		SOL OIL	COMMENTS	
щ	AL	E E	ERY S)	TEST RESU		(COLOR, RELATIVE DENSITY OR			UNIFIED SOIL CLASSIFICA- TION SYMBOL	ORILLING PROGRESS	
DEPTH BELOW SURFACE	NTERVAL	NUMBER	RECOVE	BLOWS	BPF	CONSISTENCY, MOISTURE, GRAIN SHAPE AND TYPE, STRUCTURE,	GRAPHIC		SSI N S	LOST CIRCULATION, TYPE OF DEPOSIT,	, o,
DEP	NT	NUN	LINC	6''-6''-6''	''N''	CEMENTATION, ORGANICS, MATERIAL)	GR		SUS	PROBLEMS, ETC.)	-12,13 (****,2)
(						SILTY TOPSOIL AT SURFACE		Ī		START DRILLING	··· ··· ···
· -	-									AT 3:30 -	
, .								11		-	• 2
	-						] ]			-	
· ·	-				•	-				-	
5-	5.0				········	SANDY SHITLOW QUESTICITY					
		5-1	9	2-1-1	3	SANDY SILT, LOW PLASTICITY, 30-40% FINE SAND, BROWN,			ML	_	
	6.5	, , , , , , , , , , , , , , , , , , ,	1			MOIST, VERY SOFT, TRACE OF ORGANIC MATERIAL					-
	8.0					ORGANIC MATERIAL					
· ·	0.0					SILT, LOW PLASTICITY, ABOUT 10%				-	:
· .	-	< <u>-</u> 1	~~			FINE SAND, BROWN, MOIST, VERT			1 I I	-	
10-	10.0	ST-I	20			SOFT			ML	_	· ·
						SILT, SAME ASS-1,			ML	-	
	11.5	5.2	14	2-2-4	6					-	<b>.</b>
-										-	·
	-									-	
-								11		-	
	15.0	l								,	
15-	100					SILTY SAND, LOW PLASTICITY, 58% FINE SAND, 32% SILT, 18%	itti				
.	16.5	S-3	9	3-3-4	7	58% FINE SAND, 32% SILT, 18%		ł	SM	-	
.						CLAY, BROWN, WET, LOOSE.				-	
						-				-	
	]										
· .	-								•	-	
20-	20.0	1								ENKOUNTERED -	8.7¥
			17					Į.	-	GRAVEL AT 21FT,	
	22.0	ST-2	13				.9.0	ė.		SHELBY TUBE BENT-	
-	22.8	54		00 101	921	SANDY GRAVEL, ROUNDED GRAVEL	9.6	). ()	GP-	LOSE CHRCULATION-	
	1	1	6	32-60/41/2	92/ 10/2	TO AT LEAST 14" ABOUT 25%	10	3	GM	AT 23 FT, MIX MORE MUD, SOFTER	1
	-					NON PLASTIC FINES, BROWN,	2.02			DRILLING 23-25 PT	3
25-	25.0		<u> </u>			VERY DENSE.	200	١Ų		,	8 × 41
1 25-		0.5				NO RECOVERY	69	0		POSS. SAIND LENS	in the
	265	S-5	0	14-20-5	25		0	9		FROM 23-26 FT? LOSE CIRCULATION AT	ŕ
	-				~		10	I		26 FT, MIXMORE MUD	2. ji
		the second se					DU	Ĩ		SLOW ROUGH DRILLING TO SO FT.	
or watching a real							0	3		10 20 101	
							0			- •.	
	1		}			D12	<u>8-</u> 19				
										- FORM D 1586 5/78	3

	-					SHEET 2000
CH2M						PROJECT NUMBER PI5600, A5.
						SOIL BORING LÓG
				-		
PROJEC						LOCATION OREGON CITY, OREGON
		400 <u>N</u> 42.16		ROTARY		DRILLERS & EQUIPMENT O.KENNER DE OREGON, INC
ELEVAT		NOT		DATE:		BORE HOLE: B-6 
	·	SAMPLE		STANDA	20	
(FT) w			ERY [\$]	PENETRAT TEST RES	TION	
DEPTH BELOW SURFACE	INTËRVA	NUMBER	RECOVE	BLOWS	BPF	Image: Color, Relative Density OR       O
	INI	NUN	REC	6''-6''-6''	"N"	CEMENTATION, ORGANICS,
30	30,4	5-6	0	60/5"	60/	NO RECOVERY SAMPLER BOUNCED PURING 55-6 SPT
			<del></del>		15	MIX MORE MAD AT
	_					
	-	-				
35-	35.0	A			(0)	SAMPLER BOUNCES
	1	\$-7	0	60/3"	60/ 13 <sup>11</sup>	NO RECOVERY
	]					DRILLER NOTES
	-	[				LARGE ROCKS IN HOLE
	-					
40	40.0				INS/	SANDY GRAVEL, POORLY GRADED GP- SAMPLER BOUNCES ROUNCED GRAVEL TO ATLEAST GM DURING SS-8 SPT
	41.5	5-8	6	48-45-603.	19"	ROUNCED GRALEL TO ATLEAST GO GM DURING SS 8 SPT
						ROUNCED GRAVEL TO ATTENT TO GOD GALLESS SHT -
	]					DENSE
	11- 0					
45 -	45.0	59	~	601	607	NO RECOVERY
	1		0	60/z'/2	607 121/2	
	-					DRILLER NOTES
	-					CHANGE IN DRILLING Tate (Up) at 50 FT.
	-					
50-	50.5					SILTSTONE, HIGHLY WEATHERED
	52,0	5-10	12_	14-26-47	73	ABOUT 10% ROUNDED FINE TO
						MEDIUM SAND, GRAY, MOIST, FINISH D RILLING AT 1:15
		Í				END BORING AT 52.0 FEET
55-						
					ĺ	
-						
vibiosphartstaling set					Amount of the second seco	
	1					D13
						FORM D 1586 5/78

H2M						PROJECT NUMBER
НĨЦ						SOIL BORING LÓG
						SOL DOUNG LOG
OJECT	TR	C		STP	· · · ·	LOCATION OREGON CITY, OREGON
	;	100 <u>MI</u> H.33			ME -	55 DRILLERS & EQUIPMENT D. KENNER OF OREGON, INC.
EVATI				∠ I DATE:		BORE HOLE: <u>6-7</u>
FT	<b></b>	AMPLE		STANDA	80	
•				PENETRAT	TION	COLOR, RELATIVE DENSITY OR U COMMENTS
DEPTH BELOW SURFACE	NTERVAL	NUMBER	RECOVERY (INCHES)	BLOWS	BPF	CONSISTENCY, MOISTURE, GRAIN T 56 LOST CIRCULATION, SHAPE AND TYPE, STRUCTURE, 5 22 TYPE OF DEPOSIT.
SUF	INT	NUN	REC	6''-6''-6''	"N "	
						START DRILLING AT 8:55
_	ļ					
-						
	_	-				
5-	5.0					SANDY SILT, LOW PLASTICITY,
	6.5	5-1	5	1-2-1	3	ABOUT 40% FINE SAND, BROWN, ML
-	<u>.s</u>					
-	8.0					
	-	ST-1	24			SILT, SIMILAR TO 5-1, EXCEPT NO FINE SAND. ML
10 _	10.0	2, 21	-2-4			
		5-2	7	1-3-2	5	SILTY SAND, FINE SAND WITH SILL SM
-	11,5					BROWN, MICIST, LOOSE.
	l					
-	1					
5-	15.0					
-		S-3	Ь	2-2-2	4	SILTY SAND, SIMILAR TO 5-2 HALL EXCEPT ABOUT 65% FINE SANCE SM
-	16.5					
-			-			
_0-	0.00					CUTUSAND SIMULAR TO S-2 HIT ROCK OR STONE
		ST-2	18			SILTY SAND, SIMILAR TO S-3 HIT ROCK OR STONE AT BOTTOM OF ST-2
	22.0			•		
		S-4	6	12-13-17	30.	GRAVEL AT 72 FT
	21.5					ROUNDED GRAVEL TO AT LENSI 117 INCH, 20-30% FINE SAND, ABOUT 520 GM NON PLASTIC FINES, BROWN, WET, COMPACT,
25-	25.0					
	0	5-5	6	30-49-64/2	109/	SANDY GRAVEL SIMILAR TO S-4, 5 GP- SAMPLER BOUNCES- EXCEPT ABOUT 15% FINE SAND GP GM SAMPLER BOUNCES-
	265			15	<b>└</b> ∠↓ _	MIX NOKE MUD; -
				5		SLOW, RUIGH DEILLING TO 449 FT.
	La norte entre transmissione	(mailer work)				
						D14
30-	<u>J</u>	(	}		J	FORM D 1586 5/78

CI (a) I	1							PROJEC	SHEET 2 OF 2
CH2M HILL								PI	5600. AS
	1					SOIL BORIN	G LÓ	G	
ROJECT				TP		LOCATION OR			ÓREGON
		100 <u>M</u> 41.33			1E-7	5 DRILLERS & EQUIPMENT_D.			OF DREGON, INC
LEVATI VATER	ON					START: 1/11/82 FINISH: 1/11	_вон 192	e hoi	LE:B-7 INSPECTORWH
(FT)		SAMPLE		STANDAR	D	SOIL DESCRIPTION	DOT	ы. Б. Е	COMMENTS
	AL	æ	s) S)	PENETRATI		(COLOR, RELATIVE DENSITY OR		UNIFIED SOIL CLASSIFICA TION SYMBOL	DRILLING PROGRESS,
DEPTH BELOW SURFACE	INTERVAL	NUMBER	RECOVERY (INCHES)	BLOWS	BPF	CONSISTENCY, MOISTURE, GRAIN SHAPE AND TYPE, STRUCTURE, CEMENTATION, ORGANICS,	GRAPHIC	ASSI ASSI ON S	LOST CIRCULATION, TYPE OF DEPOSIT, PROBLEMS, ETC.)
30	2 30.0	ъ Г	RE	-6''-6''-6''	"N"	MATERIAL)	ë o o D	53F	
	31.5	5-0	2	24-39-46	85	SANDY GRAVEL, SAME ASS-4			ORILLER NOTES TEMP
					_	•	200		FROM 335-34.5 FT, POSSIBLE SAND LENS,
	-						000		· · · · · · · · · · · · · · · · · · ·
							•0•6		2 
35 _	35.0 35.4	5-7	0	601	<i>.</i> 0/	NO RECOVERY		-	
		-		60/412	14'h		200		-
							2° U		₩ ₩ ₩ ₩
-									
-	40.0						0.00		
40-	40.2	5-8	0		60/	NO RECOVERY	a Do		CAVING IN HOLE TO
-	1			60/21/2	12/2	,	0		+040 TATALE SS-8 - SAMPLER BOUNCES DURING
			-	l i			, C		SS-8 SPT. DRILLER NOTES CHANGE
			,				00.		IN DIRILING RATE (49) + 4T 44.9 FT.
45-	45.0						0		
~		5-9	18	11-30-1004	10/	SILTSTONE HIGHLY WEATHERE AND OXIDIZED PARTICLES COMPOSED OF SILT AND CLAY			
-	465		10	1 20 444	10_	COMPOSED OF SILT AND CLAY			
	-					LIGHT BUE-GREY ORANGE, AND DARK GRAY, MOIST, RELIGT TEXTURE OF MORE COARSE - GRAINED ROCK APPARENT			•
	_					OF MORE COARSE - GRAINED ROCK		-	-
50 -	50.0					SUTTING SAME AS SA EXCEPT		•	_
-		5-10	12	15-28-42	70	SILTSTONE, SAME AS S-9 EXCEPT FOR UNIFORM LIGHT BLUE-GREY			-
-	51,2	5-10	122			END BORING AT SIS FT			FINGH DRILLING AT
-							Doute	1.01	1:45 Lesend
-	_			PIEZOME	TER	INSTALLATION! (See notes on TOFPERVIOUS TIP: TOP AT 35	FT. R	DITON	AT 37.5 FT
	+				31 L				_
				BENTO	NITE	SEAL: FROM 18 TO 20 FEET			м.
-				RISEF	2 · P11	DE LEWGTH : 37,5 FT.			-
	-						August 10		
				And a second sec					
						D15			FORM D 1586 5/78

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CH2M ₩HILL
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SHEET | OF 2 PROJECT NUMBER P15400, A5

•						JOIE DOMIN		00		
PROJECT	r <u> </u>		ITY	STP		LOCATION OR	260	NCI	TY, OREGON	
				ROTARY, ( FEET	SME	-55 DRILLERS & EQUIPMENT_D				
ELEVATI WATER				DATE:		START: 12 28 81 FINISH: 12			LE: <u>B-11</u> INSPECTOR CWH	
(FT)		SAMPLE	_	STANDA		SOIL DESCRIPTION	10G			ŀ
1	VAL	R	rerγ es)	PENETRAT	TION	(COLOR, RELATIVE DENSITY OR CONSISTENCY, MOISTURE, GRAIN		ED SO	DRILLING PROGRESS,	
DEPTH BELOW SURFACE	INTERVAL	NUMBER	RECOVERY (INCHES)	BLOWS 6''-6''-6''	BPF	SHAPE AND TYPE, STRUCTURE, CEMENTATION, ORGANICS, MATERIAL)	GRAPHIC	UNIFIED SOIL CLASSIFICA	TYPE OF DEPOSIT, PROBLEMS, ETC.)	r
-	-					· · ·			START DRILLING	
-	-						<u>  </u>		-	
	-								-	
5-	5.0					SILT LOW TO MEDIUM			-	· · ·
	6.5	S-1	6	1-1-2:	3	PLASTICITY, ABOUT 5% FINE SAND, BROWN, VERY MOIST, SOFT,		ML		
	-								~	i.
ļ	-								-	
10-	10.0		10	1-2-2	i 4	SILT, LOWTO MEDIUM PLAS - TIGTY, 10-15% FINE SAND BROWN		ML	-	ι,
	11.5	5-2	10	1- <u>2</u> - <u><u><u></u></u></u>		MATERIAL				·
	13.0		<u> </u>							
15-	15.0	ST-I	24						_	
- 15	16.5	5-3	18	1-1/12"	l	SILT SAME AS 5-2		ML	-	
	-								-	
									-	
-06	20.0					SANDY SILT SIMILAN TO S-2			-	-
-	<u></u>	S-4	18	1-1-1	21	SANDY SILT, SIMILAE TO S-2 EXCEPT FOR 20-30% FINE TO MEDIUM SAND MOSTLY FINE		ML	ELSUULIBE	Ď.
	~								-	=.
								P\$  ~-	DRILLER NOTES GRAVEL AT 245 FT	
25-	25.9	5-5		28-60/41	88/ .10"	SANDY GRAVEL, POORLY GRADED, ROUNDED GRAVEL TO ATLENST	1. 1	0 60- 6 60-		
	L		6	20- 0741	.10	SAUD & DA FILLES WITH LOW TO	10	¢	SLOW, ROUGH DRILLING _ TO 30 FT.	
-					ana ana ang ang ang ang ang ang ang ang	MEDIUM PLASTICITY, BRIWN, WEJ VERY DENSE		0	LOSE CIRCULATION AT -	
					an and a state of the state of the state of the	D16	.0.	2	28 FT,	
L			[ 	I			[x	fe fail Hannesson conserved	FORM D 1586 5/78	}

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SHEET 2 OF 2

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BROLET_TRI_CITY_STP         LOCATION         DESCRIPTION           DRILLING METHOD         ROTACY         DRILLENS & EQUIPMENT_D.KEAUER_D.G. OK         DRILLENS & EQUIPMENT_D.KEAUER_D.G. OK           MATER LEVELSE_TEXT_DATE:         STANDARD         STANDARD         STANDARD         BORE HOLE:         B'II           MATER LEVELSE_TEXT_DATE:         STANDARD         STANDARD         STANDARD         BORE HOLE:         B'II           TABLEN         SAMPLE         TREMATION         STANDARD         STANDARD         BORE HOLE:         B'II           TABLEN         SAMPLE         STANDARD         STANDARD         STANDARD         BOLD SECRIPTION         B'III         B'IIII STANDARD         B'IIII STANDARD         B'IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII			<i></i>								ſ			
BLEVATION         42.50 FT         BORE HOLE:         B-II           WATER LEVEL\$25C TEXT DATE:														
MATER LEVEL SET EXT DATE:START: $12/28/21$ PRINCH: $12/28/51$ INSPECTOR CLUHLSTART: $12/28/21$ INSPECTOR CLUHL		1	100 <u>1</u> 17 5/		KOLAKT		DRILLERS & EQUIPMENT U.C							
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		•					In Inclusion 12		E HO					
$\frac{340}{340} = \frac{54}{4} = \frac{20 - 4d_{ S }}{20 - 4d_{ S }} = \frac{60}{ V } = \frac{1}{11} \frac{11}{11} \frac{11}{11} \frac{12}{11} \frac{12}{20} \frac{20}{36} \frac{12}{10} \frac{12}{10} \frac{12}{10} \frac{10}{10} 1$	WATER	LEVEL	26. 15	<u> </u>	DATE:			28 31		INSPECTOR CUHL_	_			
$\frac{340}{340} = \frac{540}{4} = \frac{20 - 4d_{ S }}{20 - 4d_{ S }} = \frac{80}{ V } = \frac{1}{11} \frac{11}{11} \frac{11}{11} \frac{12}{11} \frac{12}{20} \frac{20}{30} \frac{12}{10} $	(FT)	s	AMPLE				SOIL DESCRIPTION	50	SC 1	COMMENTS	ŀ			
$\frac{340}{340} = \frac{540}{4} = \frac{20 - 4d_{ S }}{20 - 4d_{ S }} = \frac{80}{111} = \frac{11}{110} = \frac{1}{12} = \frac{3840}{110} = \frac{54844}{110} = \frac{10}{10} = \frac{10}{10$	<u>ب</u>	AL	æ	ΥHX (					YM6					
$\frac{340}{340} = \frac{54}{4} = \frac{20 - 4d_{ S }}{20 - 4d_{ S }} = \frac{60}{ V } = \frac{1}{11} \frac{11}{11} \frac{11}{11} \frac{12}{11} \frac{12}{20} \frac{20}{36} \frac{12}{10} \frac{12}{10} \frac{12}{10} \frac{10}{10} 1$	PAC	NH N	<b>1</b> BE	N N N N N N N N N N N N N N N N N N N	BLOWS	BPF		Hav	SSI SSI	TYPE OF DEPOSIT.				
$\frac{340}{340} = \frac{54}{4} = \frac{20 - 4d_{ S }}{20 - 4d_{ S }} = \frac{60}{ V } = \frac{1}{11} \frac{11}{11} \frac{11}{11} \frac{12}{11} \frac{12}{20} \frac{20}{36} \frac{12}{10} \frac{12}{10} \frac{12}{10} \frac{10}{10} 1$	BEL	NTE	NUN	UNC UNC	6''-6''-6''	"N"		GR/		PROBLEMS, ETC.)				
$\frac{4}{400}$ $\frac{4}{45}$ $\frac{20 \cdot 4}{53}$ $\frac{4}{50}$ $\frac{4}{50}$ $\frac{4}{50}$ $\frac{4}{50}$ $\frac{100}{50}$		50.0		<u> </u>		201		9.0		SLOW, ROUGH DRILLING				
$35  35.0$ $35  35.0$ $35  35.0$ $35  35.0$ $35  35.0$ $35  35.7$ $4  45 - Lo(_{3'})  105/'_{3'}$ $5 = 12  13 - 50 - C''_{3'},  105/'_{3'},  105$		30,9	5-6	4	20-60/5"	0/11	ROUNDED GRAVEL TO AT LEAST	50.0						
$\frac{1}{35} \frac{1}{350} \frac{1}{$	-				1.5	<u> </u>	SAND 5-10% NON PLASTIC FINES,							
$\frac{358}{400} = \frac{5.7}{4} + \frac{45 - 40}{3!} + \frac{105}{6!} +$								0 A 6						
$\frac{358}{400} = \frac{5.7}{400} + \frac{45 - 6q_{31}}{600} + \frac{105}{600} + \frac{105}{600} + \frac{100}{600} + 100$								90			Q			
$\frac{358}{400} = \frac{5.7}{400} + \frac{45 - 6q_{31}}{600} + \frac{105}{600} + \frac{105}{600} + \frac{100}{600} + 100$										-	7			
40 40 40 40 40 40 40 40 40 40	35-					1	SANDY GRAVEL SAME AS 5-6	30	60-	SAMPLER BOUNCES -	N. VIL			
40 400 415 58 12 13-50-63 415 58 12 13-50-63 415 58 12 13-50-63 417 58 12 13-50-63 417 415 58 12 13-50-63 417 417 417 417 417 417 417 417	-		2.7	4	45-60/21	10%				DURING SPT FOR 53-7	Sec.			
40 40 40 40 40 40 40 40 40 40	.				10			000		-				
40 40 40 40 40 40 40 40 40 40								-0	1	CONTRACTOR AND STREET				
40. 40.0 415 5.8 12 13-50-64 10 SILTSTDUE, HIGHLY WEATHERED 415 5.8 12 13-50-64 10 SILTSTDUE, HIGHLY WEATHERED PARTICLES SILTSTDUE, SAME SAUDO, SME SILTSTDUE, UTWOR LAYES - REACHETTS W. M. JUNCH THEK, GRAY, SLIGHTLY MOIST. 45 452 5.9 5 14-60/4 74/0 END BORING AT 45.8 FEET PIEZOMETER INSTALLATION: (SEE NOTES ON BOVING Leg Legend) PIEZOMETER INSTALLATION: (SEE NOTES ON BOVING LOG RACEMENT OF PERVIOUS TIP: TOP AT 33FT, BOTTOM OT 3HSFT GRAVEL PACK: FROM 465FT TO GROUND BODTINITE SENL! FROM 18 TO 20 FEET RISER PIEZ LET GTHS: 35 FEET	-													
$\frac{415}{58} \frac{58}{12} \frac{12}{12} \frac{13.50 \cdot 6g'}{179''} \frac{110}{9''} \frac{110}{10} \frac{110}{10} \frac{51157016}{100} \frac{644}{100} \frac{544}{100} \frac{542}{100} \frac{542}{100} \frac{540}{100} \frac{540}{1$	.									AT 37.5 FT	81 - 14 2 - 14			
45 450 45 450	40-	40.0				1100	SILTSTONE, HIGHLY WEATHERED			. –	÷			
45 450 45 450			5-8	12	13-50-64	110/1	TO SILT AND CLAY-SIZED PARTICLES			_	· 77			
HS USO HS S S S 5 14-60/4 74/0 HS S S S 5 14-60/4 74/0 END BORING AT 45.8 FEET FINGH DRILLING AT IND END BORING AT 45.8 FEET FINGH DRILLING AT IND FINGH DRILLING FINGH DRILLING FI		1415			/3	1.7				,	-			
45 450 458 S.9 5 14-60/4 74/10" SILTSTONE, SAME AS S.8 END BORING AT 45.8 FEET PIEZOMETER INSTALLATION: (SEE NOTES ON BORING LOG Legend) PLACEMENT OF PERVIOUS TIP: TOP AT 33FT, BOTTOM AT 345FT GRAVEL PACK: FROM 46.5 FT TO GROUND BENTONITE SEAL! FROM 18 TO 20 FEET RISER PIPE LETGTAS: 35 FEET PIEZOMETER INSTALLATION: SUPPACE							FRAGNELITS V8-Y4-INCH THICK,			· · ·				
438 59 5 14-60/4 74/0" END BORING AT 45.8 FEET PIEZOMETER INSTALLATION: (SEE NOTES ON BORING Legend) PLACEMENT OF PERVIOUS TIP: TOP AT 33FT, BOTTOM AT 34-SFT GRAVEL PACK! FROM 46.5FT TO GROUND BENTONITE SEAL! FROM 18 TO 20 FEET RISER PIPE LETGTHS: 35 FEET	-	1					GRAY, JLIBHILI MOISI.			-				
438 59 5 14-60/4 74/10 SILTSTOLE, SAME AS S-8 END BORING AT 45.8 FEET FINGH DRILLING AT PIEZOMETER INSTALLATION: (See Notes ON BOVING Legend) PLACEMENT OF PERVIOUS TIP: TOP AT 33FT, BOTTOM AT 34-SFT GRAVEL PACK! FROM 46.5FT TO GROUND SUEFACE BENTONITE SEAL! FROM 18 TO 20 FEET RISER PIPE LETGTHS: 35 FEET										-	1 5			
PIEZOMETER INSTALLATION: (See Notes ON BORING Legend) PIEZOMETER INSTALLATION: (See Notes ON BORING Legend) PLACEMENT OF PERVIOUS TIP: TOP AT 33FT, BOTTOM OT 34SFT GRAVEL PACK! FROM 46.5FT TO GROUND BENTONITE SEAL! PROM 18 TO 20 FEET RISER PIRE LETGTHS: 35 FEET	45-	1					SHITSTONE, SAME AS S-8			_				
END BORING AT 45.8 FEET PIEZOMETER INSTALLATION: (See notes on Boring Log Legend) PLACEMENT OF PERVIOUS TIP: TOP AT 33FT, BOTTOM AT 345FT GRAVEL PACK: FROM 465FT TO GROUND SURFACE BENTONITE SEAL! FROM 18 TO 20 FEET RISER PIPE LETGTAS! 35 FEET	-	45.8	59	5	14-60/4	74/				_				
PIEZO METER INSTALLATION: (See Notes on Boring Log Legend) PLACEMENT OF PERVIOUS TIP: TOP AT 33FT, BOTTOM AT 345FT GRAVEL PACK! FROM 465FT TO GROUND SURPACE BENTONITE SEAL! FROM 18 TO 20 FEET RISER PIPE LETGTHS: 35 FEET				•	2.1	.10			<b>!</b>	FINSH DRILLING AT	i, . Anji			
GRAVEL PACK: FROM 465FT TO GROUND SURFACE BENTONITE SEAL! FROM 18 TO 20 FEET RISER PIRE LETGTHS: 35 FEET							LICE DOKING AT 40.0 TOOT				· -			
GRAVEL PACK: FROM 465 FT TO GROUND SURFACE BENTONITE SEAL! FROM 18 TO 20 FEET RISER PIRE LETGTHS: 35 FEET	-						-	-			· •			
GRAVEL PACK: FROM 465FT TO GROUND SURFACE BENTONITE SEAL! FROM 18 TO 20 FEET RISER PIRE LETGTHS: 35 FEET	-	-			DICTO		lemination. (see notes on B	orina	Log	Legend)				
GRAVEL PACK: FROM 465 FT TO GROUND SURFACE BENTONITE SEAL! FROM 18 TO 20 FEET RISER PIRE LETGTHS: 35 FEET	_	-			PIE EOMET	EK IN	PERVIOUS TIP: TOP AT 33FT. B	DITOM	AT 3	45FT -				
BENTONITE SEAL! FROM 18 TO 20 FEEL RISER PIPE LET GTHS! 35 FEET											100 E			
RISER PIPE LET GTHS: 35 FEET					GRAVEL	PACK:	I EPANN 18 TO 10 FEET							
	-	1												
	-	-			RISER PIP	<u>e lei</u>	GTHS! 35 FEET			-	τ			
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sheet | of 3 project number \$15600, A5

SOIL BORING LÓG

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PROJECT						LOCATION ORE	<u>-60</u>	<u>N C</u>	. <u> T'</u>	OREGON	-	
DRILLIN ELEVATI				<sup>2</sup> mud, cr T	16- ()	5 DRILLERS & EQUIPMENT_D_K				- <u>0 regon</u> Le: <u>B-13</u>		
						START: 12 28 81 FINISH: 12				_INSPECTOR_CWH	-	
,	1	SAMPLE		STANDA		SOIL DESCRIPTION			٦٢	COMMENTS		
(PT)				PENETRAT	TION	COLOR, RELATIVE DENSITY OR	DO1 0	sol	CLASSIFICA- TION SYMBOL	DRILLING PROGRESS,		
DEPTH BELOW SURFACE	NTERVAL	NUMBER	RECOVERY (INCHES)	BLOWS	BPF	CONSISTENCY, MOISTURE, GRAIN SHAPE AND TYPE, STRUCTURE,	GRAPHIC	1ED	I SY	LOST CIRCULATION, TYPE OF DEPOSIT.		
DEPT	NTE	MUM	RECO	6''-6''-6''	"N"	CEMENTATION, ORGANICS, MATERIAL)	GRA	INN	TION	PROBLEMS, ETC.)		
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5-	5.0					SULT LOW TO MEDIUM PLASTIC-		<b>\</b>		r —	-	
-	16.5	5-1	10	1-2-2	4-	SILT, LOW TO MEDIUM PLASTIC- ITY ABOUT 5% FINE SAND,		ř	٩L	-		
-	- 0.5					BROWN, MOIST, JOFT.				- -	3	
-	-											
					1					-	<u>_</u>	
10-	10.0										* `.	
(0			111	- 		SANDY SILT, LOW TO MEDIUM			儿			
-	115	5-2	14	1-1-1	2	SANDY SILT, LOW TO MEDIUM PLASTICITY (5-20% FINE SAND, BROWN NYOIST, SOFT				-		
۰ · ·										-	Ĩ.	
-	13.0					SANDY SILT, SIMILAR TOS-2				-		
	-	ST-I	14									
15-	15.0		· 1			SILT, LOW TO MEDIUM PLASTIC-	$\  \  $					
	16.5	53	12	1-1-1	2	ITY, 5-10% FINE SAND, BROWN,		M	L	-		
-	-					MOIST, SOFT.		<u>-</u>		-	-	
-	4					-				· · · ·		
											. 3	
20-	20,0											
00-		5-4	18	1-1-1	2	SILT, LOW TO ME DIUM PLASTICITY ABOUT 5% FINE SALD, BROWN,	111	۸ III	イレ	_	·	
	215			1		MOIST, SOFT.			<del>،</del>			
	1									*a*		
	-									-		
	-	ι								-	-	
25-	25.0					UPPER & INCHES; SILT, SAME AS			11	D011160	· · ·	
	26.5	5-5	10	2-11-28	39	LOWER HINCHES: SILTYSAND, FINE		<u> </u>	Μ	DRILLER NOTES GEAUEL AT 26FT, -		
	-	<u>.</u>			and a second	TO MEDIUM SAND, 20-25% SLIGHTLY PLASTIC FINES, BROWN, MOIST,	100			~	·****	
-	1					DENSE.	00	о- - А		TO 47,5FT,		
	an a						DD			1 1, 21, 11	- Hennes	
75		***	****			D18	20				-	
- 30	1		i	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	<u></u>		Carl and and	·1.11		FORM D 1586 5/75	1	

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<u>sheet</u> 2 of 3 PROJECT NUMBER PI5600, A5-

PROJECT TRICITY STP		EGON CITY, OREGON
DRILLING METHOD ROTARY MUD, C	ME-75 DRILLERS & EQUIPMENT D. C	LENNER OF OREGON
WATER LEVELSEE TEXT DATE:	START: 12/28/81 FINISH: 12	29/81INSPECTOR_CWH
(FT) SAMPLE STANDA		OCOMMENTS
HLDWS HLDWS	ILTS (COLOR, RELATIVE DENSITY OR CONSISTENCY, MOISTURE, GRAIN SHAPE AND TYPE, STRUCTURE, CEMENTATION, ORGANICS, "N" MATERIAL)	OUN (DRILLING PROGRESS, LOST CIRCULATION, TYPE OF DEPOSIT, PROBLEMS, ETC.)
30 30.0 5-6 4 41-60/4"	101/ SANDY GRAVEL, POORLY GRADED, 10" ROUNDED GRAVEL TO AT LEAST 14 INCH, 10-15% FINE TO MEDIUM SAND, 5-10% NON TO SLIGHTLY	GP- GM
35 350 .	PLASTIC FINES, BROWN, VERY MOIST, VERY DENSE.	
35.5 5-7 4 56/6"	56/ # SAME AS 5-6	GM GM
40-40.0 40.4 5-8 1 69411	60/ SAME AS S-7	
45-453-5-9 0 401-4	60/ NO RECOVERY	
45.3 5-9 0 60/3"	<u>/3</u> <sup>h</sup>	DRILLER NOTES END.OF GRAVEL AT 47,5 FT.
50 50.0 50. A 5 -10 6 43-60/2"	103/ 78" TO SILT AND CLAY SIZED PARTICLES, WITH 10-15% T.NE SAND AND GRAVEL, BLIE-	1-2INCH POUNDED
55 55.0	GREEN WITH ORANGE -BROWN MOTTLING, SLIGHTLY MOIST, SILTSTONE, HIGHLY WEATHERED TO SILT AND CLAY SIZED PARTICLES	SAM PLER FOR ST-10
- 36.5 S-11 15 25-46-64/3"	106/ 106/ 106/ 106/ 106/ 107/ 108/	FINISH DRILLING AT
66°	D19	FORM D 1586 5/78

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# P15600, A5

PROJECT		CIT	Y S	TP			LOCATIO	N 08	PGON	CIT	Y DREGON	
DRILLIN	G METH	iop Ro	TAR	Y MUD, CN	E -75		S & EQUIPMEN	T_D,K	ENNE	R OF	OREGON, INC.	-
ELEVATI		38,8	7 Fe	ET					BOR	E HOI	LE: 6-13	-
WATER	LEVES	E TE	TXE	DATE:			81 FINISH	: _12/:	29   8	1	INSPECTOR CWH	
(FT)		AMPLE		STANDA	<u></u>		ESCRIPTION		LOG		COMMENTS	
DEPTH BELOW SURFACE	INTERVAL	NUMBER	RECOVERY (INCHES)	PENETRAT TEST RESU BLOWS	BPF	(COLOR, RELAT CONSISTENCY, SHAPE AND TY CEMENTATION,	MOISTURE, GRA PE, STRUCTURE	UN	RAPHIC	UNIFIED SOIL CLASSIFICA TION SYMBOL	(DRILLING PROGRESS, LOST CIRCULATION, TYPE OF DEPOSIT, PROBLEMS, ETC.)	-
<u>S B D</u>	<u> </u>	z	@=	6''-6''-6''	"N"	INSTALLATION	. (so notes	on R	O	100	Legenia)	· ··· •
	-			PIEZOME		OF PERVINUS	TIP' TOP AT	385	ET 8	BOTT	MAT 40.FT	-
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					-	SEAL! FROM		<i>⊷</i> 1,				`
	]			RISER	PIDE	LENGTH: 4	OFT.					
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P15600, A5

SOIL BORING LÓG

PROJECT				STP	· · · · · · · · · · · ·	ETRICONZBITORILLERS & EQUIPMENT D. KENNER CME -75						
ELEVATI		400 <u>100</u> 44.70			LEETK	CONE DI DRILLERS & EQUIPMENT U. K				LE: B-14		
		SEE TE	XT_I	DATE: 52	1182					INSPECTOR CUIH		
· (FT)	5	SAMPLE		STANDA		SOIL DESCRIPTION		1001	01L 30L	COMMENTS		
ů, ů,	VAL	R	ERY (S)	TEST RESU		(COLOR, RELATIVE DENSITY OR CONSISTENCY, MOISTURE, GRAIN			ED S	IDRILLING PROGRESS, LOST CIRCULATION,		
DEPTH BELOW SURFACE	NTERVAL	NUMBER	RECOVERY (INCHES)	BLOWS	BPF	SHAPE AND TYPE, STRUCTURE, CEMENTATION, ORGANICS,		GRAPHIC	UNIFIED SOIL CLASSIFICA- TION SYMBOL	TYPE OF DEPOSIT, PROBLEMS, ETC.)		
0.82	2	ž	RE (1)	6''-6''-5''	"N"	MATERIAL)	$\frac{1}{1}$	ຜ່ T∏T	305	START DRILLING AT		
.	-								2	9:40		
	2.5				•					-		
	4.0	5-1	4	2-1-1	2	SILT LOW PLASTICITY, ABOUT 6-10%			ML	-		
	5.0							-		· -		
5 -	2.0	S-2	7	1-1-1	2	SANDY SILT SIMILAR TO S-I, EXCEPT IT GRADES INTO A SILTY SAND			ML	DRILLER NOTES - ALTER NATING SOFTER		
	65	3-2	1	1-1-1		WITH 30-50% FINE SAND TOWARD BOTTOM.	`			E FIRMER DRILLING - 5-10 FT.		
	7.5					SILTY SAUD FINE SAND, 20-25%	Щ					
	9,0	S-3	5	2-3-4	7	SILTY SAND, FINE SAND, 20.25% FINES WITH LOW PLASTICITY, BEAUN, WET, SOFT TOFIRM,			SM			
10-	10.0											
	115	5.4	7	2-1-1	2	SILTY SAND, SIMILAR TO S-3. EXCEPT WITH 30-35% FILES			SM	-		
				· · _ · · · · · · · · · · · · · · · · _ · / /		WITH LOW PLASTICITY	. <u>₹</u> .11			MLISAT VERY		
	13.5	ST-5	2.4			SILT, LOW PLASTICITY, ABOUT 10% FINE SAND, BROWN, WET, SOFT.			ML	BOTTOM OF ST-5		
										-		
15-	15.0					SANDY SILT LOW PLASTICITY						
	16.5	5-6	5	3-2-4	6	ABOUT 20% FINE SAND, DAR'S BROWN, MOIST, FIRM			ML			
-	-								·	-		
	]			-						_		
· ·	20.0											
20-	10.0	0 -	L		х л	UPPER 2" SILT LOW PLASTICITY			ML	•		
-	21.5	S-7	6	3-22-22	44		Ш	III	SM	DEILLER NOTES		
	-					LOWER 4"; SILTY SAND, FINE TO MEDIUM SAND, ABOUT 15% FINES				GRAUEL AT 215 FT.		
	].					BROWN, WET, DENSE.						
25-	250									CANNOL ON ROUNTET		
	25.5	5-8	4	60/5%	50/	GRACELLY SAND, POORLY GRACED, 25,30% SUBROUMED			SP-	SAMPLER BOUNCED		
	and the second		*	15/2	15/2	GRACED, 25 30% SUBRAINCED GRAVEL TO ATLEAST 14 INCH, FINE TO COARSE SAND, MOSTLY				075-8		
						COARSE, 5-10% FINES, BROWN, WET, DENSE.				SLOW, ROUGH, DRILLING		
						YYEI) DENVE.				TO 30FT		
-	1					D21		***** *****				
										FORM D 1586 5/70		

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CH2M HILL									15600.A5
l	]					SOIL BORING	G LÓ	G	
PROJECT	r_ <u></u> RI	<u>C</u> 1	ry :	STP		LOCATION OR	EGOI	V CI	TY. OREGON
		100 RC			TAILÉ	RICONE BRILLERS & EQUIPMENT D			
ELEVATI WATER				DATE: 5/24	182				LE: B-14 INSPECTOR CWH
(ET)	S	SAMPLE		STANDA		SOIL DESCRIPTION	100		COMMENTS
CE V	VAL	E H	/ERΥ ES)	TEST RESU	JLTS	(COLOR, RELATIVE DENSITY OR CONSISTENCY, MOISTURE, GRAIN	1	ED S(	DRILLING PROGRESS,
DEPTH BELOW SURFACI	NTERVA	NUMBER	RECOVE	BLOWS	BPF	SHAPE AND TYPE, STRUCTURE, CEMENTATION, ORGANICS,	GRAPHIC	UNIFIED SOIL CLASSIFICA- TION SYMBOL	TYPE OF DEPOSIT, PROBLEMS, ETC.)
30	= 30,0 30,9	2			92/	MATERIAL) SANDY GRAVEL WELL GRADED	30		SLOW ROUGH DRILLING
		2-1	5	32.69/5.	11"	ANGUL AR AND SUBROUNCED GRAVEL TO ATLEAST 20-25% FINE TO	0.0	6P	
						COARSE SAND, LESS THAN 5% FINES, BROWN AND BLACK, WET DENSE.	0.0		· .
	-								
35-	35.0			35 1 1	051	SANDY GRAVEL, SIMILAR TO 5-9	0		DRILLER POUNDE P
	35,8_	5-10	2	35-60/4/2	10/2	BUT TOO LITTLE RECOVERY TO PROVIDE A THOROUGH DESCRIPTION.	<b>.</b>	GP	CRILLER POUNDED. SAMPLER DOWN SFT. TO GET IT IN ROSITION JO ROSEDE SAMPLES - DO
	-						9.0		SOME OF SAMPLES -10 MIGHT BE CAULTY -
	-						Jo°,		LOSE CIRCULATION AT -
40	40.0						° D D D 0 0		SLOW, ROUGH DRILLING-
	41.2	5-11	8	25-31-60/2%	91/	SANDY GRAVEL, SAME AS 5-9		GP	LOST CIRCULATION AT 42 FT, MIX MID SLOVE-
	-			120	1012		90.0		ROUGH DRILLING TD
	-					-	0.U.o		4()-1.
						•			
45-	45.0	5-12		60/211	60/31	NO RECOVERY			SAMPLER BOUNCES IN-
	-			CI	13	-	90		OF 5-12
									DRILLER NOTES END OF GRAVELLY MATERIAL AL
	-								47 FT
50-	50.0					SILTSTONE, HEHLY WEATHERED, FRAC		-	
	51,5	S-13	18	22-41-36	77	TURES INTO ANGULAR, BLOCKY, PIECES ABOUT Y4"ON A SIDE,			
	1					CONTAINS ABOUT 10% FINE SAND, AND LOCAL PECES OF THOROUGHLY			FINISH DEILLING AT
	-					WEATHERED GRAVEL TO ~ 12 INCH; GRAY W/BILLE - GREEN MOTTLING			- 1
						AT TOP, MOIST.			
	_			PIEZO INI	STALL	ATTON: (see wotes on Boving	Log	Leger	
	-			VIN GAL	ATT /	FROM 51.5 FEET TO GROUND	1,00	11 61 41	
	-			BENTCHI	TE SE	INL! FROM 15,5 to 17.5FT, AND	FROM	ABC	IT TO OFEET
	-			REER F	IPE D	MENSIONS 40 FEET			ter series and series a
	1					D22			FORM D 1588 5/70

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HILL

SHEET OF

P 15600, A5

PROJECT					mand	LOCATION OREGON CITY, OREGON								
					TAIL	BIT DRILLERS & EQUIPMENT D. KENNER OF OREGON.								
ELEVATI WATER	ON	46,6	<u>9 FI</u>	, 		BORE HOLE: B-15								
							s. Santa Santa							
(FT)		SAMPLE		STANDA PENETRAT TEST RESU	TION									
ACE	AVF	ЗЕА	VER (ES)	BLOWS	BPF	COLOR, RELATIVE DENSITY OR CONSISTENCY, MOISTURE, GRAIN SHAPE AND TYPE, STRUCTURE, STRUC								
DEPTH BELOW SURFACE	INTERVAL	NUMBER	RECOVERY (INCHES)	6"-6"-6"		Image: Color, Relative Density OR       O								
		2.	<u></u> щ~-	8-0-0	14	START DRILLING AT								
-	-					3:35 -								
	2.5						10.53							
		<b>C</b> )		2-2-2	4	SILT LOW PLASTICITY, 10-15% ML								
.	4,0	5-1	5	2-2-2	-		W.S.							
5-	5.0						-							
	6.5	5-2	8	1-2-2	4	SANDY SILT, LOW PLASTICITY, ABOUT								
				·		LOOSE, SCHIE ROOTS PRESENT								
	30													
						SANDY SILT, SIMILAR TO S-2	and a second							
	10.0	ST-3	24-											
- 01		5.4		5 7 7	· _	SANDY SILT LOW PLASTICITY, ABOUT 15% FINE SAND, DARK BROWN, MOIST, SOFT TO FIRM,								
-	11.5_	5-7	5	2-2-3	5	ABOUT 15% FINE SAND, DARK BROWN, MOIST, SOFT TO FLOM.								
-	-						10 <sup>0</sup>							
							4							
15-	15.0					SILT LOW TO MEDIUM PLASTICITY								
	16.5	S-5	7	2-2-3	5	LESS THAN 5% FINE SAND BROWN, WET, SOFT TO FIRM								
.	-													
	-													
	-													
30-	20.00		L				·							
		5-6	10	2-3-4	7	SANDY SILT LOW PLASTICITY 35-42 ML	8							
	21.5					- FIRM								
	]													
	-													
	10= 0													
25-	25.0			-		UPPER 9": SAND UNIFORMULY GRADED, FINE SAND, 5-12% FINE SP.SM WITHLOW PLACTOR THE BROWN WET								
	26.5	S-7	12	8-19-58	77	WITHLOW PLACTO ITT, BROWN, WET								
	~					LOWER 3": SANDY GRAVEL, WELL FINISH DRILLING AT-								
	-		5-2-4-4			FINE TO COARSE SAND, LESS THAN 5%								
						END BORING AT 26.5FT								
				4		D23								
						FORM D 1586 5/78								

-Link d					[	PROJECT NUMBER
CH2M ∎HILL						P15600.A5
						SOIL BORING LÓG
RILLING	G METI	CITY 100_R 400.7	DTARY	MUD FISH	TAIL	BIT DRILLERS & EQUIPMENT D.KENNER OF CLEGON BORE HOLE: B-16
				DATE:		START: 5/19/82 FINISH: 5/19/82 INSPECTOR CWH
се (1-				STANDA PENETRA TEST RES	TION	SOIL DESCRIPTION     O     I     I     COMMENTS       (COLOR, RELATIVE DENSITY OR CONSISTENCY, MOISTURE, GRAIN SHAPE AND TYPE, STRUCTURE, CEMENTATION, ORGANICS, MATERIAL)     O     I     I     I     IO     IO <td< td=""></td<>
DEPTH BELOW SURFACE	INTERVAL	NUMBER	RECOVERY (INCHES)	BLOWS 6"-6"-6"	BPF-	
-				•		- START D'RILLING AT
-	25	S-1	7	2-2-1	3	SILT LOW TO MEDIUM PLASTICITY ML
5 -	5.0					
	6.5	5-2	9	1-1-2	3	SILT, SIMILAR TO S-I, EXCEPT WITH 5-10% FINE SAND
	7.5 9.0	5-3	12	1-1-1	2	SILT LOW TO MEDIUM PLASTICITY, ABOUT 10% FINE SANG ML DARK BROWN, MOIST, SCFT,
10 -	10.0					
.0	12.0	ST-4	24		-	TSANDY SILT, LOW PLASTICITY 18% FINE TO MEDIUM SAND, MOSTLY FINE 65% SILT, 17% CLAY, MOIST, SOFT.
	13.5	S-5	18	- -	2	SILT SIMILARTOS-I, EXCEPT ABOUT 5% FINE SAND
Б-	15.0					
-	16,5	5-6	18	1-1-2	З	SILT, LOW PLASTICITY, DARK BROWN, MOIST, SOFT
-						
- 20	20.0		****			SANDYSILT LOW PLASTICITY, 15-
	21.5	5-7	12	2-2-1	3	20% FINE SAND, BROWN, MOIST, ML
-	0.5					
25-	25.0	5-8	5	7-7-8	15	SAND, UNIFORMLY GRADED, FINELILLI SP- TO MEDIUNI SAND, MOSTLY FINE, 5-12% SM FINES, BROWN, MOIST, COMPACT SM DRILLER NOTES
-	<u>27.5</u>	5-9	·")	41-696"	101/ ,,	SANDY GRAVEL, POORLY GRADED
2	25.5	5-7		1	/12"	FINE TO COARSE SAND, S-129, FINES, FI

SHEET OF 2 P15600, A5

SOIL BORING LÓG

PROJECT	TRI	CIT	Y 5	TP		LOCATION_	DR	<u>560</u>	IN CI	TY. OREGON
					TAILS	RICONE DRILLERS & EQUIPMENT 1				<u>de Okegon</u> Le: <u>B-17</u>
ELEVATI WATER		40.5' NOT MEAG						20/2		INSPECTOR CWH
(Ft)	T	AMPLE		STANDA						COMMENTS
	AL	~	ЧЧ	PENETRAT		COLOR, RELATIVE DENSITY OR			UNIFIED SOIL CLASSIFICA- TION SYMBOL	(DRILLING PROGRESS,
DEPTH BELOW SURFACE	NTERVAL	иОМВЕЯ	RECOVERY (INCHES)	BLOWS	BPF	CONSISTENCY, MOISTURE, GRAIN SHAPE AND TYPE, STRUCTURE,		GRAPHIC	ASSIE N S'	LOST CIRCULATION, TYPE OF DEPOSIT,
DEP BEL SUF	INT	ΪΩ	REC	6''-6''-6''	"N"	CEMENTATION, ORGANICS, MATERIAL}		GR	10 L	PROBLEMS, ETC.)
										START DRILLING AT 8:45
					]					
					Î		Ì			]
5-	5.0						a l			
5-		5-1	5	1-2-2	4	SILT LOW PLASTICITY A BOUT S FINE SAND, BROWN, WET, SOFT	0		ML	
	6.5		)		,	FIRM.	Í			
	]									
	]							<i> </i>		
10-	10.0						Í			
10-		S-2	12	1-1-1	2	SANDY SILT, LOW PLASTICITY, 25-30% FINE SAND, BROWN, WE	T,		ML	
-	111.5	2-2		1-1-1	4	50FT.	Í			-
-	13.0									
-	10.0					SILT LOW TO MEDIUM PLASTICIT	rY,			-
	15.0	ST-3	24			6% FINE SAND, 73% SILT, 21%. CLAY, BROWN, SOFT,			ML	-
15-						SANDY SILT, SIMILAR TO S-2, EXCEPT WITH 20-25% FINE, SAND.			ML	
	16.5	5-4	18	1-1-1	2	SAND.			-	-
-	18.0									
	1010			ŧ		SANDY SILT SIMILAR TO 5-2, EXCEPT WITH 10-15% FINE			ML	
	20.0	ST-5	24			SAND.			.   .	
20-						SANDY SILT SIMILAR TO 5-2, EACEFT WITH 10-15"'S FINE SAN	a	{	ML	PRILLER NOTES SLIGHT
-	215	S-6	15	1-1-1	2	ENCERT WITH TO TO IS FINE OTH				20-23 FT.
	22 M									
	23.0					SANDY SILT, SIMILAR TO S - 2				+
	DEA	ST-7	20			EXCEPT WITH 10-20% FINE			ML	
25-	25.0					SANDY SILT SIMILAR TO 5-2,				Ĭ
	26.5	5-8	18	3-2-2	4	EXCEPT WITH 15.30% FINE SAN AND ORANGE - BROWN MOTTLING	ND,		ML	
	-					IN LOWER 6 INCES				
	-						anna anna ann ann ann ann ann ann ann a			1
Valense Konne-o	-		****			D25	N. Car		Ð	BRILLER NOTES GRAVEL AT 29FT.
30-	1 1 1 P = 100 P = 10 P						E	0.0	2.	FORM D 1586 5

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						,			SHEET 2 OF	
CH2M							ę		T NUMBER 5600, A5	-
	•					SOIL BORING	G LÓC			
PROJEC	τ <u></u> ΓŔ	21 C	ITY	STP		LOCATION DRE	GON	CIT	Y, OREGON	[-
	IG METH	IOD ROT	ARY	MILD, DRAG	EROLLE	R BITS DRILLERS & EQUIPMENT D. K	ENNE	ROF	OREGON	
ELEVAT	ION	40.57 NOT	2 <u>F</u> E	ET			BORE	E HOI	LE: B-17	
WATER	LEVEL								INSPECTOR CLUH	
(FT)		AMPLE	X	STANDA PENETRAT TEST RESL	ION	SOIL DESCRIPTION	1.06	SOII CA- MBD	COMMENTS	
NCE SW	NTERVAL	BER	N EF HES)	BLOWS	BPF	(COLOR, RELATIVE DENSITY OR CONSISTENCY, MOISTURE, GRAIN SHAPE AND TYPE, STRUCTURE,	GRAPHIC	ssifi sylfi	LOST CIRCULATION, TYPE OF DEPOSIT,	
DEPTH BELOW SURFACE	INTE	NUMBER	RECOVERY (INCHES)	6"-6"-6"	"N"	CEMENTATION, ORGANICS, MATÉRIAL)	GRA	UNIFIED SOIL CLASSIFICA- TION SYMBOL	PROBLEMS, ETC.)	÷
30	30.3	5-9	M	60/311	60/ 1311	SANDY GRAVEL, POORLY GROUEL, SUBANGULAR GRAVEL TO AT EAST 194 (NXH, 12-15% FINE TO		GP- GM	SLOW, ROLLAN DRILLING TO 465 FT.	2. 19 <sup>1</sup> 5 19 <sup>1</sup> 5
	-					COARSE CAND, S-10% FINES, BROWN AND BLECK, WET, DELSE				r Sa - E
35-	35.0								DRILLER NOTES SLIGHTLY SOFTER DRILLING AT 35 FT, PROCABLY A SAND LENS, HE THINKS -	
- 62-	35.5	S-0	5	69512"	60/	SANDY GRAVEL, SIMILAR TO S-9 EXCEPT FOR 35-40% FINE TO COARSE SAND,	)	GP- GM	LENS, HE THINKS -	
and a second	-								LOSE CIRCULATION AT 38FT, MIX MUD	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1
46	400	5-11	5	الما الما	.56/	SANDY GRAVEL, SIMILAR TO S-9, EXCEPT FOR 20-25% FINE TO COARSE SAND	9 0 q 0 q	6р- 6М	LOSE CIRCULATION AT	
- 	-						0.4		AZET, MIX MUG' DEILLER THINKS GROUNOWATER IS DILUTING MUD MUXTURE.	
45_	45.0			-			0%		DRILLER NOTES	1 10 10 10 10 10 10 10 10 10 10 10 10 10
	45.1	5-12	0	60/ Y2"	GO/ 1/2	NO RECOVERY			BOTTOMOE GRAVELAT 465 FT.	
	47.5	Ś-13	11	29-60/5/12"	<i>89/_</i> 11	SILTSTONE, WEATHERED, FRACTURES				
50	-				11/2	ALMOST Y4INCH ON ASIDE, BLUE- GREEN, MOIST,			-	м ма т
	-								_	
	- 52.5					ACCIZEV/FUT			-	2
	53.5	5-14	11	16-5461	75/ 12"	SILTSTONE, SAME AS S-13 EXCEPT CONTAINS THOROLGALY WEATHERED PEBBLES (COARSE SAND) WEATHERED TO BLUE GREEN YELLOWAND REDDISH			DM-1515A 2 NCH -	er C
				-		BROWN, SILTSTONE IS ELUE GREEN IN UPPER 4 INCHES, GRAY IN LOWER TINCHES			HOLE HAMMER WAS -	
and an address in the second	57.5								AFTER A SINCH PRIVE - BECALLSE OFCAVING, -	-
numbh vela weeke o	158.0	DM-15	0	82/5"	52/5"	END BORING AT 58.0 FT.		* 	ν-ηγουματογογιατικό πολλογιατικό ματοβουρβουρβουρβουργογγαγιατικό για το ματοβουρβουργαρικό ματοβοργατικό ματο Τ	
every-vector or university						D26			-	

SHEET OF

P15600.A5

SOIL BORING LÓG

1	PROJECT						LOCATION OREGON CITY, OREGON	
1	DRILLIN		HOD <u>KC</u> 44.14		MUD EET		DRILLERS & EQUIPMENT D. KENNER OF OREGON BORE HOLE: B-18	
. with	WATER	LEVEL	NOT METSU	RED_C	DATE:		START: 5/19/82 FINISH: 5/19/82 INSPECTOR CWH	
A for realizing a	DEPTH BELOW SURFACE (1	NTERVAL	NUMBER	RECOVERY (INCHES)	STANDA PENETRAT TEST RESI BLOWS	TION	SOIL DESCRIPTION     O     J     J     COMMENTS       ICOLOR, RELATIVE DENSITY OR CONSISTENCY, MOISTURE, GRAIN SHAPE AND TYPE, STRUCTURE, CEMENTATION, ORGANICS, MATERIAL)     O     J     COMMENTS       ICOLOR, RELATIVE DENSITY OR CONSISTENCY, MOISTURE, GRAIN SHAPE AND TYPE, STRUCTURE, CEMENTATION, ORGANICS, MATERIAL)     O     J     COMMENTS	
1 canora	SUI	INT	NU	R R	6''-6''-6''	''N''	CEMENTATION, ORGANICS, 250 PROBLEMS, ETC.) MATERIAL	
		2,5					9:45	
		4.0	5-1	b	2-2-2	4	SILT LOW PLASTICITY, 5-10% FINE	
	5-	50	<u> </u>	~			SANDY SILT, LOW PLASTICITY, 10-	
		6.5 7.5	5-2	5	- -			
No.		9.0	5-3	5	1-2-2	4	SILT, LOW PLASTICITY, ABOUT 5% FINESAND, DARK BROUN, MOIST, ML FIRM.	•
	10 -	10.0 12.0	ST-4			-	SILTY SAND, 53% FING TO MEDIUM	ž
3		13,5	S-5	2	3-2-2	4	SILT, SAME AS S-3	
!	15 -	15,0			**····		SILT SIMU AR TO S-2 PY PPT NO	
and a state of the		16.5	5-6	8	2-2-3	5	SILT SIMILAR TO S.3, EXCEPT NO ML	
S.S.		20.0						
4		- 21.5	5.7	٦	3-5-3	8	SILT LOW FLASTICITY, ABOUT 5% ML FINE SAND, BROWN, MOIST, FIRM, ML DR!LLER NOTES	
		-					FIRMER DRILLING - 20-25 FT.	
	25	250	5-8	6	3-3-5	8	UPPER 3 INCHES; SILT, SAME AS ML S-3 LOWER 3 INCHES; SILTY SAND, FINE	
		27.5					SAND, 5-12% FINES, DARK BROWN, 1111 PRILLENNOLES, AT 27.5 FT.	
	eré waya sa na kara ang	-	5-9	5	60/4.5	60/4.5"	SILTY GRAVEL DOOPLY GRADED GRAVE TO GANE TO GANE TO AT LEAST I VAINCY, 10-15% SANL OF GM TO AT LEAST I VAINCY, 10-15% SANL OF GM TO AT LEAST I VAINCY, 10-15% SANL OF GM PLASTICITY COMPACT FINISH DRILLING AT END D27ING AT 29.0 FT 10:45	ett i
	1	<u>i</u>			Śrewsze		FORM (0 1526 5/79	

CH2M HILL CH2M HILL

SHEET | OF 2 PROJECT NUMBER PI5600,A5

<u> </u>											
PROJECT						LOCATION_DR					-
DRILLIN ELEVATI	G METH	4159		Y 'WAT	<u>= K</u>	DRILLERS & EQUIPMENT D.					D C
							5/a	80F 14 8	E HU え	LE: <u>B-21</u>	-
1	<u> </u>	SAMPLE	·	STANDA		SOIL DESCRIPTION					Ĩ
(FT)				PENETRAT TEST RESU	ION	COLOR, RELATIVE DENSITY OR	-	C LOG	SO! ICA-	IDRILLING PROGRESS,	-
TH PW FAC	NTERVAL	NUMBER	ÓVEI HESI	BLOWS	BPF	CONSISTENCY, MOISTURE, GRAIN SHAPE AND TYPE, STRUCTURE,	ļ	GRAPHIC	SSIF SSIF	LOST CIRCULATION, TYPE OF DEPOSIT,	
DEPTH BELOW SURFACE	INTE	NUN	RECÓVERY (INCHES)	6''-6''-6''	''N''	CEMENTATION, ORGANICS, MATERIAL)		GRA	UNIFIED SOIL CLASSIFICA- TION SYMBOL	PROBLEMS, ETC.)	
		•					1		1	START DRILLING AT	2 - 2 -
-							ì			DRILLTO 8FT WITH	-
-	-			~			a anti-			WATER, CIRCULATED	×.
-	-									SOME WATER INTO	-
	1						A			SET 5 IN I.D. LASING TO 3 FT, THEN	
5-	<b>_</b>						Ì			PRILLED TO LOFT	· · · ·
-	-									FALLING HEAD PERMEABILITY TEST	
							ľ			H PERFORMED WHAT	1
-	-		·							8 TO LOFT ASTEST	- - -
										INTERVA-	- `
10_	10.0					SANDY SILT, SAME AS 5-2					
		ST-1	24			(SEE BELOW)			ML	-	
-	12.0					SANDY SILT, LOW TO MEDIUM				-	_
	13.5	S-2	15	1-1-1	2	PLASTICITY, 20-25% FINE SAND, DARK BROWN, WET, SOFT.			ML	-	
						DALL CROWN, WE 1, SOF				DRILLED TO IS FEET	
15-							ł			CASING AT ISFEET, THEN DRILLED TO 20PT.	-
-	-									FALLING HEAD	1 a
-	1						ł			PERMEABLITY TEST = #2 PERFORMED WITH	<u>.</u>
				(						18 TO 20 FT AS -	4.
-	-									TET INTERVAL	-
20-	20.6					UPPER PART: SAME AS S-2				DRILLER NOTES ABOUT	-
-		57-3	24			LOWER PART: SAME AS 5-4	Ļ		ML	SINCHES OF SLOUGH SETTLED ON BOTTOM -	
	22.0	3.0				SILTY SAND, FINE SAND, 15-20%			SM	OF HOLE DURING	-
-	A3.5	S-4	12	5-7-7	14	FINES WITH LOW PLASTICITY, MORE FINES TOWARD TOP OF			SM	DRILLED TO 28 FT -	
	Q					SAMPLE, DARK BROWN, WE I				WITH WATER, NO LOST CIRCULATION AT 28FT	
25-	Ļ					COMPACT.				WHEN BIT SNCOUNTER GRAVEL.	
	-										
-									1	SCRILLER, NCTES VERY - SCRIMATE 26.5. TO	
types and the second seco	_								1	28 FT. DRILLER NOES GEAVEL	
							C	) : c	GP	AT 25 FJ SET CASING TO 20 FT, PERMEABILITE TEST 344 FROM 28 to	
30						Dog	1	, € , ₽ (		TEST 344 FROM 28 to 30 FT.	
30-	1	ll	L	**************************************	ş	D28		Juin the second	}	FORM D 1586 5/75	

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SHEET 2 OF 2 P15600,A5

SOIL BORING LÓG

PROJECT TRI CITY STP LOCATION OREGON CITY, OREGON DRILLING METHOD ROTARY, WATER DRAG BIT DRILLERS & EQUIPMENT D.KENNER OF OREGON CHE-75 ELEVATION 41.58 FEET BORE HOLE: B-21

WATER LEVELSEE TEXT DATE:

START: 5/24/82 FINISH: 5/24/82

\_INSPECTOR CWH

(FT)	S	SAMPLE		STANDA		SOIL DESCRIPTION	LOG	OL OL	COMMENTS	
	AL	~ ~	s)	PENETRAT TEST RESU		COLOR, RELATIVE DENSITY OR		P SC YMB	DRILLING PROGRE	
TH	INTERVAL	NUMBER	OVE	BLOWS	BPF	CONSISTENCY, MOISTURE, GRAIN SHAPE AND TYPE, STRUCTURE,	GRAPHIC	FIEI (SSII N S	LOST CIRCULATION TYPE OF DEPOSIT, PROBLEMS, ETC.)	ч <b>.</b>
DEPTH BELOW SURFACE	INT	NUN	RECOVERY (INCHES)	6''-6''-6''	"N"	CEMENTATION, ORGANICS, MATERIAL)	_	UNIFIED SOIL CLASSIFICA- TION SYMBOL	PROBLEMS, ETC.)	1
30	30.0	55		693"	101	NORECOVERY	00			
	1		0	- 13	60/3"		0.0	GF		
	-					END BORING 30.5 FT			FINISH DRILLING	5 <del> </del>
	- ,									-
	-			PIEZOM	ETER	INSTALLATION !				-
35 -				PLACE	MEN	OF PERVIOUS TIP: TOP AT 28	SFT,	8077	MAT 20.FT	-
	1			GDAVE	I PAC	K: FROM 31 5 FT TO GROUNE	SUR	LFACE	-	-
	-			BENTO	NITE	SEAL: FROM 24.7 TO 26.7	FT			-
	_					LENGTH: 30 FT				
	-									-
-										_
	_				•					_
	~									-
	]					· _				
	]							ĺ		
-			i.						×	7
									- <u>-</u>	
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	-					-				-
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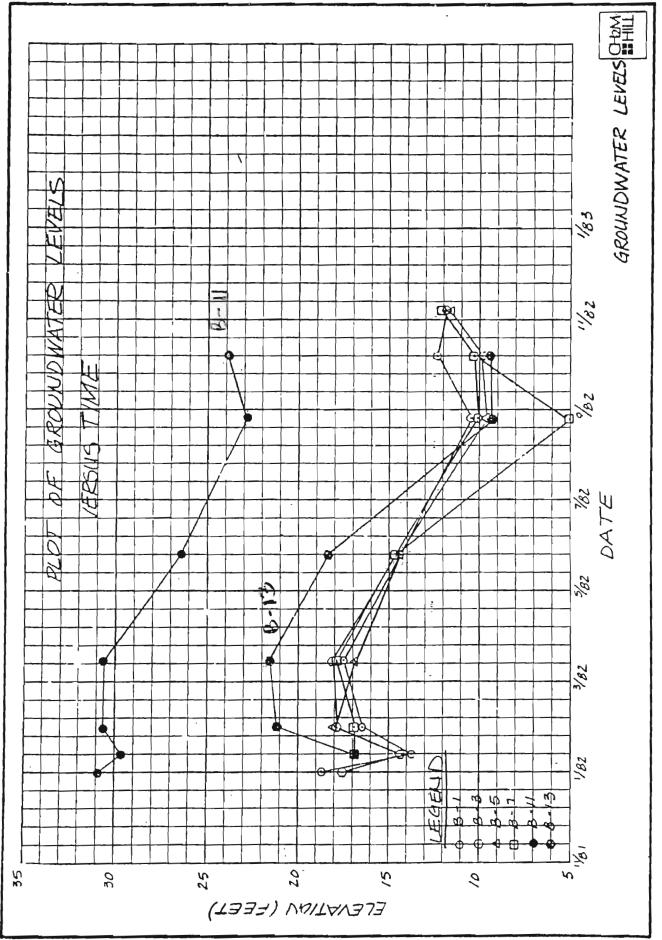
SUMMARY OF GROUNDWATER LEVELS (ELEVATIONS IN FEET)

12/23/81 12/20/81 12-29-81 1-11-82 1-12-82 1-13-82 2-2-82 3-12-82 5-24-82 8-26-82 10-7-82 11-8-82 12.0 Lill 1.1 0:21 6.11 J 2 2 9.4 23.8 12.4 10.3 10.3 6.6 2 9 22.8 17.5 14.4 10.4 10.1 5.0 6.3 3.6 م ٩ \* READINGS WERE TAKEN WITHIN 24 HOURS AFTER PIEZOMETER WAS INSTALLED. 22.7ª 14,4 26.4 18.4 18.1 14.6 14.9 14.60 PIEZOMETER 6.11 21.4 6.91 30,7 1 1 21.2 16.5 14.4 14.3 17.8 26.04 17.9 16.5 30.7 1 DATE b NID WATER LEVEL MEASURED IN 13.7 16.91 18.3 L.62 1 1 20.54 30.0 ウ・レー 13.7 1 13.60 13.6 15.2 29.5 1 ï 1 1 4.11 30.8 18.7 4 1 32,0ª 18.6 17.8 1 1 19.5 a 34.3 0 1 1 1 ١ NOTE: BORING NUMBER 8-14 12-8 B-13 6.9 8-5 2-9 11-8 1-8

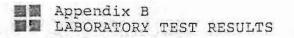
Char Hill

C. PIELOMETER DESTROYED.

D30



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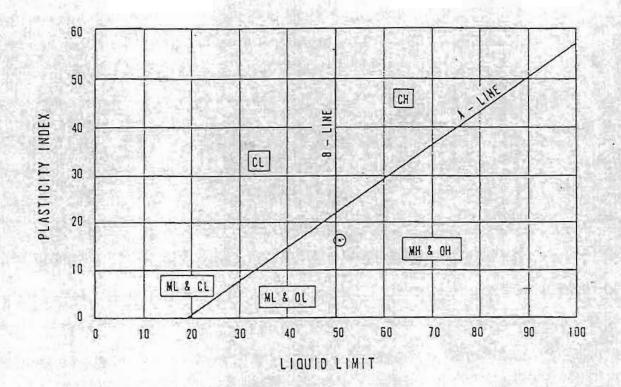




PROJECT ĎESCRIPTION:				1			The second	F15600, AS. 10
	*			SOILS (	CLASSIF	CLASSIFICATION	AND TEST	SUMMARY
· · ·	TRI	CITIES .		-	A STOCK		La sulta a	ASIM 02487
•	7	Hur INC.		1000	TYPE OF	SAMPLE:		A DESCRIPTION OF A DESC
	AS NI	NUTED			12-24-24		1. 1. V. W.	SAMPLE NO:
SAMPLE LOCATION NUMBER	DEPTH INTERVAL (FEET	DESCRIPTION OF MATERIAL	ASTM CLASSIFI- CATION	MOIS P.L. (%)	MOISTURE	GRADATION, % PASSING 3" 1%" #4 #200	, % PASSING # 4 #200	LA BORATORY TES
R-1-22 1-8	7.0-8.5	HED ROWN MED-F SAND	SP				100 <5	
B-6 ST-1 8	8.0-10.0	MER. BORNN SUT W/FSAND	TW				× × 40	
B-6 55-3 1	15.0-16.5	MEDBROWN SILTY F SAND	SM				100 43	Hydrometer
-7 37-1	8.0-10.0	MED. REDWY SILT	ML				100 100	Direct Shear
-7 55-3 1	5.0-16.5	MED BROWN SILTY FSAND	SM				k * 100 35	
B-14 SS- 6 1	15.0-16.5	MED. BROWN F SANDY SILT	ML	1.10			K X 100 80	
B-15 SS-2	5.9-0.5	MED. BROWN F SANDY SILT	TW	01			* * 100 85	
B-15 25-51	15.0-16.5	MED. BROWN SILT	W	NP 41	I NP		× 45	Limits
B-15 S2-4	10-0-11.5	MED BROWN FSANDY SILT	ML	2			× × 100	
B-16 SS-3	0.5-5.2	MED BOWN SILT W/ FRAND	ML				06 001 X X	
B-16 ST-4	100-12.0	MED. BROWN F SANDY SILT	ML	NP 5	SO NP	1	100 82	Hydromiter, Limits
8-16 SS-6 1	5.0-16.5 Value	MED. BROWN SILT	ML				100 47	177 Surg light

1		の思い				- Color			2	PISGOD	N. A.S. 10	
				so	SOILS CI	ASSIF	CLASSIFICATION	UN AND	TES	T SUMMARY	<b>NRY</b>	
PROJECT DESCRIPTION.		721 0	CITIES								ASTM D2487	482
MATERIALS LABORATORY:		1	HILL INC.	1000		TYPE OF	SAMPLE:					
SAMPLE LOCATION:		AS A	NoTED		al have					SAMPLE 1	NO:	
SAMPLE LOCATION	SAMPLE NUMBER	DEPTH INTERVAL (FCaT)	DESCRIPTION OF MATERIAL	CLASSIFI- P. CATION (%	MOISTURE P.L. (%) (%)	JRE L.L. (%)	GRADAT 3" 1	GRADATION, % PASSING 3" 1%" #4 #200	ASSING #200	YAGTA AUGAL		B15
E-17 S	1-55	5.0-6.5	MED. BROWN SILT	MH 3	5 <i>B</i> I	SI		201 *	2 100		r	
B-17 S	ST- 3	13.0-15.0	MED. BROWN SILT	ML				100	46 0	Hydrometer	ncten	
B-18 S	57-4	10.21-0.01	MED. BROWN SUTY FSAND S	SM M	030	NP		100	<i>Lħ</i> 0		Direct Shear	X
B-18 S	25-6	15.0-16.5	MED BROWN SILT	ML				201	001 0 *			
S 81-518	55-7	5-12-0-02	MED. BROWIN SILT	ML				4001 *	25			1.30
8-2.0 5	5 - 55	15.0-16.5	MED BROWN SILT .	74				201	2 200			
B-20 S	ss-6	20.0-21.5	MED. BROWN F SANDY SILT	ML				100	282			
BAG SAMPLE A	CWH B2-1		NEAR B-1 NED BROWN F 11 SAUDY SUT.	760	29			*	SZ 0	lomple	tion D	1557
B-17 5	57-3	13.0-15.0	MED BROWAL SILT	ML	54			001	98	Hydrometer		
8-17	1-16	23.0 - 25.0	MED, BROWN SANDY SILT	ML	52			100	89 0	Hydro Conso	Hydrometer, Consolidation	
REMARKS: X = EST	ESTIMATED	D VALUE	ne									
		DATE.		nare.			U ALCKEU	.>			DATE	

PLASTICITY CHART



SYMBOL	SAMPLE	LIQUID	PLASTICITY INDEX	NATURAL MOISTURE
$\odot$	6-17,55-1,50-6.5	51	16	81
	B-15, 55-5, 15.0-16-5'	NP*		4-1
	B-14, 5T-4, 10.0-12.0'	NP*		50
	8-18, ST-4, 10.0-12.0	NP*		30

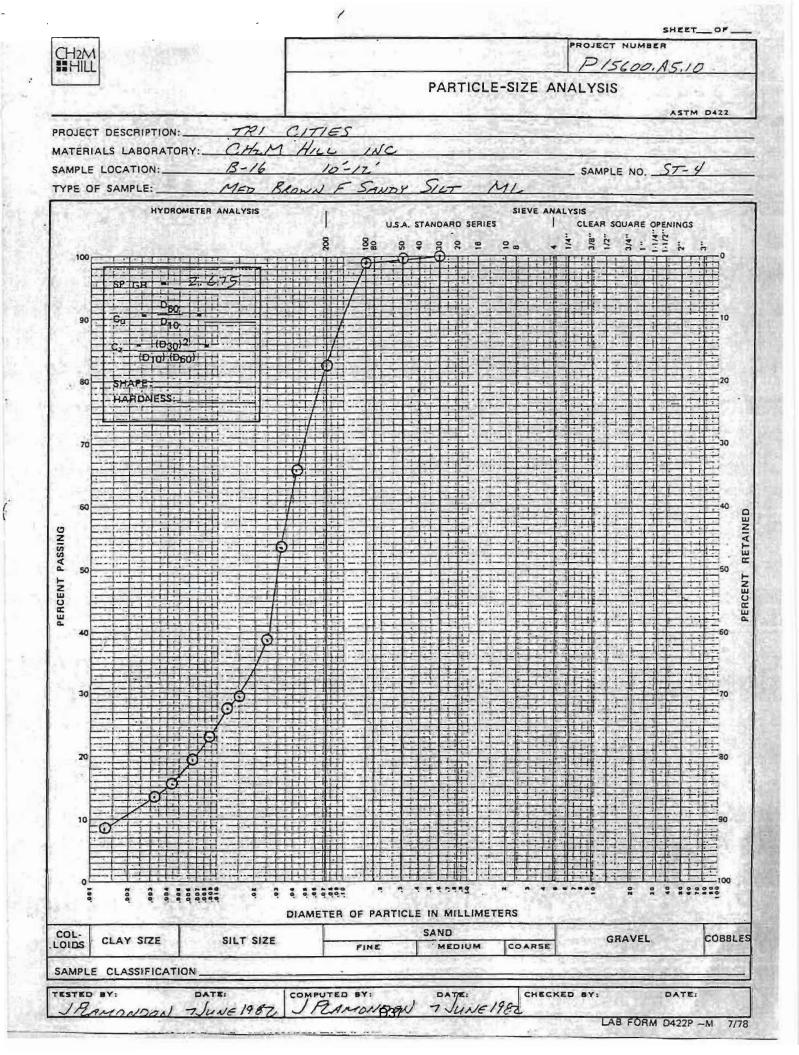
NOTE: \* NONPLASTIC

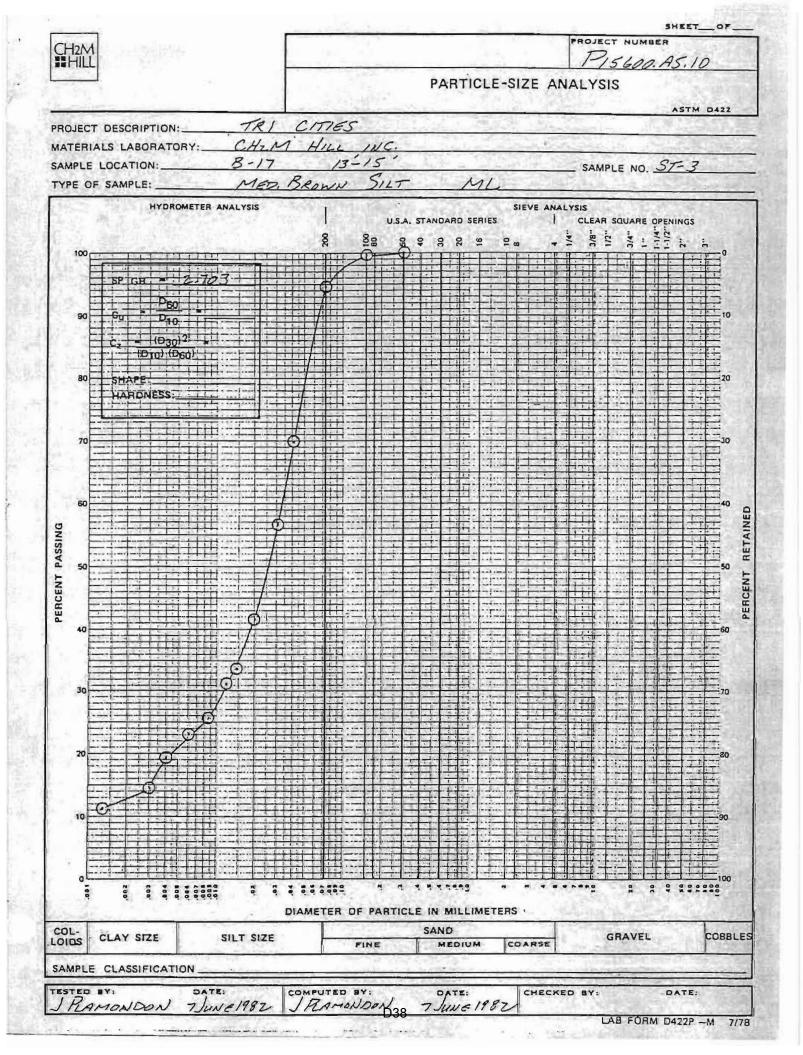
P15600 AS.10

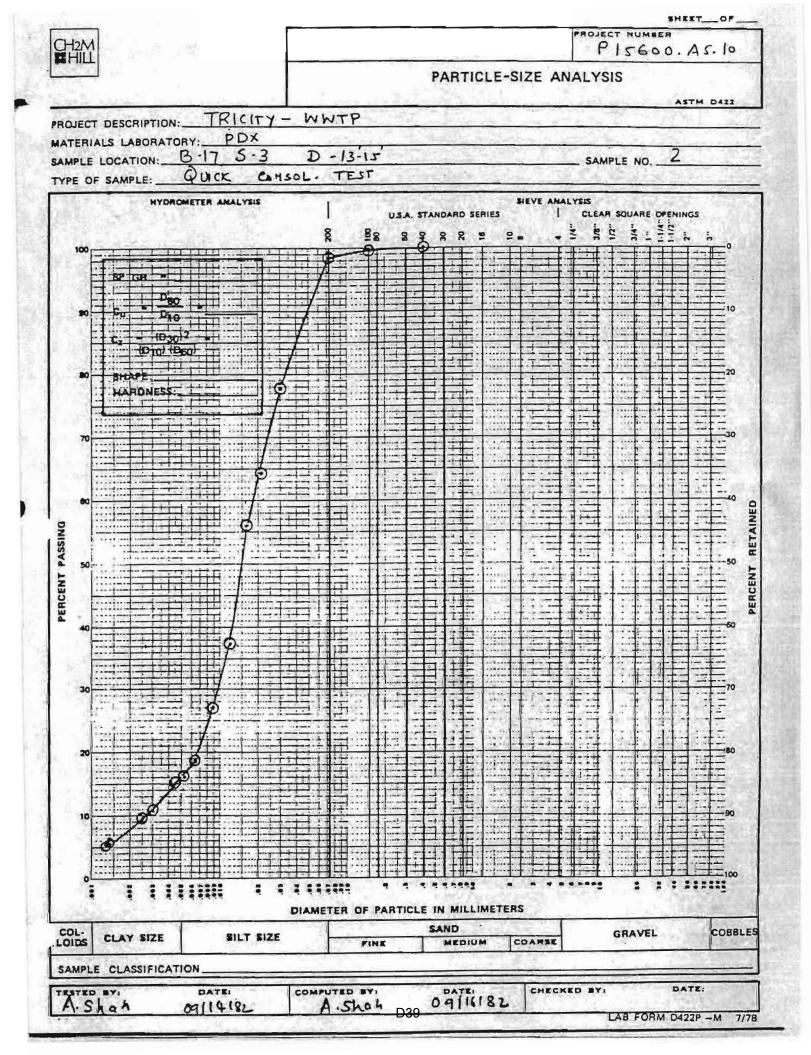
PLASTICITY CHART TRI-CITY SEWAGE TREATMENT PLANT

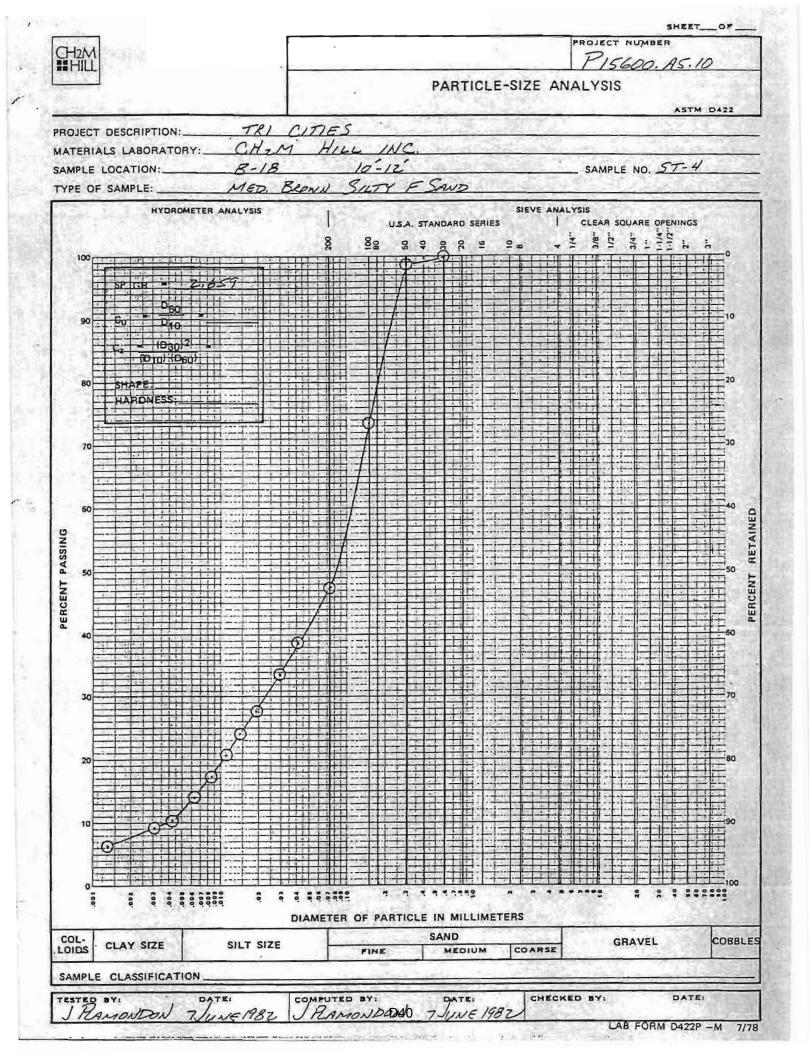
CH2M HILL

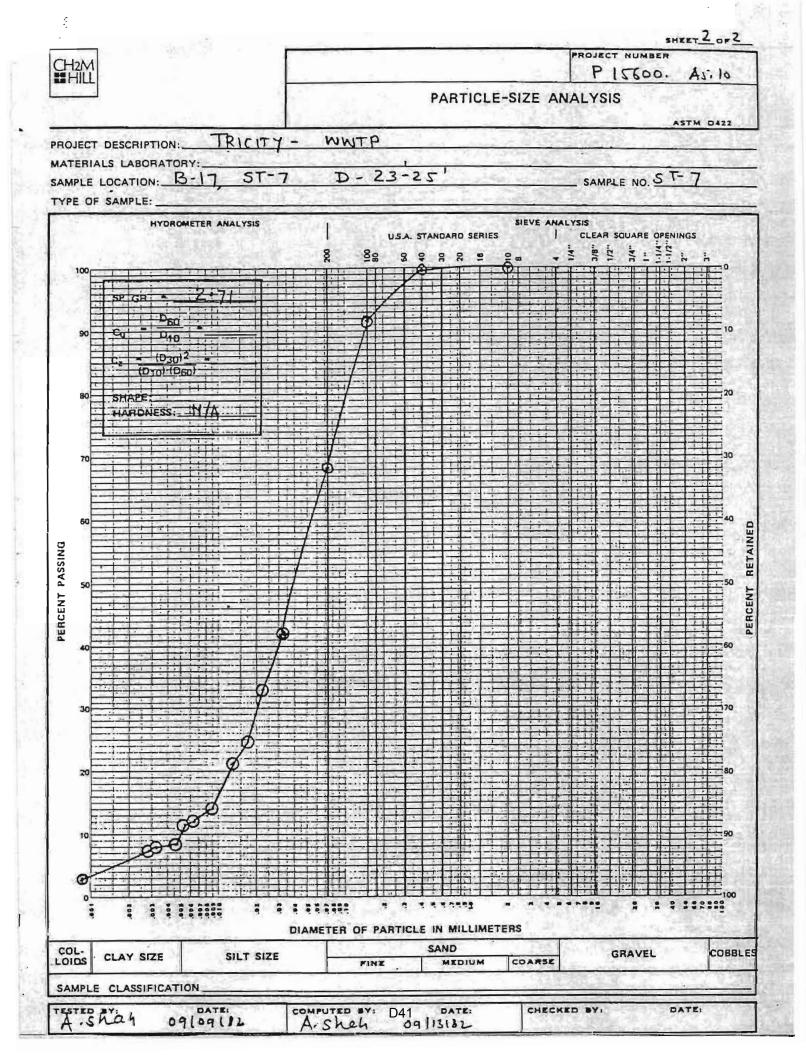
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	TOESCRIPTION	TRI C	ITIES	1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-	-	308				^	STM DA
MATER	ALS LABORATOR	Y: CHIM	HILL 1	NC.		1.40	a strategies		in a second		
SAMPLE	LOCATION:	B.G MED. REONA	1.511-1	5-16.	5	5	~	SAN	IPLE N	o. <u>55</u>	5-3
	ALC: NOT THE REAL PROPERTY OF	TETER ANALYSIS		1.2			SIEVE A	VALYSIS	11570		A COLOR
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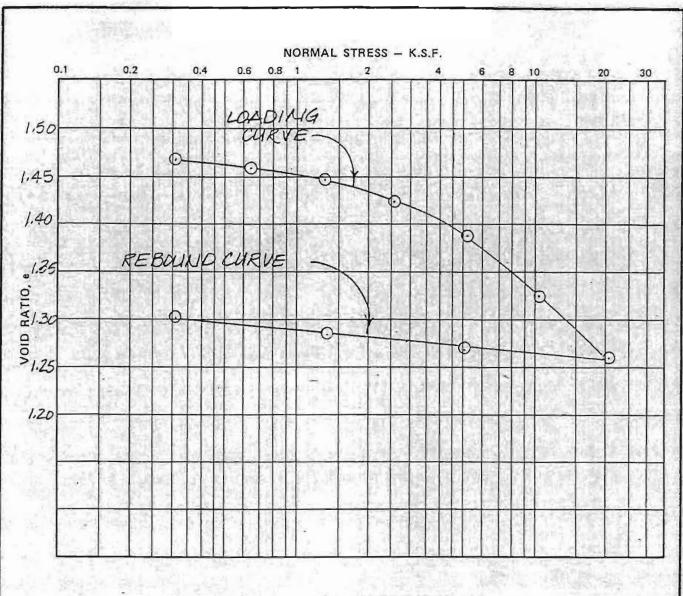












PLOT OF PRIMARY CONSOLIDATION

SAMPLE DATA:

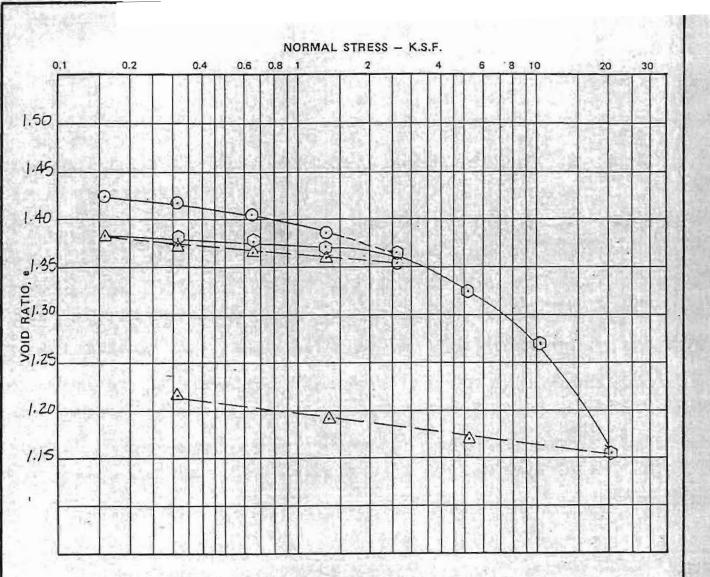
P15600.A5

BROWN SANDY SILT (ML) DEPTH 10,0-12.0 FT. INITIAL DIAMETER = 2.50 INI. INITIAL HEIGHT = 1.00 INI. INITIAL VOID RATIO = 1.47 NATURAL MOISTURE CONTENT = 52 % DRY DENSITY = GIPCF

> 8-16 ST-4 CONSOLIDATIONS TEST TRJ-CITY SEWAGE TREATMENT PLANT



FORM 70



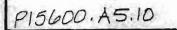
PLOT OF PRIMARY CONSOLIDATION

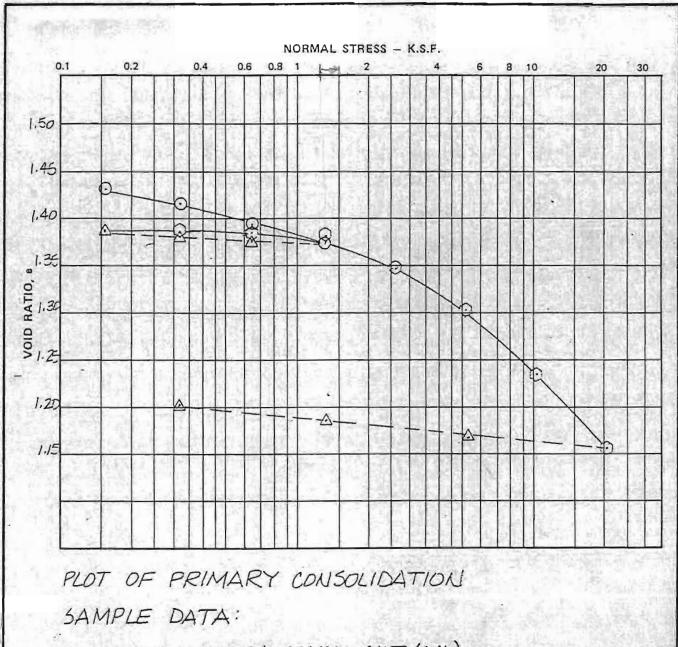
SAMPLE DATA :

MEDIUM BROWN SILT (ML) DEPTH 13-15 FT. INITIAL DIAMETER = 2.50 IN. INITIAL HEIGHT = 1.00 IN. INITIAL VOID RATIO = 1.426 INITIAL MOISTURE CONTENT = 54% DRY DENSITY = 69.4 PCF

D43

B-17 ST-3 CONSOLIDATION TEST TRI-CITY SEWAGE TREATMENT PLANT



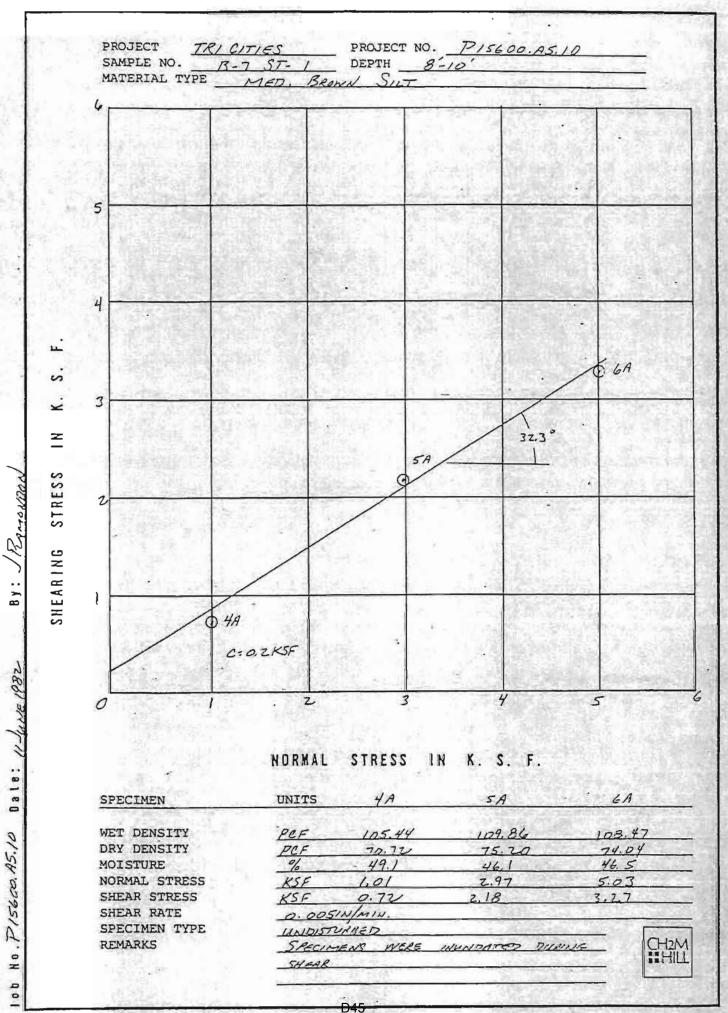


MEDIUM BROWN SANDY SILT (ML) DEPTH 23-25 FT, INITIAL DIAMETER = 2.50IN. INITIAL HEIGHT = 1.00 IN. INITIAL VOID RATID = 1.44 NATURAL MOISTURE CONTENT = 52 % DRY DENSITY = 69 PCF

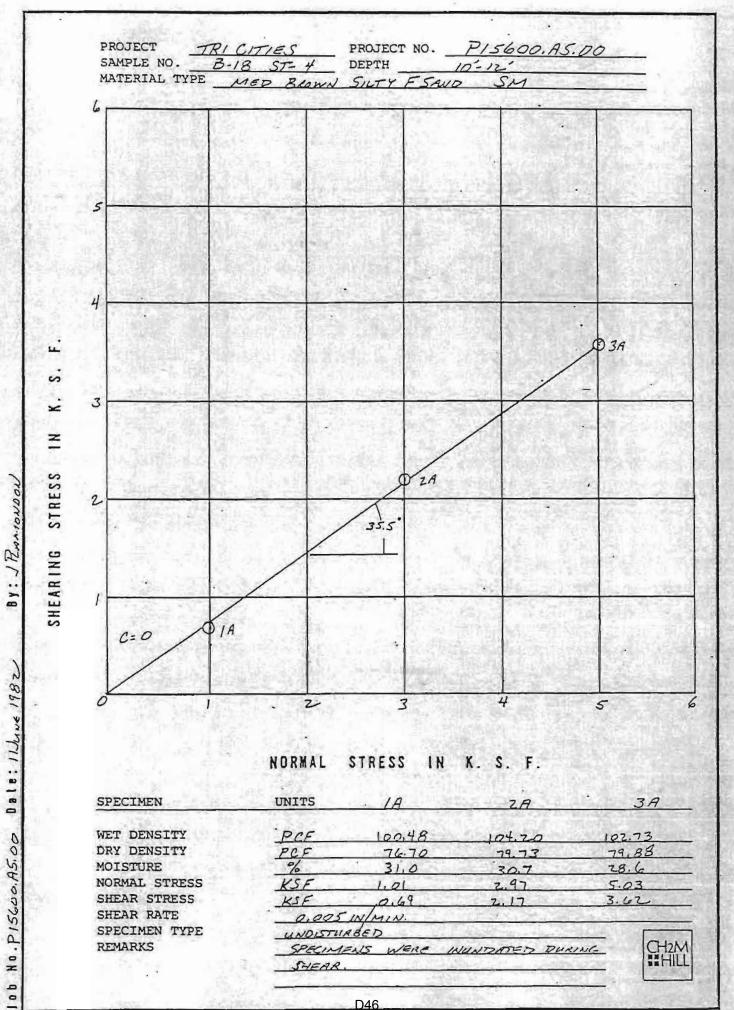
> B-17 ST-7 CONSOLIDATION TEST TRI-CITY SEWAGE TREATMENT PLANT

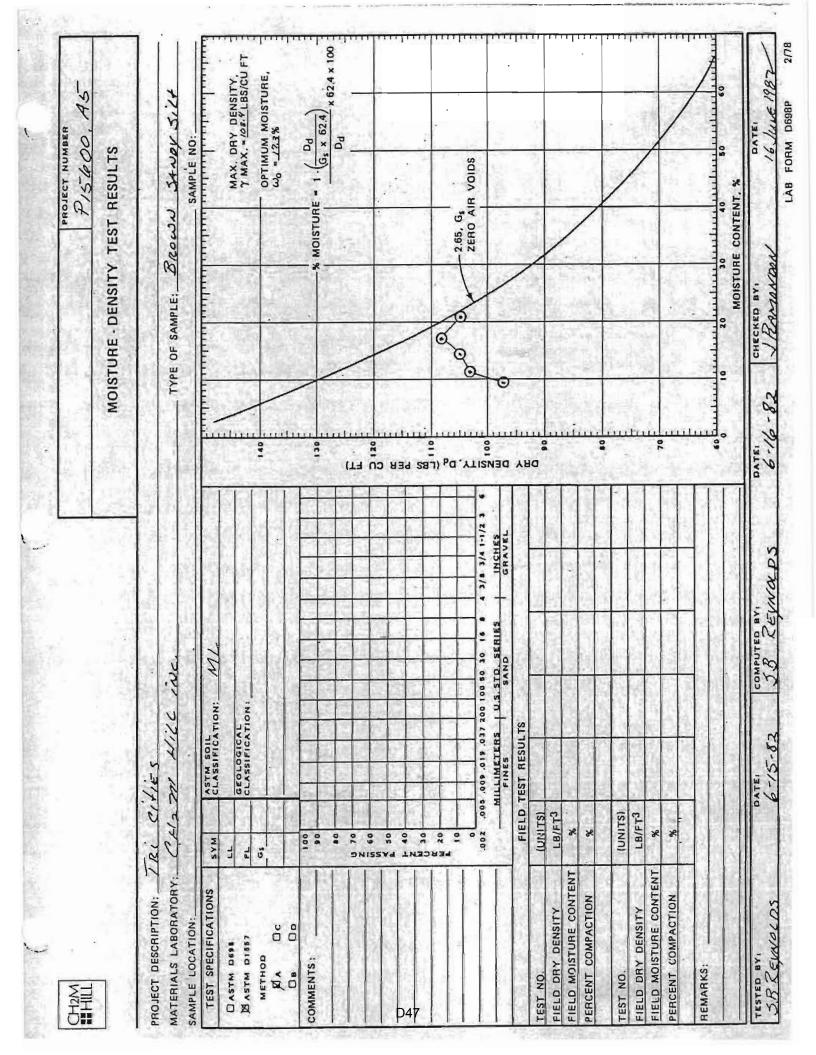
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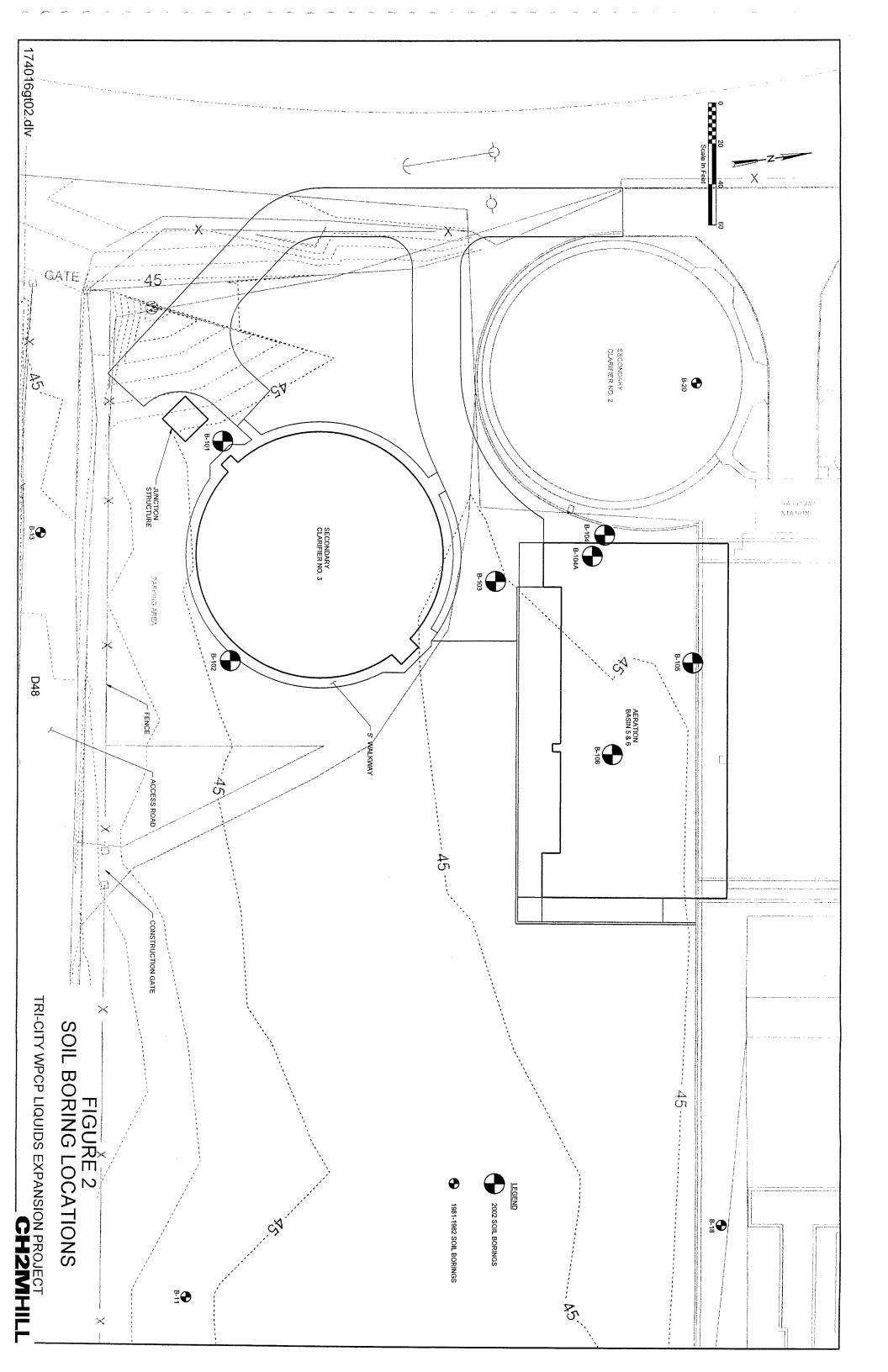
CH2M HILL



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**ELEVATION: 45'** 

BORING NUMBER: B-101

Sheet: 1 of 2

# SOIL BORING LOG

PROJECT: Tri-City WPCP Liquids Expansion

**LOCATION:** SW of clarifier no. 3

DRILLING CONTRACTOR: Geo-Tech Explorations, Tualatin, Oregon

DRILLING METHOD AND EQUIPMENT: Mobile B-59 rubber-tire drill rig, mud rotary, 4-7/8" tri-cone bitWATER LEVELS: N/ASTART: 8/5/02FINISH: 8/5/02LOGGER: R. Wilcock

ACE		SAMPL	E	STANDARD	SOIL DESCRIPTION	COMMENTS
DEPTH BELOW GROUND SURFACE	INTERVAL	TYPE AND NUMBER	RECOVERY (IN)	PENETRATION TEST RESULTS 6"-6"-6"	SOIL NAME, USCS GROUP SYMBOL, COLOR, MOISTURE CONTENT, RELATIVE DENSITY OR CONSISTENCY, SOIL STRUCTURE, MINERALOGY	DEPTH OF CASING, DRILLING RATE, DRILLING FLUID LOSS, TESTS AND INSTRUMENTATION
0	-				Ground Surface	<ul> <li>140-pound safety hammer, rope and cathead with 1½ wraps around cathead</li> </ul>
-	2.5 4.0	SS-1	9	6-11-12 (23)	SILT (ML) dark brown and gray-brown, moist, very stiff, medium plasticity, one piece of 1" subangular	w = 30%
5- - -	5.0 6.5	SS-2	2	17-18-32 (50)	gravel in shoe (FILL) Poor Recovery <u>POORLY GRADED GRAVEL (GP)</u> black, wet, very dense, fine to coarse angular and subangular gravel up to 1½" (FILL)	Native material at 8 ft
-   	10.0	SS-3	3	6-5-6 (11)	SILT (ML) gray, wet, stiff, low to medium plasticity,one piece of 1" black gravel in shoe	Stiffer silt at 12 ft
- 15 - -	15.0 16.5	SS-4	12	6-7-10 (17)	<b>SANDY SILT (ML)</b> mottled gray and red, moist, very stiff, low to medium plasticity, 15% very fine sand at top of sample grading to 40% at bottom of sample	Scattered gravel from 16.5-17.5 ft, then back into silt
- 20 -	20.0 21.5	SS-5	15	5-5-6 (11)	<u>SILT (ML)</u> reddish brown, moist, stiff, nonplastic to low plasticity, trace of very fine sand	
	23.0 25.0	SH-6	NR	PUSH	No Recovery	
25	25.0 26.5	SS-7	15	2-2-4 (6)	<u>SILT (ML)</u> reddish brown, moist, firm, nonplastic to low plasticity, 5-10% very fine sand	PP = 1.5, 2.0, 2.5 tsf
	27.5 29.0	SS-8	18	3-3-4 (7)	Same as SS-7	LL, PL, PI = 42, 31, 11; w = 45%
30-					D49	



BORING NUMBER: B-101 Sheet: 2 of 2

# SOIL BORING LOG

LOCATION: SW of clarifier no. 3

PROJECT: Tri-City WPCP Liquids Expansion DRILLING CONTRACTOR: Geo-Tech Explorations, Tualatin, Oregon **ELEVATION: 45'** 

DRILLING METHOD AND EQUIPMENT: Mobile B-59 rubber-tire drill rig, mud rotary, 4-7/8" tri-cone bit LOGGER: R. Wilcock **FINISH:** 8/5/02 **START:** 8/5/02 WATER LEVELS: N/A

ACE	5	SAMPLE		STANDARD PENETRATION	SOIL DESCRIPTION	COMMENTS
DEPTH BELOW GROUND SURFACE	INTERVAL	TYPE AND NUMBER	RECOVERY (IN)	TEST RESULTS 6"-6"-6"	SOIL NAME, USCS GROUP SYMBOL, COLOR, MOISTURE CONTENT, RELATIVE DENSITY OR CONSISTENCY, SOIL STRUCTURE, MINERALOGY	DEPTH OF CASING, DRILLING RATE, DRILLING FLUID LOSS, TESTS AND INSTRUMENTATION
	30.0 31.5	SS-9	6	2-4-14 (18)	SILT (ML) reddish brown, wet, very stiff, 1 piece of black 1½" gravel in shoe	
-						Dense gravel at 32.8 ft
-						Driller indicates cemented gravel (Troutdale formation?)
35-	35.0 35.5	SS-10	3	100/6"	POORLY GRADED GRAVEL WITH SAND (GP) black and red gravel, red sand, wet, very	
-					dense, fine gravel with one piece 1½" gravel, subangular and fractured, one piece of fine	
-	38.0 38.3	SS-11	NR	50/3"	angular quartzite gravel	End Boring at 38.3 ft Boring backfilled in accordance with OAR 690-240
40-					BOTTOM OF BORING	
-						
-						
45-						
	4					
50-						
	-					
	4					
55-						
	-	-				
60-	_				D50	



**ELEVATION: 45'** 

BORING NUMBER: B-102

Sheet: 1 of 3

# SOIL BORING LOG

**PROJECT:** Tri-City WPCP Liquids Expansion

LOCATION: SE of clarifier no. 3

DRILLING CONTRACTOR: Geo-Tech Explorations, Tualatin, Oregon

DRILLING METHOD AND EQUIPMENT: Mobile B-59 rubber-tire drill rig, mud rotary, 4-7/8" tri-cone bitWATER LEVELS: 22.95'START: 8/6/02FINISH: 8/7/02LOGGER: R. Wilcock

ACE	S	SAMPLE		STANDARD PENETRATION	SOIL DESCRIPTION	COMMENTS
DEPTH BELOW GROUND SURFACE	NTERVAL	TYPE AND NUMBER	RECOVERY (IN)	TEST RESULTS 6"-6"-6"	SOIL NAME, USCS GROUP SYMBOL, COLOR, MOISTURE CONTENT, RELATIVE DENSITY OR CONSISTENCY, SOIL STRUCTURE, MINERALOGY	DEPTH OF CASING, DRILLING RATE, DRILLING FLUID LOSS, TESTS AND INSTRUMENTATION
0-		<u> </u>	<b>L</b>		Ground Surface	140-pound safety hammer, rope and cathead with 1½ wraps around cathead
-	2.5 4.0	SS-1	11	15-15-15 (30)	SILTY GRAVEL (GM) black gravel, brown silt, moist, medium dense, gravel up to 1", low to medium plasticity silt (FILL)	
5	5.0 6.5	SS-2	14	18-15-23 (38)	GRAVELLY SILT (ML) brown with black gravel, moist, hard, low plasticity silt, angular gravel up to 1", trace organics (FILL)	
						Native material at 8.5 ft
10	10.0 11.5	SS-3	12	7-5-6 (11)	SILT (ML) brown with gray and rust mottling, moist, stiff, low plasticity, trace very fine sand	PP = 2.0 tsf w = 42%
- 15 -	15.0 16.5	SS-4	15	3-7-5 (12)	<u>SANDY SILT (ML)</u> brown with gray mottling, moist, stiff, nonplastic, 15% very fine sand	
20	20.0 21.5	SS-5	18	2-3-6 (9)	<u>SILT (ML)</u> mottled brown and gray, moist, stiff, low plasticity, 5% very fine sand at top of sample grading to 10% at bottom of sample	
	22.5 24.5	SO-6	24	PUSH	<u>SILT (ML)</u> D51	Osterberg piston sampler TV = $0.35$ tsf; PP = $2.0, 2.0, 1.5$ tsf LL, PL, PI = $48, 32, 16$ ; w = $43\%$ Consolidation test



BORING NUMBER: B-102 Sheet: 2 of 3

# SOIL BORING LOG

PROJECT: Tri-City WPCP Liquids Expansion LOCATION: SE of clarifier no. 3

DRILLING CONTRACTOR: Geo-Tech Explorations, Tualatin, Oregon

**ELEVATION: 45'** DRILLING METHOD AND EQUIPMENT: Mobile B-59 rubber-tire drill rig, mud rotary, 4-7/8" tri-cone bit **FINISH:** 8/7/02 **START:** 8/6/02

WATER LEVELS: 22.95

LOGGER: R. Wilcock

ACE	S	SAMPLE		STANDARD PENETRATION	SOIL DESCRIPTION	COMMENTS
DEPTH BELOW GROUND SURFACE	INTERVAL	TYPE AND NUMBER	RECOVERY (IN)	TEST RESULTS 6"-6"-6"	SOIL NAME, USCS GROUP SYMBOL, COLOR, MOISTURE CONTENT, RELATIVE DENSITY OR CONSISTENCY, SOIL STRUCTURE, MINERALOGY	DEPTH OF CASING, DRILLING RATE, DRILLING FLUID LOSS, TESTS AND INSTRUMENTATION
	<b>≅</b> 24.5 26.0	F 2 SS-7	18	4-4-5 (9)	SILT (ML) brown, moist, stiff, low plasticity	PP = 1.25, 1.25, tsf (SS-7) w = 45%
-	27.5 29.0	SS-8	18	3-4-7 (11)	SILT TO SANDY SILT (ML) Upper 12": same as above; Lower 6": brown, wet, stiff, nonplastic to low plasticity, 15% very fine sand	Bagged upper 12" as sample SS-8A, lower as SS-8B Push bottomed out at 30.4 ft
30-	29.5 30.4 30.5	SO-9	12	PUSH	<u>SILTY SAND (SM)</u> SILTY SAND (SM)	Hit dense gravel at 30.4 ft; silty sand at bottom of SO-9
	30.5	SS-10	16	22-16-11 (27)	black with some white and red grains, moist, medium dense, fine grained sand, 1" zone of cemented sand at top of sample, 15% silt, 2" sandy silt layer near bottom of sample	P200 = 19% Driller indicates silt and sand seams to 34 ft
35-	35.0 35.8	SS-11	NR	42-50/4*	POOR RECOVERY one piece of 1½* black gravel wedged in shoe	
- 40	40.0 41.5	SS-12	5	23-20-20 (40)	POORLY GRADED GRAVEL WITH SILT AND SAND (GP-GM) black gravel and sand, brown silt, wet, dense, fractured and angular gravel ¾" up to 1½",	Drilling rate increased from 39-40 ft; lost 10-15 gallons of mud
-					10% sand, 10% silt	Reamed out hole and continued with 6" tri-cone bit
45-	45.0 45.2	SS-13	NR	50/2"	POOR RECOVERY one piece of black 1½" angular gravel in shoe, black, wet, very dense	Slow drilling, approx. 20 min/ft
- 50-					D52	



**ELEVATION: 45'** 

BORING NUMBER: B-102 Sheet: 3 of 3

# SOIL BORING LOG

PROJECT: Tri-City WPCP Liquids Expansion

**LOCATION:** SE of clarifier no. 3

DRILLING CONTRACTOR: Geo-Tech Explorations, Tualatin, Oregon

DRILLING METHOD AND EQUIPMENT: Mobile B-59 rubber-tire drill rig, mud rotary, 4-7/8" tri-cone bitWATER LEVELS: 22.95'START: 8/6/02FINISH: 8/7/02LOGGER: R. Wilcock

ACE		SAMPL		STANDARD PENETRATION	SOIL DESCRIPTION	COMMENTS
DEPTH BELOW GROUND SURFACE	INTERVAL	TYPE AND NUMBER	RECOVERY (IN)	TEST RESULTS 6"-6"-6"	SOIL NAME, USCS GROUP SYMBOL, COLOR, MOISTURE CONTENT, RELATIVE DENSITY OR CONSISTENCY, SOIL STRUCTURE, MINERALOGY	DEPTH OF CASING, DRILLING RATE, DRILLING FLUID LOSS, TESTS AND INSTRUMENTATION
-	50.0 50.3	SS-14	NR	50/3 <b>*</b>	POOR RECOVERY 1" slough in sampler	Bagged up slough to show gravel type; mostly black with 2-3 pieces of quartzite
	54.5 55.9	SS-15	17	28-32-50/5"	SILTSTONE brown with 1" blue-green seam and blue and rust mottling, moist, hard	Hit siltstone at 53.5 ft Shut down at 4:30, start drilling on 8/7/02 at 6:00 PP = no penetration at 4.5 tsf End Boring at 55.9 ft
-					BOTTOM OF BORING	Installed Piezometer in accordance with OAR 690-240
-						Finished piezo install at 7:00 moved to B-103
60-						Took reading in piezo on 8/9/02 groundwater at 22.95 ft
					Piezometer Materials: 2" OD schedule 40 PVC pipe 5' 20-slot machine-slotted screen with end cap 3/4 bentonite chips 8/12 Colorado silica sand Grout mix: 30 gal. water 70 lbs. portland cement 20 lbs. bentonite powder	
- - - 70- -					Piezometer Configuration: 54.5-53.5 bentonite chips 53.5-45.2 sand 52.5-47.5 screen 45.2-42.2 chips 42.2-1.5 grout (50-55 gallons used) 1.5-0 flush-mount monument set in concrete	
					D53	



**ELEVATION: 45'** 

BORING NUMBER: B-103 Sheet: 1 of 2

# SOIL BORING LOG

**PROJECT:** Tri-City WPCP Liquids Expansion

LOCATION: N of clarifier no. 3

DRILLING CONTRACTOR: Geo-Tech Explorations, Tualatin, Oregon

DRILLING METHOD AND EQUIPMENT: Mobile B-59 rubber-tire drill rig, mud rotary, 4-7/8" tri-cone bitWATER LEVELS: N/ASTART: 8/7/02FINISH: 8/7/02LOGGER: R. Wilcock

ACE	SAMPLE			STANDARD PENETRATION	SOIL DESCRIPTION	COMMENTS
DEPTH BELOW GROUND SURFACE	INTERVAL	TYPE AND NUMBER	RECOVERY (IN)	TEST RESULTS 6"-6"-6"	SOIL NAME, USCS GROUP SYMBOL, COLOR, MOISTURE CONTENT, RELATIVE DENSITY OR CONSISTENCY, SOIL STRUCTURE, MINERALOGY	DEPTH OF CASING, DRILLING RATE, DRILLING FLUID LOSS, TESTS AND INSTRUMENTATION
0-					Ground Surface	140-pound safety hammer, rope
						and cathead with 1½ wraps around cathead
-	2.5 3.1	SS-1	4	29-12/1"	SILTY GRAVEL (GM) black gravel, brown silt, moist, very dense, fine angular gravel, 25-35% silt, 5-10% sand (FILL)	Big cobble pushing sampler to side, stopped SPT after 7"
5-	5.0 6.5	SS-2	NR	17-18-19 (37)	<u>No Recovery</u>	Gravel fill
-						Into native material at 7 ft
- 10-	10.0					
-	10.0 11.5	SS-3	13	2-2-1 (3)	SILT (ML) brown, moist, very soft, low plasticity	
- - 15 -	15.0 16.5	SS-4	15	1-1-1 (2)	<u>SILT (ML)</u> Same as SS-3	LL, PL, PI = 44, 31, 14; w = 50%
- - 20 -	20.0 21.5	SS-5	14	2-1-3 (4)	<u>SILT (ML)</u> same as SS-3	PP = 1.5, 1.25, 1.25 tsf
-	22.5 24.0	SS-6	17	3-2-2 (4)	<u>SILT (ML)</u> same as SS-3	PP = 1.0, 1.75, 1.75 tsf w = 46%
25—	25.0 27.0	SO-7	24	PUSH	<u>SILT (ML)</u> (top) <u>SILTY SAND (SM)</u> (bottom)	
	27.0 28.5	SS-8	14	3-5-10 (15)	<u>SILTY SAND (SM)</u> brown, moist, medium dense, fine sand, 45% silt at top of sample grading to 25% in shoe	P200 = 29%
30-					D54	Hit gravel at 30 ft



BORING NUMBER: B-103 Sheet: 2 of 2

# SOIL BORING LOG

LOCATION: N of clarifier no. 3

**PROJECT:** Tri-City WPCP Liquids Expansion DRILLING CONTRACTOR: Geo-Tech Explorations, Tualatin, Oregon **ELEVATION: 45'** DRILLING METHOD AND EQUIPMENT: Mobile B-59 rubber-tire drill rig, mud rotary, 4-7/8" tri-cone bit

WATER LEVELS: N/A **START:** 8/7/02

**FINISH:** 8/7/02

LOGGER: R. Wilcock

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ACE	5	SAMPLE		STANDARD PENETRATION	SOIL DESCRIPTION	COMMENTS
DEPTH BELOW GROUND SURFACE	INTERVAL	TYPE AND NUMBER	RECOVERY (IN)	TEST RESULTS 6"-6"-6"	SOIL NAME, USCS GROUP SYMBOL, COLOR, MOISTURE CONTENT, RELATIVE DENSITY OR CONSISTENCY, SOIL STRUCTURE, MINERALOGY	DEPTH OF CASING, DRILLING RATE, DRILLING FLUID LOSS, TESTS AND INSTRUMENTATION
-	30.0 31.0	SS-9	3	34-50/6"	POORLY GRADED GRAVEL WITH SILT (GP- GM)	
					black and red, wet, very dense, subrounded to subangular gravel, 10% silt, 5-10% sand	Smoother, faster drilling (5 ft/20 min) in gravel than in B-101 and 102; driller indicates smaller gravel size (<2")
35-	35.0 35.4 36.0	SS-10	2	100/5"	POORLY GRADED GRAVEL (GP) black and red, wet, very dense, rounded to angular gravel up to 2"	Poor recovery in SS-10, so drilled out and went right back down with 3" splitspoon and 300-pound hammer to get SS-11
-	37.5	SS-11	6	16-16-19 (35)	SILTY GRAVEL WITH SAND (GM) black and red, wet, dense, gravel up to 2½",	P200 = 6% End Boring at 37.5 ft
- 40-					\15% sand, 15% silt BOTTOM OF BORING	Boring backfilled in accordance with OAR 690-240
-						
45-						
-						
- 55	     			s		
-						
. 60-					D55	



BORING NUMBER: B-104 Sheet: 1 of 1

# SOIL BORING LOG

PROJECT: Tri-City WPCP Liquids ExpansionLOCATION: SW corner of aeration basins 5 and 6ELEVATION: 45'DRILLING CONTRACTOR: Geo-Tech Explorations, Tualatin, OregonDRILLING METHOD AND EQUIPMENT: Mobile B-59 rubber-tire drill rig, mud rotary, 4-7/8" tri-cone bitWATER LEVELS:START: 8/7/02FINISH: 8/7/02LOGGER: R. Wilcock

111						
ACE	S	AMPLE		STANDARD PENETRATION	SOIL DESCRIPTION	COMMENTS
DEPTH BELOW GROUND SURFACE	INTERVAL	TYPE AND NUMBER	RECOVERY (IN)	TEST RESULTS 6"-6"-6"	SOIL NAME, USCS GROUP SYMBOL, COLOR, MOISTURE CONTENT, RELATIVE DENSITY OR CONSISTENCY, SOIL STRUCTURE, MINERALOGY	DEPTH OF CASING, DRILLING RATE, DRILLING FLUID LOSS, TESTS AND INSTRUMENTATION
0					Ground Surface	140-pound safety hammer, rope and cathead with 1½ wraps around cathead
5-	2.5 4.0 5.0 6.5	SS-1 SS-2	14	10-8-7 (15) 7-16-43 (59)	<u>SILT (ML)</u> gray with brown mottling, moist, stiff, low to medium plasticity (FILL) <u>SILT (ML)</u> brown with black mottling, low plasticity, black	Very slow drilling in fill; drilling through backfill material at existing clarifier
- - 10-	10.0 10.8	SS-3	4	20-50/3*	fractured gravel in shoe (FILL) GRAVELLY SILT (ML) brown with black gravel, moist, hard, gravel up to 1"	End Boring at 10.8 ft Boring backfilled in accordance
- - 15- -					BOTTOM OF BORING	with OAR 690-240 Moved 8' to the east and 6' to the south to get out of clarifier backfill zone (See boring 104A)
- 25- - - - -					D56	



15

20

25

30

26.0

27.5

SS-7

16

3-4-5 (9)

BORING NUMBER: B-104A Sheet: 1 of 2

COMMENTS

DEPTH OF CASING.

INSTRUMENTATION

P200 = 47%

Gravel at 29.9 ft

# SOIL BORING LOG

LOCATION: SW corner of aeration basins 5 and 6 **PROJECT:** Tri-City WPCP Liquids Expansion DRILLING CONTRACTOR: Geo-Tech Explorations, Tualatin, Oregon **ELEVATION: 45'** DRILLING METHOD AND EQUIPMENT: Mobile B-59 rubber-tire drill rig, mud rotary, 4-7/8" tri-cone bit LOGGER: R. Wilcock

FINISH: 8/7/02 WATER LEVELS: N/A **START:** 8/7/02 DEPTH BELOW GROUND SURFACE STANDARD SAMPLE SOIL DESCRIPTION PENETRATION (NE) TEST RESULTS RECOVERY SOIL NAME, USCS GROUP SYMBOL, TYPE AND NUMBER NTERVAL **DRILLING RATE, DRILLING** COLOR, MOISTURE CONTENT, RELATIVE **DENSITY OR CONSISTENCY, SOIL** FLUID LOSS, TESTS AND 6"-6"-6" STRUCTURE, MINERALOGY Ground Surface 0-140-pound safety hammer, rope and cathead with 2 wraps around cathead 5 SILT (ML) 5.0 w = 34%SS-1 5 4-50/5" brown, moist, hard, one piece 1" angular 5.9 gravel in shoe (FILL) 10 10.0 SILT (ML) **SS-2** 10 2-3-3 (6) brown with gray and red mottling, moist, firm, 11.5 low plasticity

Into native material at 9 ft Quick, easy drilling 15.0 SILT (ML) SS-3 15 2-2-2 (4) brown, moist, soft, low plasticity, 5% very fine 16.5 sand 20.0 SILT (ML) SS-4 13 2-3-4 (7) Same as SS-3 21.5 SILT (ML) 22.5 SS-5 14 3-3-3 (6) Same as SS-3 24.0 Osterberg sampler TV = 0.15 tsf SANDY SILT (ML) 24.0 SO-6 24 PUSH 26.0

> SANDY SILT (ML) at top of sample grading to SILTY SAND (SM) at bottom of sample brown, wet, firm/loose, fine sand, low plasticity silt, 30% sand at top, 30-40% silt at bottom



BORING NUMBER: B-104A Sheet: 2 of 2

# SOIL BORING LOG

PROJECT: Tri-City WPCP Liquids ExpansionLOCATION: SW corner of aeration basins 5 and 6ELEVATION: 45'DRILLING CONTRACTOR: Geo-Tech Explorations, Tualatin, OregonDRILLING METHOD AND EQUIPMENT: Mobile B-59 rubber-tire drill rig, mud rotary, 4-7/8" tri-cone bitWATER LEVELS: N/ASTART: 8/7/02FINISH: 8/7/02LOGGER: R. Wilcock

ACE	5	SAMPLI		STANDARD PENETRATION	SOIL DESCRIPTION	COMMENTS
DEPTH BELOW GROUND SURFACE	INTERVAL	TYPE AND NUMBER	RECOVERY (IN)	TEST RESULTS 6"-6"-6"	SOIL NAME, USCS GROUP SYMBOL, COLOR, MOISTURE CONTENT, RELATIVE DENSITY OR CONSISTENCY, SOIL STRUCTURE, MINERALOGY	DEPTH OF CASING, DRILLING RATE, DRILLING FLUID LOSS, TESTS AND INSTRUMENTATION
	30.0 31.0	SS-8	6	34-50/6"	SILTY GRAVEL (GM) black gravel, red silt, wet, very dense, angular gravel, 15% silt, 5-10% medium sand	
35	35.0 35.9	SS-9	8	46-50/5"	SILTY GRAVEL (GM) black and red gravel, reddish brown silt, wet, very dense, 15-20% silt, 10% sand BOTTOM OF BORING	End Boring at 35.9 ft Boring backfilled in accordance with OAR 690-240
 40 						
- 45 -						
50						
- 55						
60					D58	



## BORING NUMBER: B-105

Sheet: 1 of 2

# SOIL BORING LOG

 PROJECT: Tri-City WPCP Liquids Expansion
 LOCATION: N edge of aeration basins 5 and 6

 ELEVATION: 45'
 DRILLING CONTRACTOR: Geo-Tech Explorations, Tualatin, Oregon

 DRILLING METHOD AND EQUIPMENT: Mobile B-59 rubber-tire drill rig, mud rotary, 4-7/8" tri-cone bit

WATER LEVELS: N/A START: 8/8/02 FINISH: 8/8/02 LOGGER: R. Wilcock

ACE		SAMPL		STANDARD PENETRATION	SOIL DESCRIPTION	COMMENTS
DEPTH BELOW GROUND SURFACE	INTERVAL	TYPE AND NUMBER	RECOVERY (IN)	TEST RESULTS 6"-6"-6"	SOIL NAME, USCS GROUP SYMBOL, COLOR, MOISTURE CONTENT, RELATIVE DENSITY OR CONSISTENCY, SOIL STRUCTURE, MINERALOGY	DEPTH OF CASING, DRILLING RATE, DRILLING FLUID LOSS, TESTS AND INSTRUMENTATION
0-					Ground Surface	140-pound safety hammer, rope
						and cathead with 1½ wraps around cathead
5-	5.0					
	6.5	SS-1	15	10-9-10 (19)	SILT (ML) brown, moist, very stiff, medium plasticity, trace very fine sand, one piece of 1" gravel at top of sample (FILL)	w = 32%
	7.5	SS-2	15	9-14-15 (29)	GRAVELLY SILT (ML)	
10-	1				brown and black, moist, very stiff, medium plasticity, 30% black fractured gravel up to 1"	Large cobble at 9.5 ft
10-	10.0 11.5	SS-3	14	11-17-25 (42)	(FILL) GRAVELLY SILT (ML)	
- I					brown with black gravel, moist, hard, 30% rounded and angular gravel up to 1*, 10% fine	Hit rubble or boulder at 12.2 ft
	1				to coarse sand (FILL)	Into native material at 12.5 ft
- 1						
15-	15.0 16.5	SS-4	NR	3-3-3 (6)	NO RECOVERY went back down with 3" splitspoon sampler	Driller indicates no recovery because sampler was pushing a
-					and recovered gravelly silt (ML), brown, moist, firm, low plasticity 15% black angular gravel up to 2-1/2*	piece of coarse gravel; went right back down hole with 3" splitspoon sampler and recovered 8" on 1.5 ft push from 15-16.5 ft; w = 35%
20-	20.0 21.5	SS-5	8	4-4-5 (9)	<u>SILT (ML)</u> brown, moist, stiff, low plasticity, trace very fine sand	
-	23.0				SANDY SILT (ML)	TV = 0.15 tsf
25-	25.0	SO-6	22	PUSH		
- 20-	25.0 26.5	SS-7	18	2-3-3 (6)	<u>SILT (ML)</u> brown, moist, firm, low plasticity	LL, PL, PI = 42, 36, 6; w = 47%
	27.5 28.0	SS-8	18	21-11-9 (20)	<u>SILTY SAND (SM)</u> brown silt, black, red and white sand grains, moist, medium stiff, fine sand, 25-30% silt	4" gravel seam at 27.5 ft
30-					D59	



BORING NUMBER: B-105 Sheet: 2 of 2

## SOIL BORING LOG

PROJECT: Tri-City WPCP Liquids ExpansionLOCATION: N edge of aeration basins 5 and 6ELEVATION: 45'DRILLING CONTRACTOR: Geo-Tech Explorations, Tualatin, OregonDRILLING METHOD AND EQUIPMENT: Mobile B-59 rubber-tire drill rig, mud rotary, 4-7/8" tri-cone bitWATER LEVELS: N/ASTART: 8/8/02FINISH: 8/8/02LOGGER: R. Wilcock

DEPTH BELOW GROUND SURFACE STANDARD SAMPLE COMMENTS SOIL DESCRIPTION PENETRATION Ê TEST DEPTH OF CASING, RESULTS SOIL NAME, USCS GROUP SYMBOL, RECOVERY TYPE AND NUMBER INTERVAL COLOR, MOISTURE CONTENT, RELATIVE DRILLING RATE, DRILLING FLUID LOSS, TESTS AND DENSITY OR CONSISTENCY, SOIL 6"-6"-6" INSTRUMENTATION STRUCTURE, MINERALOGY Gravel at 30.5 ft SILTY SAND (SM) 30.0 SS-9 12 8-45-50/3" same as above except some rust staining and 31.3 3/4" rounded gravel in shoe Slow, difficult drilling Lost circulation, lost 30 gal. 35 POOR RECOVERY mud, faster drilling, driller 35.0 21-15-7 (22) SS-10 NR one piece of 11/2" black angular gravel in shoe indicates looser gravel from 36.5 35-38 ft Back into very dense gravel at 38 ft 40 POORLY GRADED GRAVEL (GP) End Boring at 40.5 ft 40.0 3 50/6" SS-11 black and red, wet, very dense, angular to 40.5 Boring backfilled in accordance rounded gravel up to 11/2" with OAR 690-240 BOTTOM OF BORING 45-50 55 60 D60



BORING NUMBER: B-106 Sheet: 1 of 2

### SOIL BORING LOG

PROJECT: Tri-City WPCP Liquids ExpansionLOCATION: near center of aeration basins 5 and 6ELEVATION: 45'DRILLING CONTRACTOR: Geo-Tech Explorations, Tualatin, OregonDRILLING METHOD AND EQUIPMENT: Mobile B-59 rubber-tire drill rig, mud rotary, 4-7/8" tri-cone bit

WATER LEVELS: N/A

**START:** 8/8/02 **FINISH:** 8/8/02

LOGGER: R. Wilcock

ACE		SAMPLE		STANDARD PENETRATION	SOIL DESCRIPTION	COMMENTS
DEPTH BELOW GROUND SURFACE	INTERVAL	TYPE AND NUMBER	RECOVERY (IN)	TEST RESULTS 6"-6"-6"	SOIL NAME, USCS GROUP SYMBOL, COLOR, MOISTURE CONTENT, RELATIVE DENSITY OR CONSISTENCY, SOIL STRUCTURE, MINERALOGY	DEPTH OF CASING, DRILLING RATE, DRILLING FLUID LOSS, TESTS AND INSTRUMENTATION
0					Ground Surface	140-pound safety hammer, rope and cathead with 1½ wraps around cathead
- 5 -	5.0 6.5	SS-1	10	9-7-6 (13)	<u>SILT (ML)</u> gray with red staining, moist, stiff, medium plasticity (FILL), material in tip is low plasticity, brown native silt	Last 2" of SS-1 is native silt
- - 10-	7.5 9.0	SS-2	10	2-4-6 (10)	SILT (ML) brown, moist, stiff, low plasticity, one piece of 1" black angular gravel	Scattered gravel at top of sample
- - - 15-	10.0 11.5	SS-3	NR	2-2-2 (4)	NO RECOVERY some silt stuck to sample catcher	Driller indicates samples lost at SS-3 and SS-4 probably due to scattered coarse gravel in silt; sampler is probably pushing a piece of gravel
	15.0 16.5	SS-4	NR	2-2-2 (4)	NO RECOVERY some silt stuck to sample catcher	
20 	20.0 21.5	SS-5	15	2-3-3 (6)	<u>SILT TO SANDY SILT (ML)</u> brown, moist, firm, nonplastic, 10-20% very fine sand	
- - 25	23.0 25.0	SO-6	24	PUSH	SILT (ML) at top and bottom of shelby tube	Osterberg sampler TV = 0.2 tsf LL, PL, PI = 47, 38, 9; w = 47% Consolidation test
	25.0 26.5	SS-7	18	1-2-2 (4)	SILT (ML) brown, moist, soft, low plasticity, trace very fine sand	
	27.5 29.0	SS-8	13	9-6-6 (12)	<u>SILTY SAND (SM)</u> red, black, brown, moist, medium dense, 25% nonplastic to low plasticity silt	Driller indicates sand at 27.5 ft P200 = 35%
30-					D61	



BORING NUMBER: B-106 Sheet: 2 of 2

# SOIL BORING LOG

PROJECT: Tri-City WPCP Liquids ExpansionLOCATION: near center of aeration basins 5 and 6ELEVATION: 45'DRILLING CONTRACTOR: Geo-Tech Explorations, Tualatin, OregonDRILLING METHOD AND EQUIPMENT: Mobile B-59 rubber-tire drill rig, mud rotary, 4-7/8" tri-cone bitWATER LEVELS: N/ASTART: 8/8/02FINISH: 8/8/02LOGGER: R. Wilcock

ACE	9	SAMPLE		STANDARD PENETRATION	SOIL DESCRIPTION	COMMENTS
DEPTH BELOW GROUND SURFACE	INTERVAL	TYPE AND NUMBER	RECOVERY (IN)	TEST RESULTS 6"-6"-6"	SOIL NAME, USCS GROUP SYMBOL, COLOR, MOISTURE CONTENT, RELATIVE DENSITY OR CONSISTENCY, SOIL STRUCTURE, MINERALOGY	DEPTH OF CASING, DRILLING RATE, DRILLING FLUID LOSS, TESTS AND INSTRUMENTATION
	30.0 31.5	SS-9	9	20-20-41 (61)	SILTY SAND (SM) black and red sand, brown silt, wet, very dense, 15% silt, 2" silt lens near top of sample, bottom 2" of sample is gravel	Gravel at 31.4 ft 30 gal. mud loss at 32 ft; lost circulation at 32.5 ft; added bentonite to thicken mud Slow, difficult drilling from 30-35 ft
35	35.0 35.3	SS-10	NR	50/4"	POOR RECOVERY fractured black gravel in shoe BOTTOM OF BORING	End Boring at 35.3 ft Boring backfilled in accordance with OAR 690-240
40						
45						
- 55 -						
60					D62	

### CH2M Hill Tri-City WPCP Liquids Expansion Project Number 174016

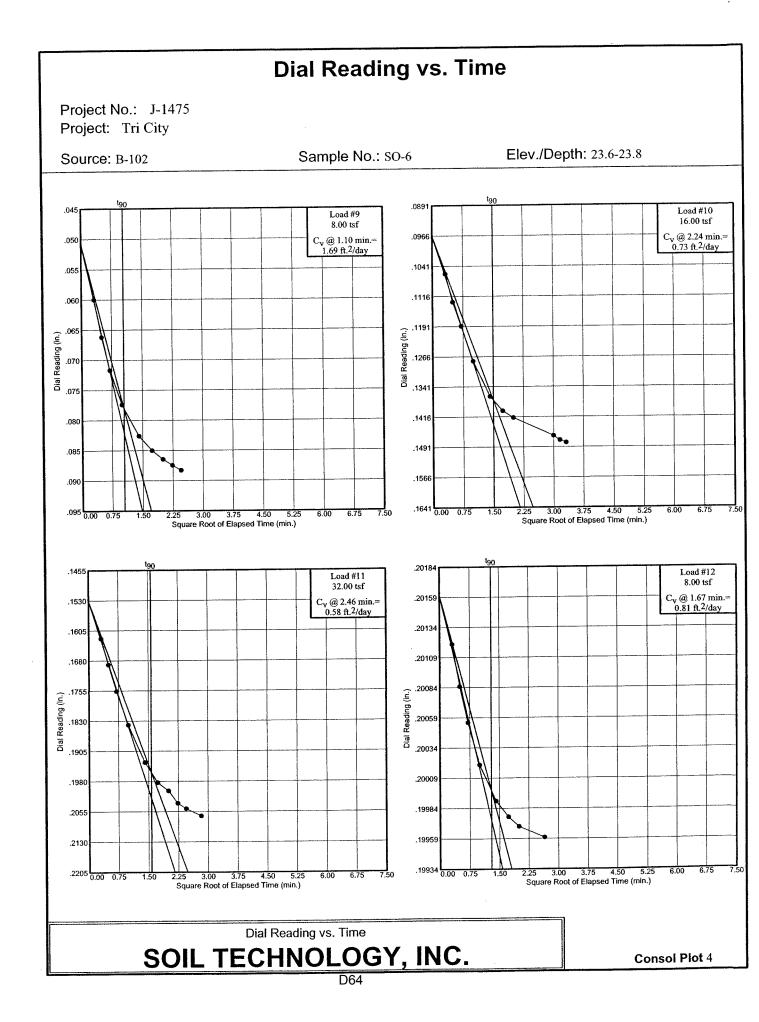
### Moisture Contents Table 1

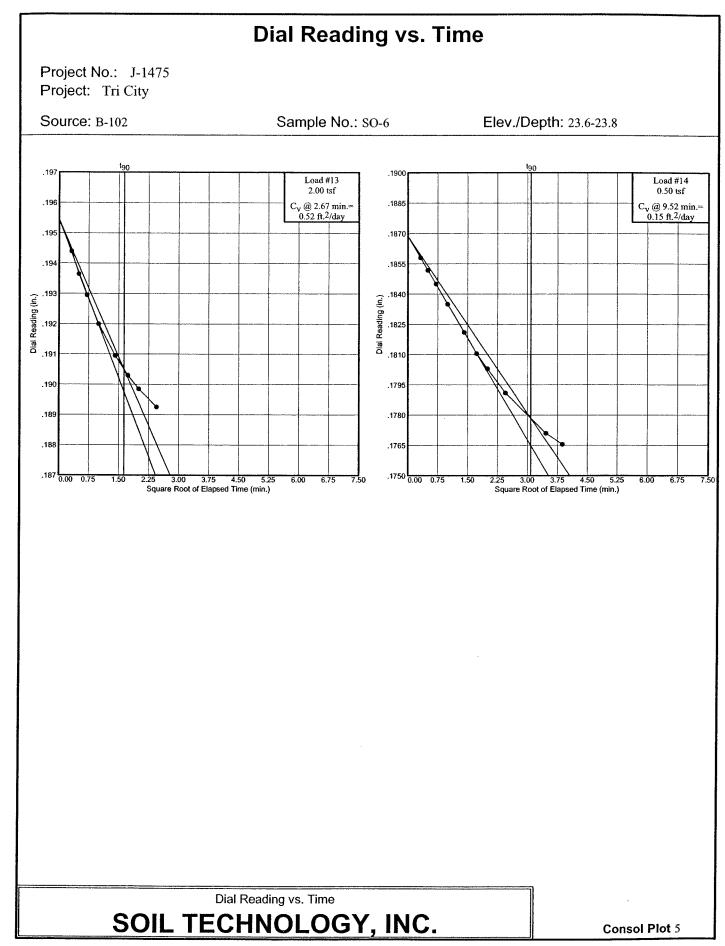
Exploration	Sample	Sample Depth	Moisture Content
Number	Number	(ft)	%
B-101	S-1	2.5-4.0	30
B-101	SS-8	27.5-29.0	45
B-102	SS-3	10.0-11.5	42
B-102	SS-7	24.5-26.0	45
B-103	SS-4	15.0-16.5	50
B-103	SS-6	22.5-24.0	46
B-104	SS-1	5.0-6.5	34
B-104	SS-7	26.0-27.5	37
B-105	SS-1	5.0-6.5	32
B-105	SS-4	15.0-16.5	35
B-105	SS-7	25.0-26.5	47

### Percent Passing U.S. Sieve Number 200 Table 2

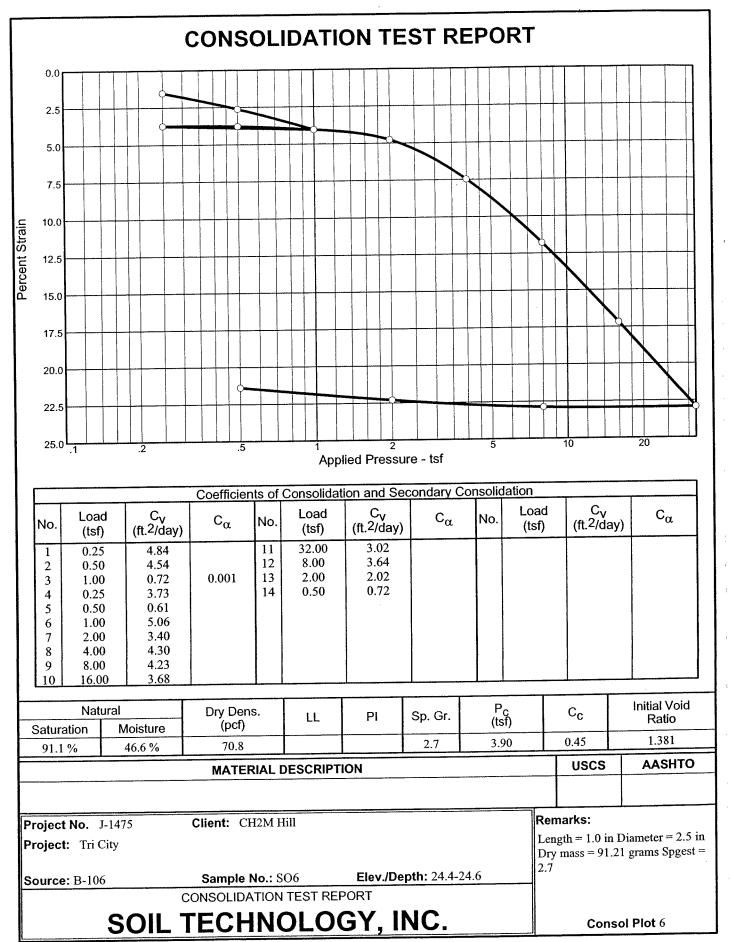
Exploration Number	Sample Number	Sample Depth (ft)	Percent Passing 75 micron
B-102	SS-10	30.5-32.0	19
B-103	SS-8	27.0-28.5	29
B-103	S-11	36.0-37.5	6
B-104	SS-7	26.0-27.5	47
B-106	SS-8	27.5-29.0	35

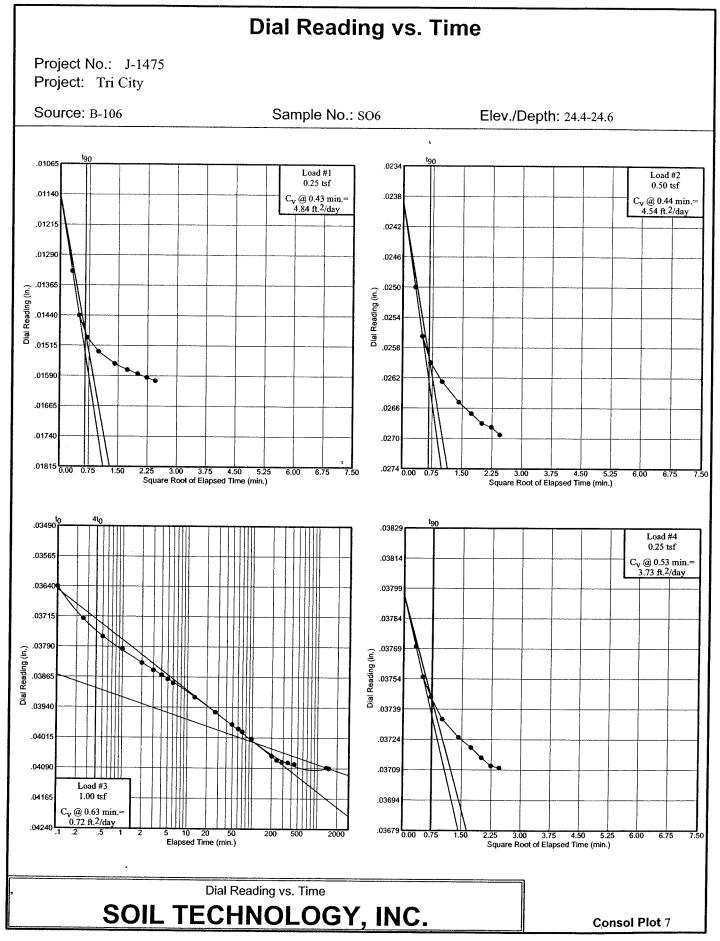
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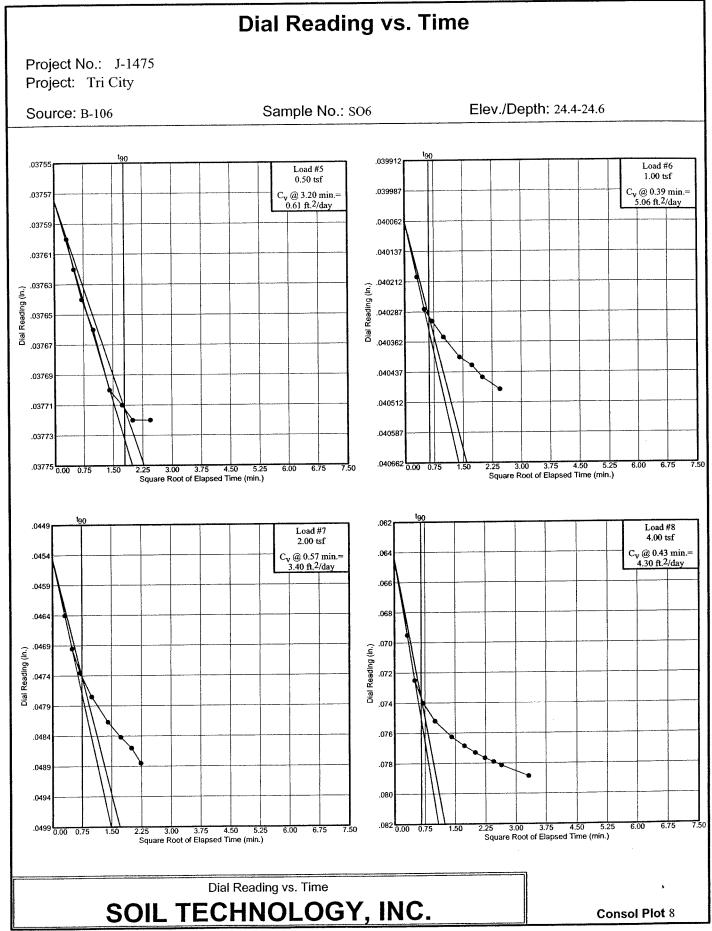


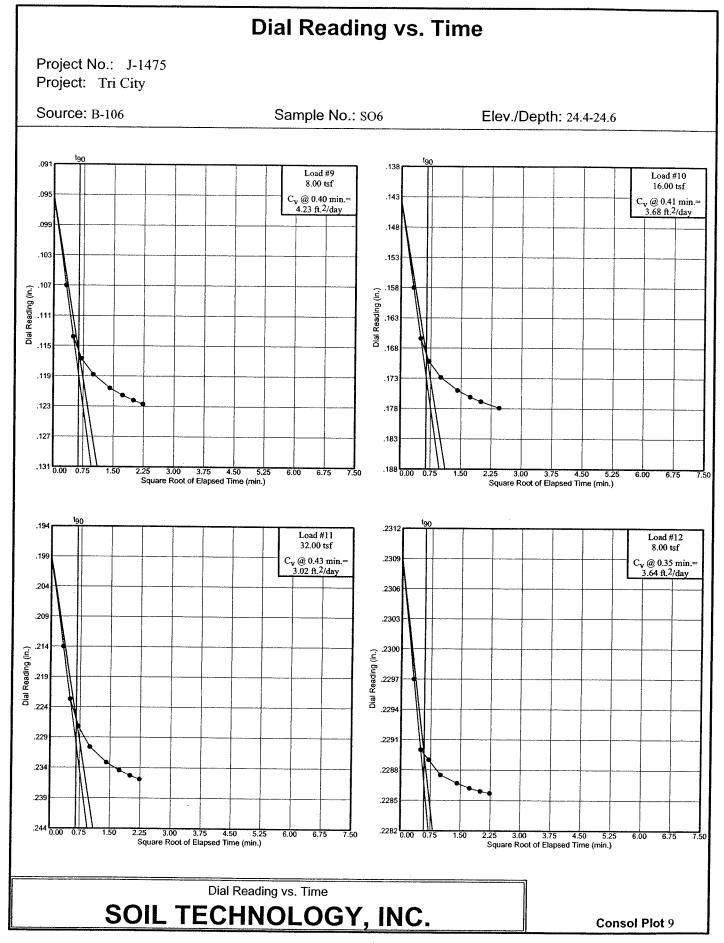
D65

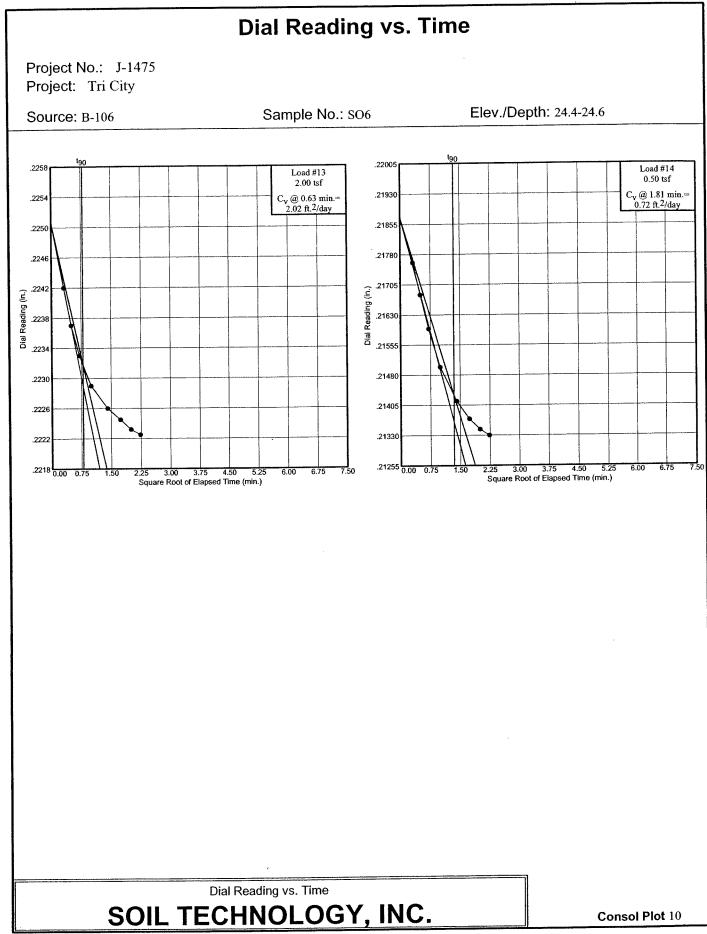




D67







D70

### APPENDIX E IMPORTANT INFORMATION ABOUT YOUR GEOTECHNICAL REPORT



Date:	May, 2008	
To:	MWH Global	
	Americas, Inc.	

### **Important Information About Your Geotechnical/Environmental Report**

### CONSULTING SERVICES ARE PERFORMED FOR SPECIFIC PURPOSES AND FOR SPECIFIC CLIENTS.

Consultants prepare reports to meet the specific needs of specific individuals. A report prepared for a civil engineer may not be adequate for a construction contractor or even another civil engineer. Unless indicated otherwise, your consultant prepared your report expressly for you and expressly for the purposes you indicated. No one other than you should apply this report for its intended purpose without first conferring with the consultant. No party should apply this report for any purpose other than that originally contemplated without first conferring with the consultant.

### THE CONSULTANT'S REPORT IS BASED ON PROJECT-SPECIFIC FACTORS.

A geotechnical/environmental report is based on a subsurface exploration plan designed to consider a unique set of project-specific factors. Depending on the project, these may include: the general nature of the structure and property involved; its size and configuration; its historical use and practice; the location of the structure on the site and its orientation; other improvements such as access roads, parking lots, and underground utilities; and the additional risk created by scope-of-service limitations imposed by the client. To help avoid costly problems, ask the consultant to evaluate how any factors that change subsequent to the date of the report may affect the recommendations. Unless your consultant indicates otherwise, your report should not be used: (1) when the nature of the proposed project is changed (for example, if an office building will be erected instead of a parking garage, or if a refrigerated warehouse will be built instead of an unrefrigerated one, or chemicals are discovered on or near the site); (2) when the size, elevation, or configuration of the proposed project is altered; (3) when the location or orientation of the proposed project is modified; (4) when there is a change of ownership; or (5) for application to an adjacent site. Consultants cannot accept responsibility for problems that may occur if they are not consulted after factors, which were considered in the development of the report, have changed.

#### SUBSURFACE CONDITIONS CAN CHANGE.

Subsurface conditions may be affected as a result of natural processes or human activity. Because a geotechnical/environmental report is based on conditions that existed at the time of subsurface exploration, construction decisions should not be based on a report whose adequacy may have been affected by time. Ask the consultant to advise if additional tests are desirable before construction starts; for example, groundwater conditions commonly vary seasonally.

Construction operations at or adjacent to the site and natural events such as floods, earthquakes, or groundwater fluctuations may also affect subsurface conditions and, thus, the continuing adequacy of a geotechnical/environmental report. The consultant should be kept apprised of any such events, and should be consulted to determine if additional tests are necessary.

#### MOST RECOMMENDATIONS ARE PROFESSIONAL JUDGMENTS.

Site exploration and testing identifies actual surface and subsurface conditions only at those points where samples are taken. The data were extrapolated by your consultant, who then applied judgment to render an opinion about overall subsurface conditions. The actual interface between materials may be far more gradual or abrupt than your report indicates. Actual conditions in areas not sampled may differ from those predicted in your report. While nothing can be done to prevent such situations, you and your consultant can work together to help reduce their impacts. Retaining your consultant to observe subsurface construction operations can be particularly beneficial in this respect.

### A REPORT'S CONCLUSIONS ARE PRELIMINARY.

The conclusions contained in your consultant's report are preliminary because they must be based on the assumption that conditions revealed through selective exploratory sampling are indicative of actual conditions throughout a site. Actual subsurface conditions can be discerned only during earthwork; therefore, you should retain your consultant to observe actual conditions and to provide conclusions. Only the consultant who prepared the report is fully familiar with the background information needed to determine whether or not the report's recommendations based on those conclusions are valid and whether or not the contractor is abiding by applicable recommendations. The consultant who developed your report cannot assume responsibility or liability for the adequacy of the report's recommendations if another party is retained to observe construction.

### THE CONSULTANT'S REPORT IS SUBJECT TO MISINTERPRETATION.

Costly problems can occur when other design professionals develop their plans based on misinterpretation of a geotechnical/environmental report. To help avoid these problems, the consultant should be retained to work with other project design professionals to explain relevant geotechnical, geological, hydrogeological, and environmental findings, and to review the adequacy of their plans and specifications relative to these issues.

#### BORING LOGS AND/OR MONITORING WELL DATA SHOULD NOT BE SEPARATED FROM THE REPORT.

Final boring logs developed by the consultant are based upon interpretation of field logs (assembled by site personnel), field test results, and laboratory and/or office evaluation of field samples and data. Only final boring logs and data are customarily included in geotechnical/environmental reports. These final logs should not, under any circumstances, be redrawn for inclusion in architectural or other design drawings, because drafters may commit errors or omissions in the transfer process.

To reduce the likelihood of boring log or monitoring well misinterpretation, contractors should be given ready access to the complete geotechnical engineering/environmental report prepared or authorized for their use. If access is provided only to the report prepared for you, you should advise contractors of the report's limitations, assuming that a contractor was not one of the specific persons for whom the report was prepared, and that developing construction cost estimates was not one of the specific purposes for which it was prepared. While a contractor may gain important knowledge from a report prepared for another party, the contractor should discuss the report with your consultant and perform the additional or alternative work believed necessary to obtain the data specifically appropriate for construction cost estimating purposes. Some clients hold the mistaken impression that simply disclaiming responsibility for the accuracy of subsurface information always insulates them from attendant liability. Providing the best available information to contractors helps prevent costly construction problems and the adversarial attitudes that aggravate them to a disproportionate scale.

### READ RESPONSIBILITY CLAUSES CLOSELY.

Because geotechnical/environmental engineering is based extensively on judgment and opinion, it is far less exact than other design disciplines. This situation has resulted in wholly unwarranted claims being lodged against consultants. To help prevent this problem, consultants have developed a number of clauses for use in their contracts, reports and other documents. These responsibility clauses are not exculpatory clauses designed to transfer the consultant's liabilities to other parties; rather, they are definitive clauses that identify where the consultant's responsibilities begin and end. Their use helps all parties involved recognize their individual responsibilities and take appropriate action. Some of these definitive clauses are likely to appear in your report, and you are encouraged to read them closely. Your consultant will be pleased to give full and frank answers to your questions.

The preceding paragraphs are based on information provided by the ASFE/Association of Engineering Firms Practicing in the Geosciences, Silver Spring, Maryland